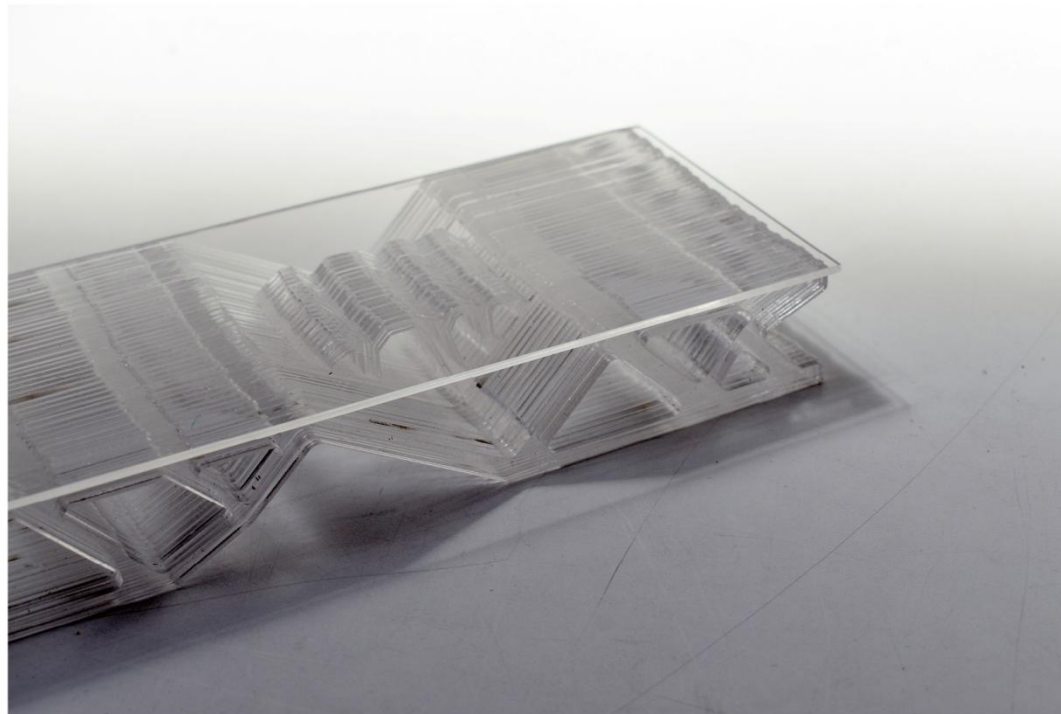


Just Glass.

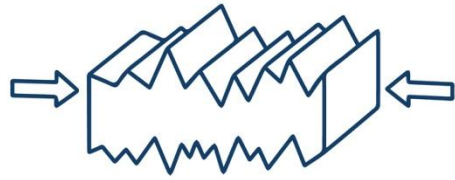
Development of a Topology Optimization Algorithm for a mass-customized cast glass component.



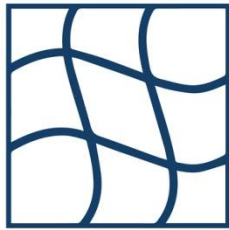
P5 Presentation
June 2022

Student: Anna Maria Koniari | **Mentor Team:** Dr. Faidra Oikonomopoulou & Dr. Charalampos Andriotis

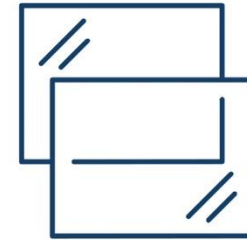
Introduction



compressive strength



Young's modulus



Spatial continuity



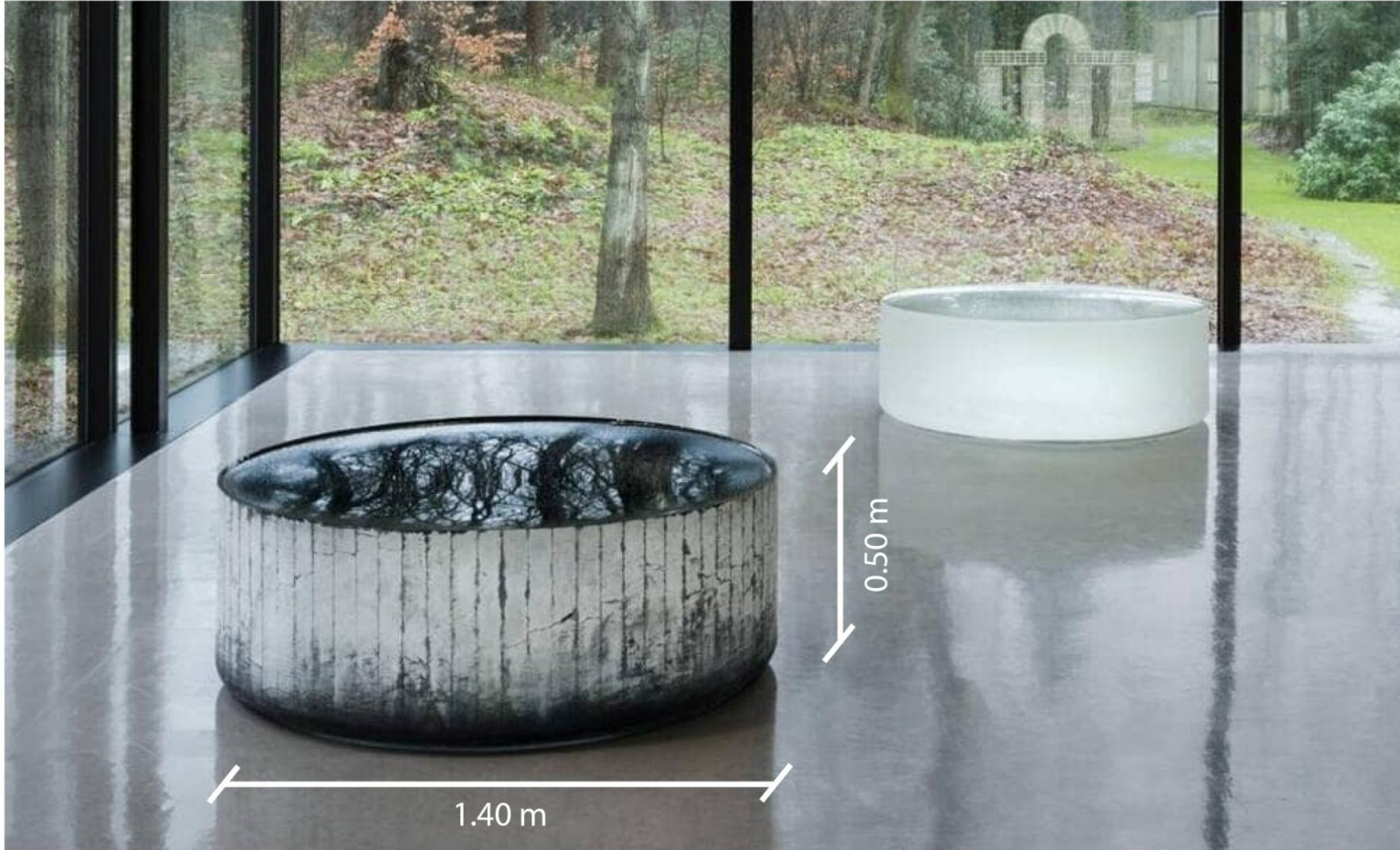
Apple Store, 5th Avenue, New York



Human-scale cast glass piece
Karen le Monte, Corning Museum of Glass

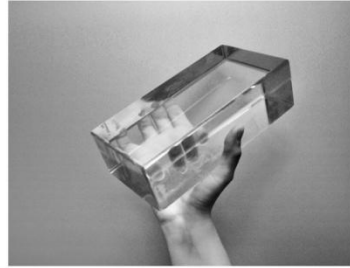


Glass composites promise to change the look of bridges as dramatically as the transition from wood to steel.



🕒 4 months

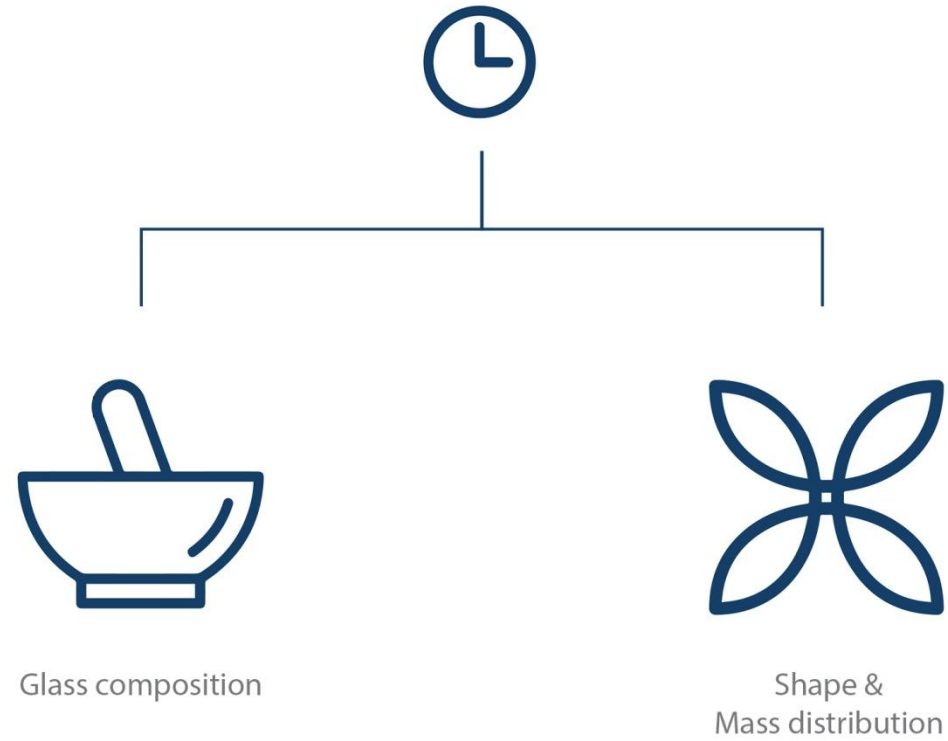
Opposites of white' by Roni Horn displayed in Kroller Moller museum



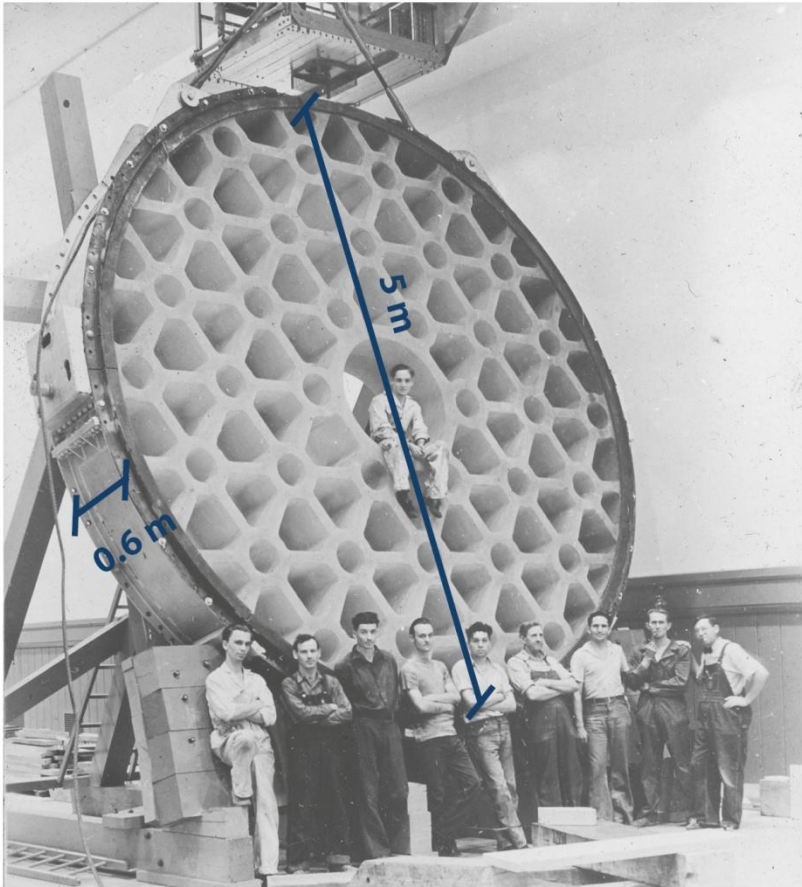
Crystal Houses, Amsterdam
(Oikonomopoulou, 2019)



8 - 38 hours



Borosilicate glass



Telescope mirror Hale 1



10 months

E6 Glass



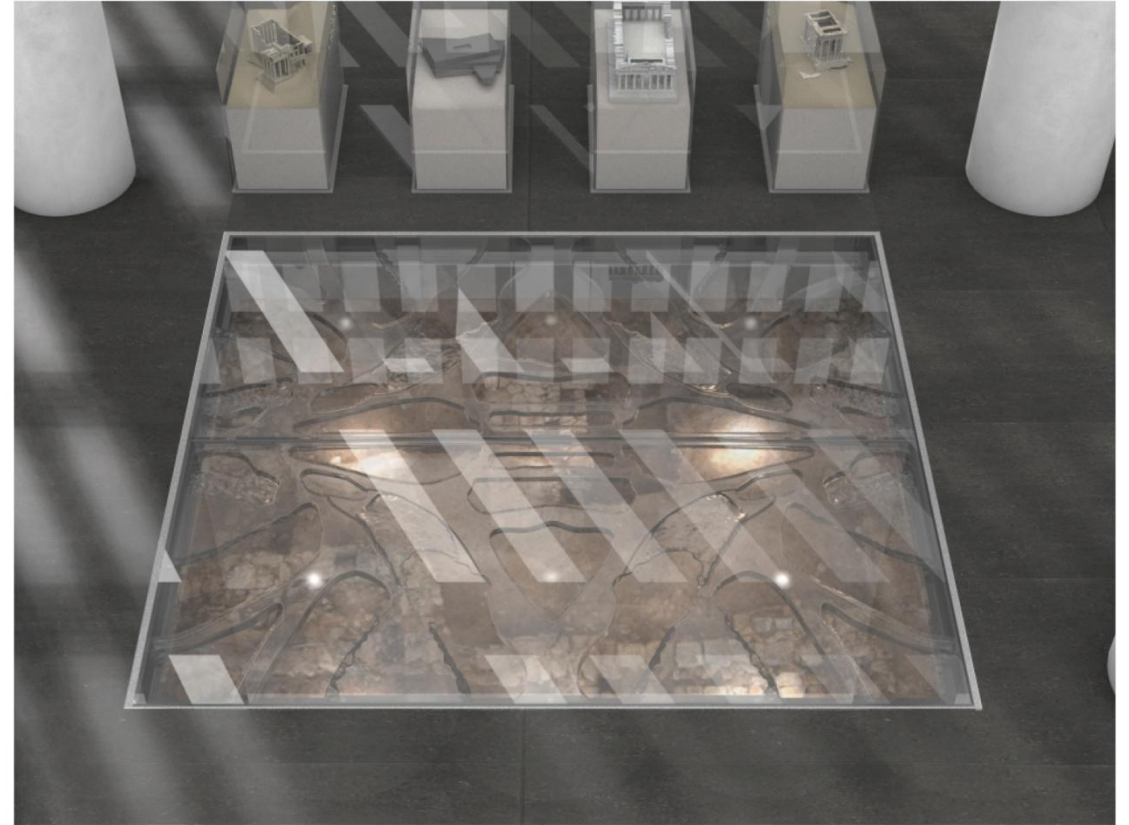
Giant Magellan Telescope Mirror



3 months



Topologically Optimized Cast Glass Grid Shell Nodes
Wilfried Damen (2019)



Glass Giants. Mass-optimized massive cast glass slab.
Iro-Maria Stefanaki (2020)



commercial software



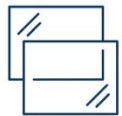
compression



tension



annealing & manufacturing criteria



glass



compression
500 MPa



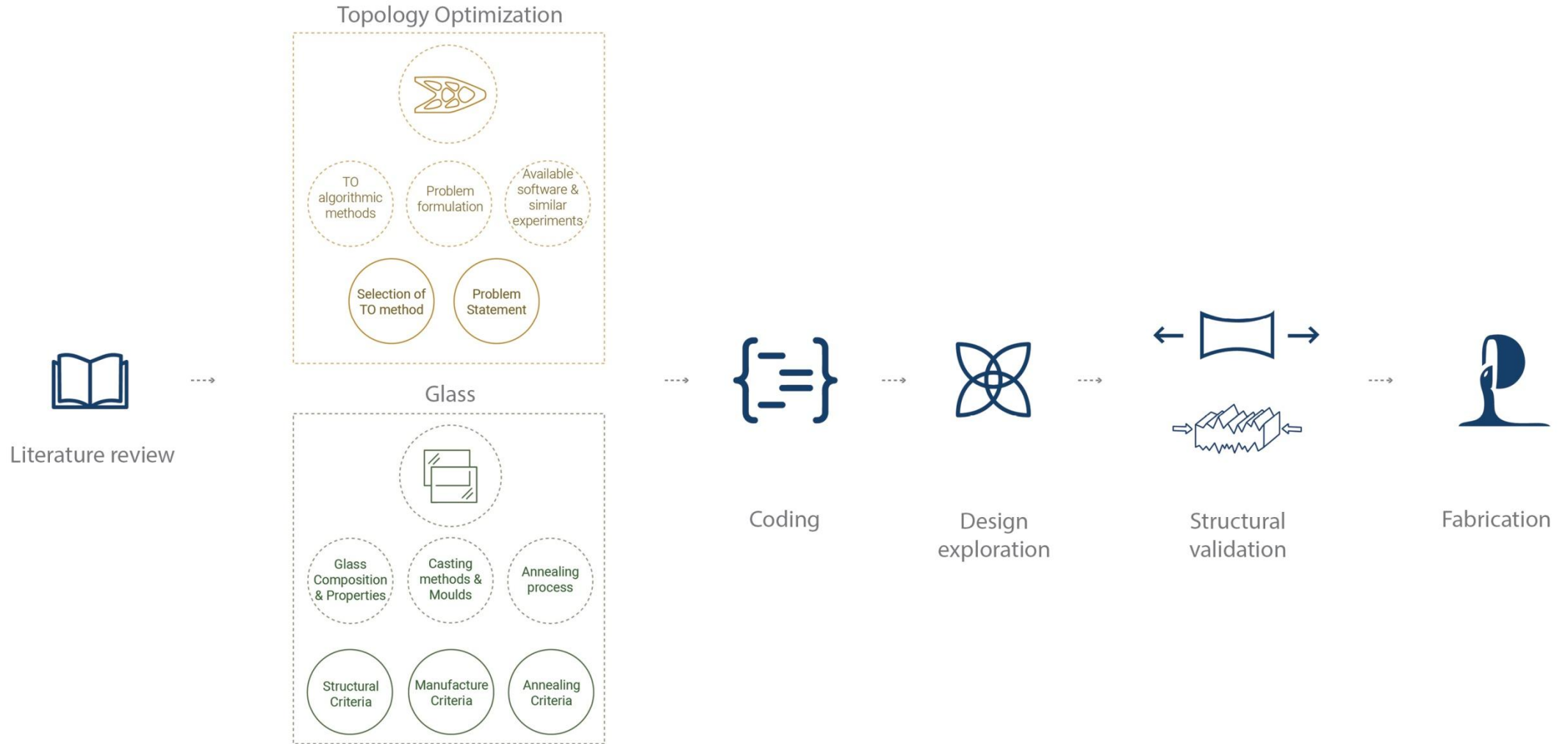
tension
45 MPa



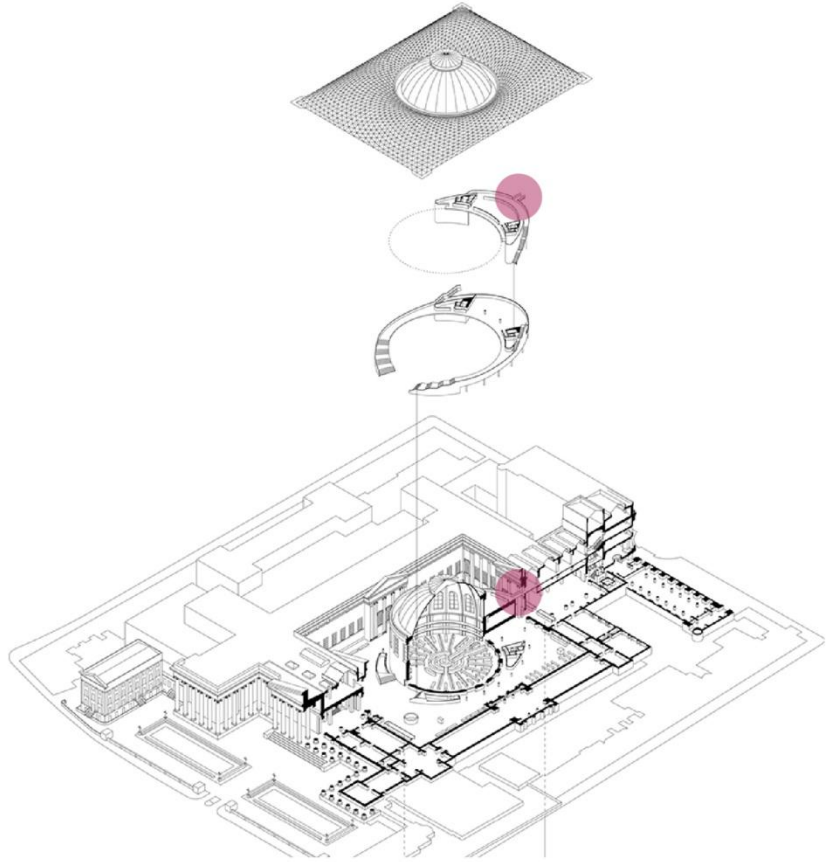
annealing & manufacturing criteria



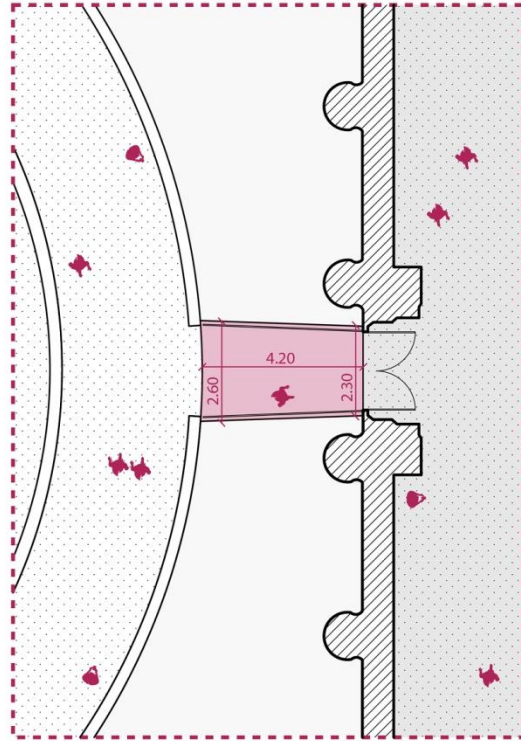
What are the main aspects and inherent limitations of composing a Topology Optimization algorithm for the design of massive cast glass structures which are time and cost efficient?



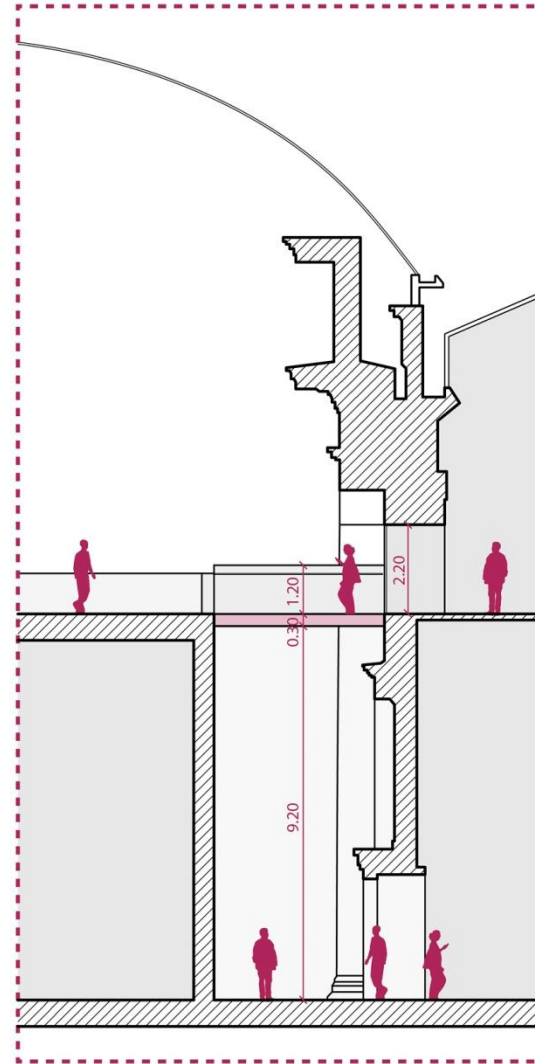
Case Study



Glass slab inside the Great Court in the British Museum
Intervention by Foster + Partners (2000)

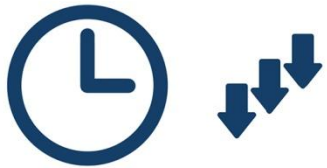


Plan

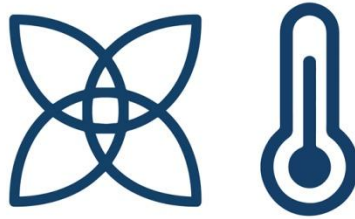


Section

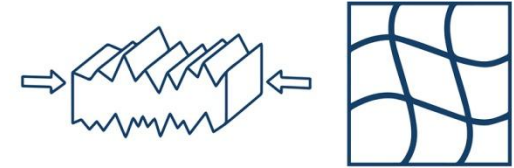
Glass



annealing time



shaping behavior
melting temperature



structural & mechanical
properties



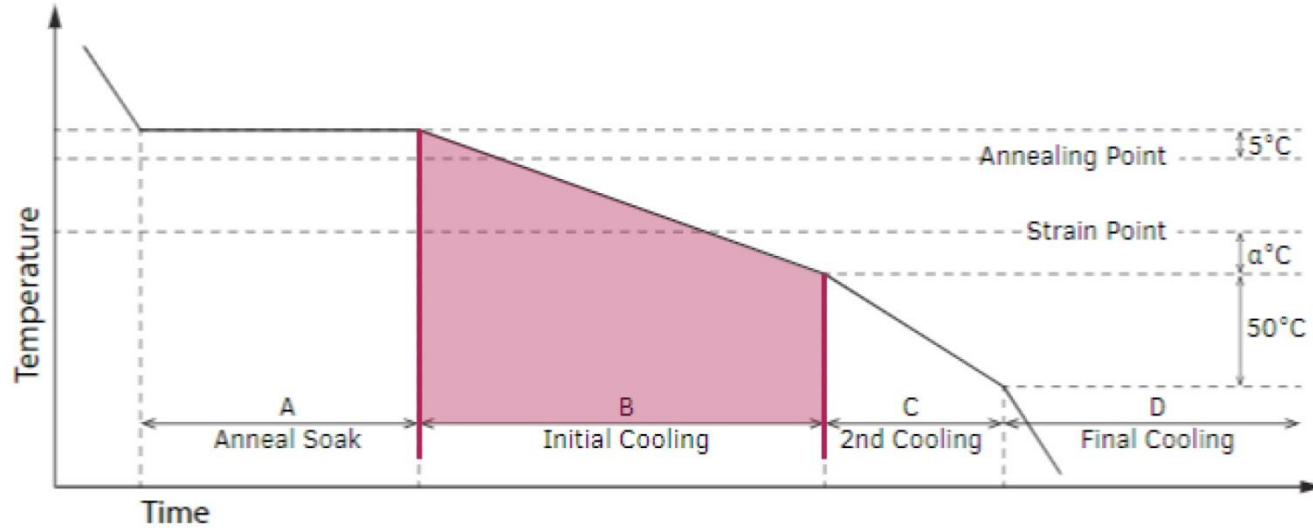


(Oikonomopoulou, 2019)



Kiln-casting





(Oikonomopoulou, 2019)

$$h = \frac{\sigma}{\frac{E \alpha_{ex} \rho c_p}{(1 - \mu) \lambda} \times d^2 \times b}$$



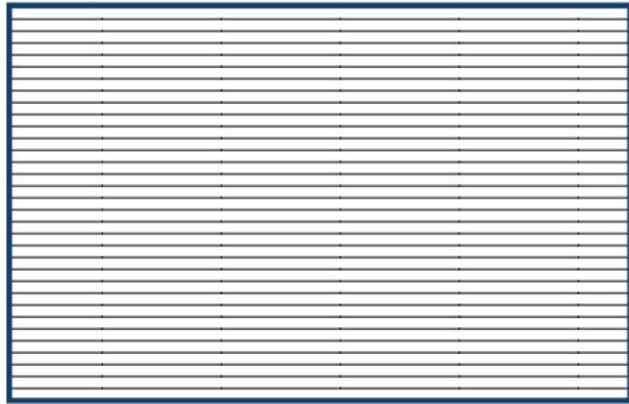
Arup/Davidfotografie.



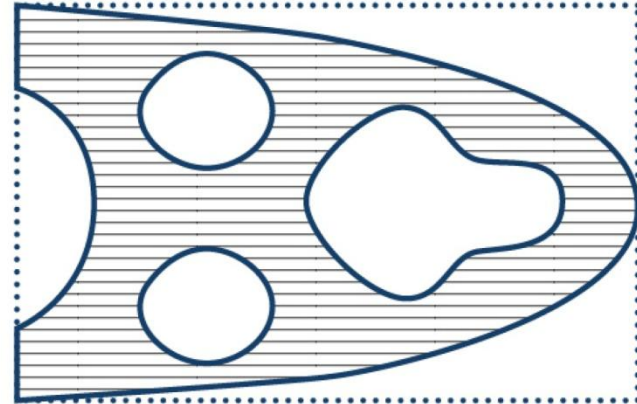
Damen, W. (2019). Topologically Optimised Cast Glass Grid Shell Nodes



Topology Optimization

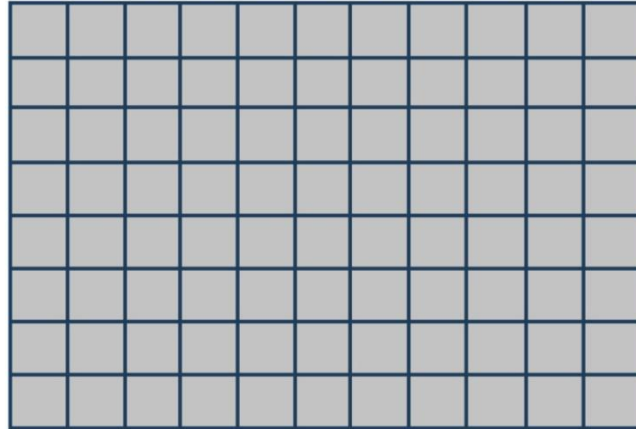


Initial shape



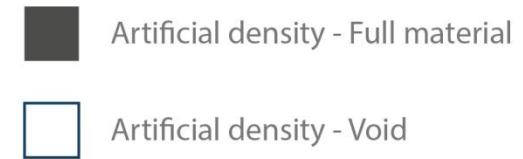
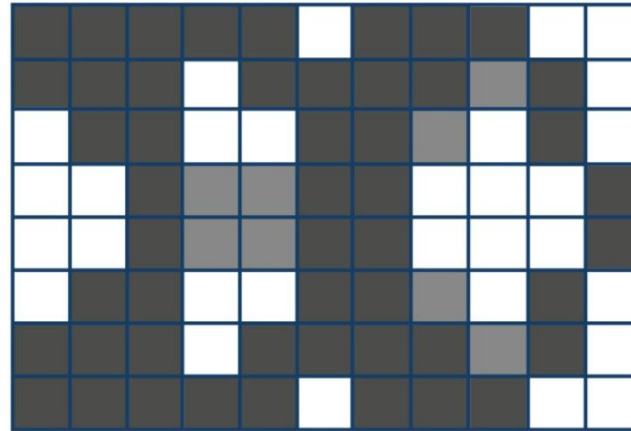
Shape after optimization





■ Initial value of artificial density





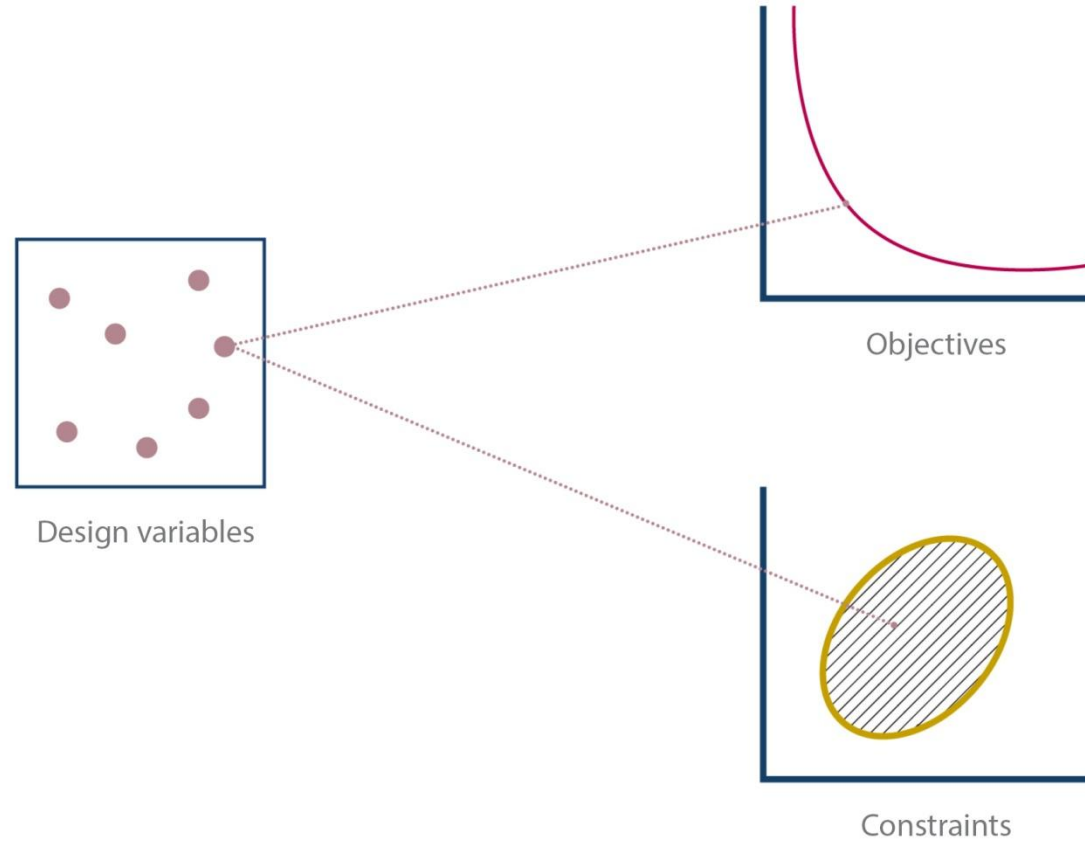
$$\min_x f(x), \quad x(e)^p, \quad 0 < x_{min} \leq x(e) \leq 1, \quad x_{min} = 10^{-3}, \quad p = 3$$

$$e \in \Omega_{des} = \Omega_{mat} \setminus \Omega_{nonmat}, \quad \Omega_{mat} \subseteq \Omega \subseteq \mathbb{R}^n, n = 2,3$$

$$\text{subject to } g_i(x) \leq 0, \quad i = 1,2, \dots, m$$

$$h_i(x) = 0, \quad i = 1,2, \dots, p$$

Problem statement





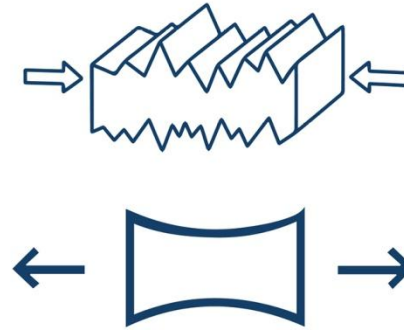
Compliance

$$\min_x C(x) = U^T K U$$

$$\text{subject to: } \frac{V(x)}{V} \leq f$$

$$K U = F$$

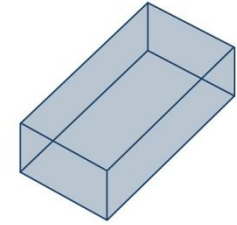
$$0 < x_{min} \leq x \leq 1$$



Stress

$$\min_x G(x)$$

$$\text{subject to: } \int_{\Omega} x \, d\Omega \leq M_0$$



Volume

$$\min_x V(x) = \sum_N x_e V_e$$

$$\text{subject to: } K U = F$$

$$\frac{c}{c_L} \leq 1$$

$$x_e^{(p-q)} \frac{\sigma_e}{\sigma_{Lt}} \leq 1, \quad e = 1, \dots, N$$

$$0 < x_{min} \leq x \leq 1$$



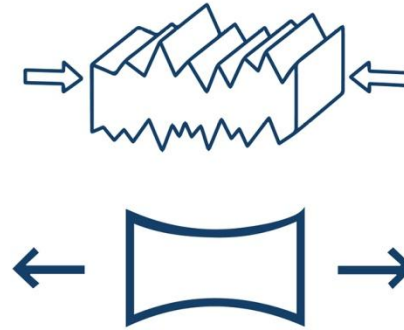
Compliance

$$\min_x C(x) = U^T K U$$

subject to: $\frac{V(x)}{V} \leq f$

$$K U = F$$

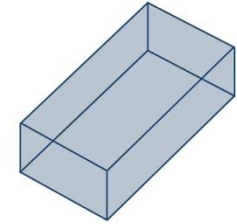
$$0 < x_{min} \leq x \leq 1$$



Stress

$$\min_x G(x)$$

subject to: $\int_{\Omega} x \, d\Omega \leq M_0$



Volume

$$\min_x V(x) = \sum_N x_e V_e$$

subject to: $K U = F$

$$\frac{c}{c_L} \leq 1$$

$$x_e^{(p-q)} \frac{\sigma_e}{\sigma_{Lt}} \leq 1, \quad e = 1, \dots, N$$

$$0 < x_{min} \leq x \leq 1$$



Constraints

	Equilibrium*	Min element dimension/ filtering*	Volume	Compliance	Deflection	Principal stresses	Drucker - Prager	Annealing & Manufacturing (dmax)
Volume	✓	✓		✓	✓	✓	✓	✓
Compliance	✓	✓	✓		✓	✓	✓	✓

Objectives



Constraints

	Equilibrium*	Min element dimension/ filtering*	Volume	Compliance	Deflection	Principal stresses	Drucker - Prager	Annealing & Manufacturing (dmax)
Volume	✓	✓		✓	✓	✓	✓	✓
Compliance	✓	✓	✓		✓	✓	✓	✓

Objectives

$$\sum_{e=1}^N K_e(x_e) U_e = \sum_{e=1}^N f_e \Rightarrow \sum_{e=1}^N E(x_e) K_e U_e = \sum_{e=1}^N f_e$$

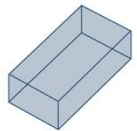


$$x_e = \frac{\sum_{j \in S_e} x_j w_j v_j}{\sum_{j \in S_e} w_j v_j}, \quad j \in S_e \text{ if } r_j \leq r_{min}, \quad r_j = \|x_j - \bar{x}^e\|, \quad r_{min} = \frac{d_{min}}{2}, \quad w_j = \begin{cases} \frac{r_{min} - r_j}{r_{min}}, & \text{if } j \in \Omega_s \\ 0, & \text{if } j \in \Omega_s \text{ if } r_j = \text{dist}(e, j) \leq r_{min} \end{cases}$$

Problem statement

Constraints

	Equilibrium*	Min element dimension/ filtering*	Volume	Compliance	Deflection	Principal stresses	Drucker - Prager	Annealing & Manufacturing (dmax)
Objectives								
Volume	✓	✓		✓	✓	✓	✓	✓
Compliance	✓	✓	✓		✓	✓	✓	✓

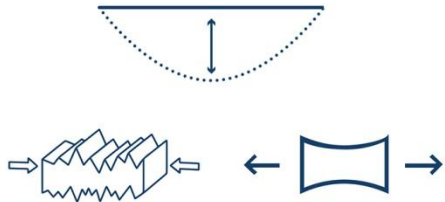


$$V(x) = \int_{\Omega_{des}} x(e) d\Omega_{des}, \quad 0 < x_{min} \leq x(e) \leq 1, \quad e \in \Omega_{des} = \Omega_{mat} \subseteq \Omega \subseteq R^n, n = 2 \quad \frac{V(x)}{V} \leq f$$

$$\frac{c(x)}{c_L} \leq 1, \quad c(x) = \sum_{e=1}^N U_e^T E(x_e) K_e U_e, \quad c_L = a_c c_0$$

Constraints

Objectives	Constraints							
	Equilibrium*	Min element dimension/ filtering*	Volume	Compliance	Deflection	Principal stresses	Drucker - Prager	Annealing & Manufacturing (dmax)
	Volume	✓	✓		✓	✓	✓	✓
Compliance	✓	✓	✓		✓	✓	✓	✓



$$v_k^e < \frac{1}{500} l, \quad k = 1,2,3,4, \quad e \in \Omega_{des} = \Omega_{mat} \subseteq \Omega \subseteq R^n, n = 2$$

$$x_e^{(p-q)} \left(\frac{\sigma_{comp,e}}{\sigma_{comp,lm}} \right) \leq 1, \quad e = 1,2, \dots, N$$

$$\sigma^{eq} = \frac{s+1}{2s} \sqrt{3J_{2D}} + \frac{s-1}{2s} I_1$$

$$x_e^{(p-q)} \left(\frac{\sigma_{ten,e}}{\sigma_{ten,lm}} \right) \leq 1, \quad e = 1,2, \dots, N$$

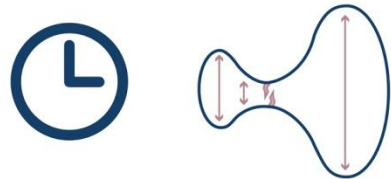
$$x_e^{(p-q)} \frac{\sigma^{eq}}{\sigma_{ten,lm}} \leq 1$$



Constraints

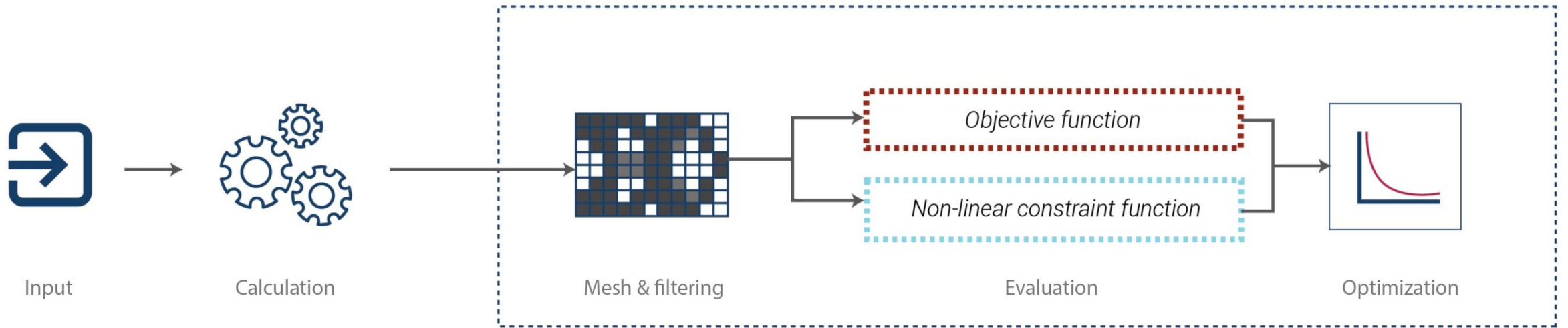
Objectives

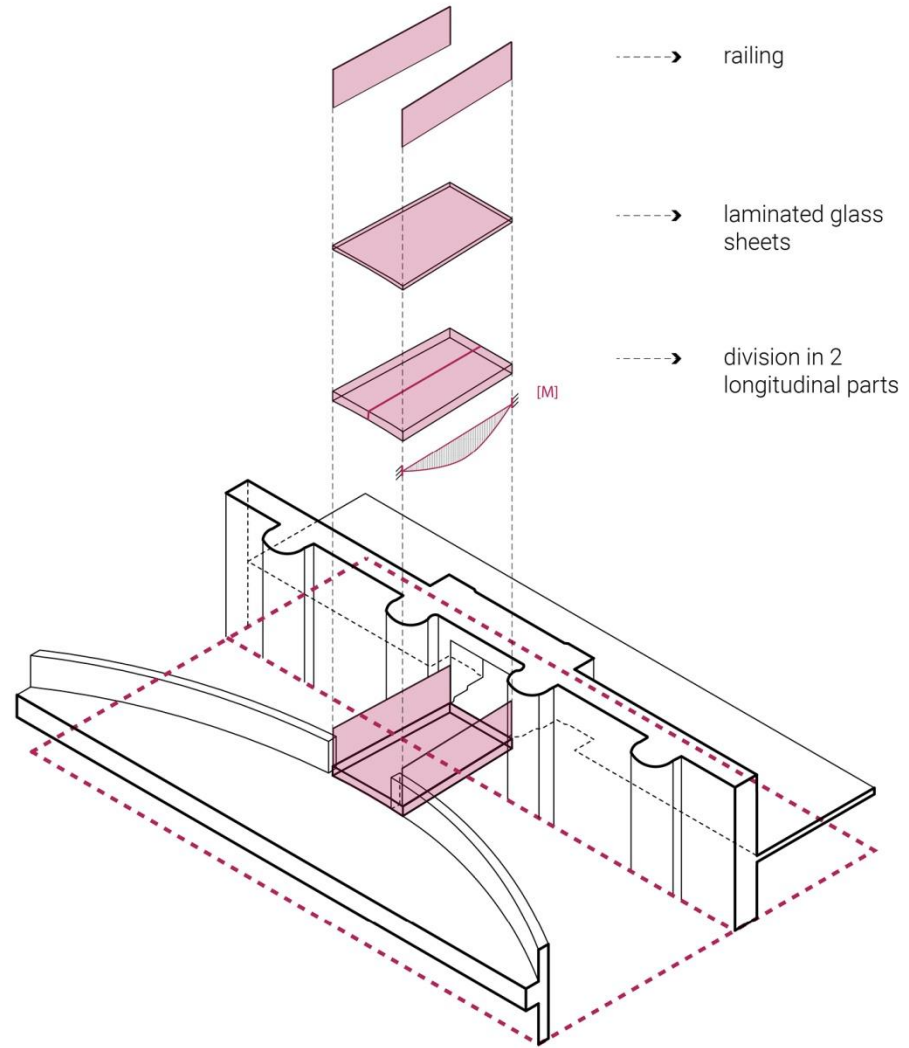
	Equilibrium*	Min element dimension/ filtering*	Volume	Compliance	Deflection	Principal stresses	Drucker - Prager	Annealing & Manufacturing (dmax)
Volume	✓	✓		✓	✓	✓	✓	✓
Compliance	✓	✓	✓		✓	✓	✓	✓

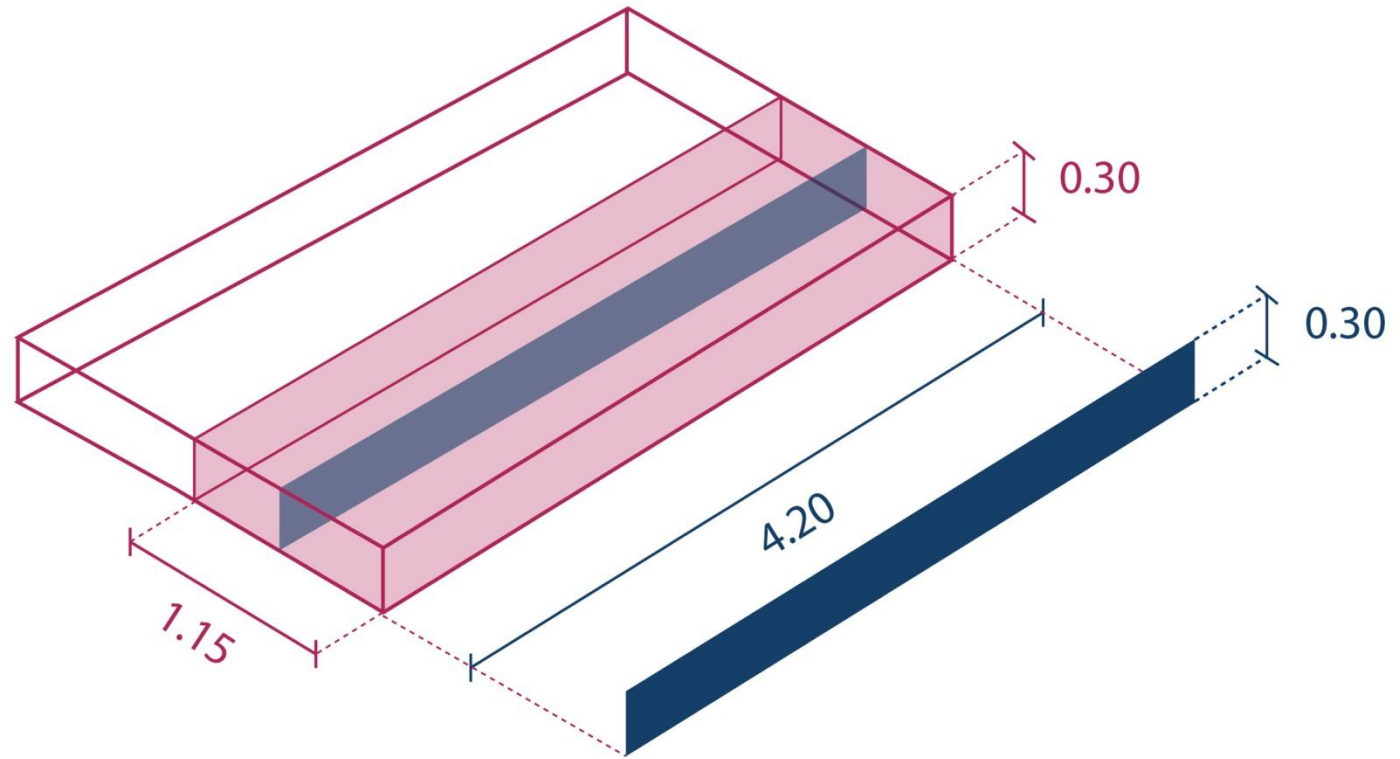


$$d_{max} = \begin{cases} 2 \times d_{min}, & \text{if } T_{ann}(2 \times d_{min}) \leq T_{annmax} \\ \sqrt{\frac{T_{annmax} \times \sigma_{res}}{\Delta T \times \frac{E \times \alpha_{ex}}{1 - \mu} \times \frac{\rho \times c_p}{\lambda} \times b}}, & \text{if } T_{ann}(2 \times d_{min}) > T_{annmax} \end{cases}$$

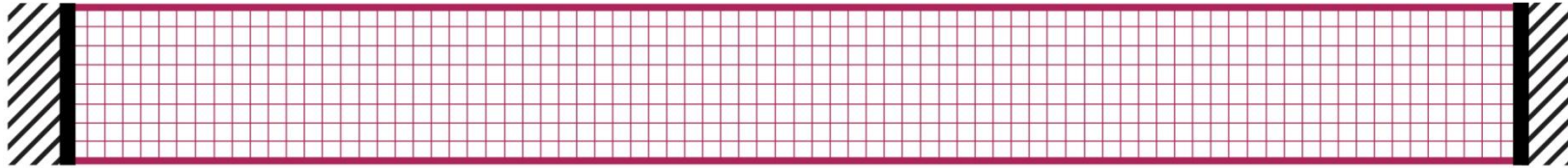
Case Study Application
First iterations

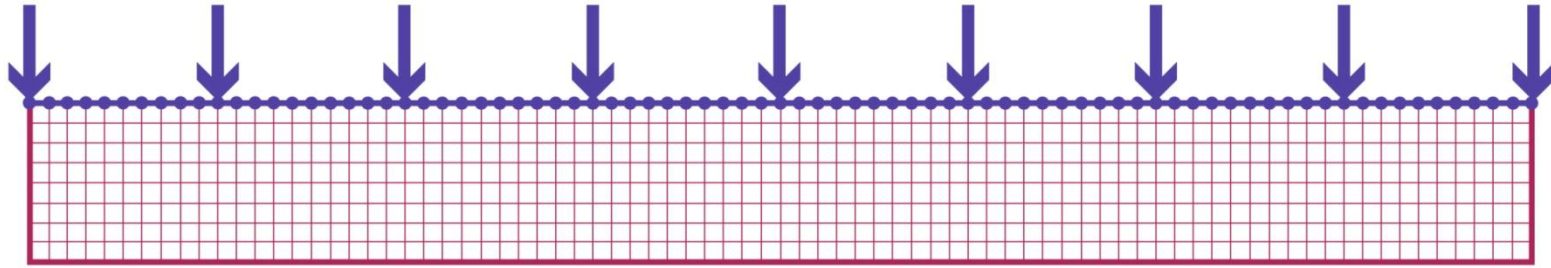


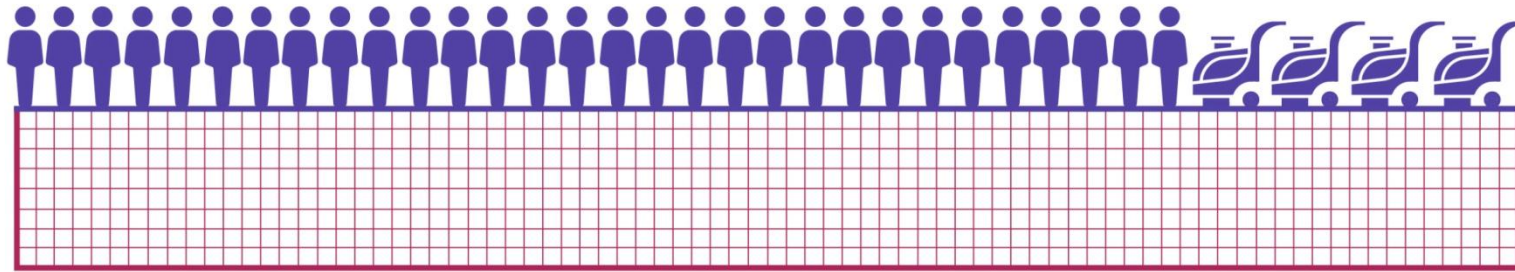






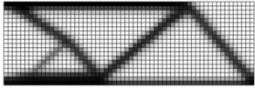



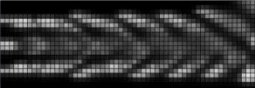
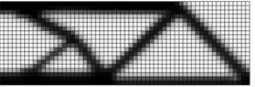










Constraints

Objectives

	Equilibrium*	Min element dimension/ filtering*	Volume	Compliance	Deflection	Principal stresses	Drucker - Prager	Annealing & Manufacturing (dmax)
Compliance	✓	✓						
Volume	✓	✓						

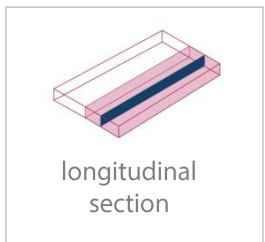
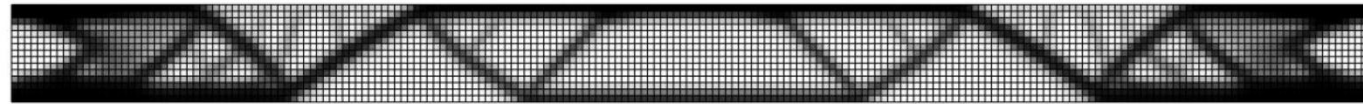
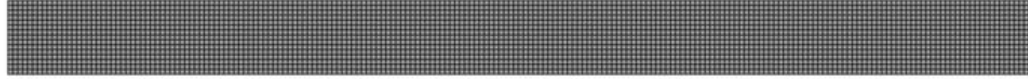


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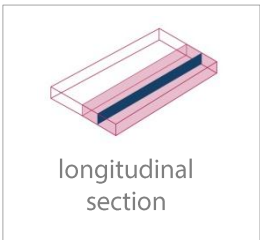
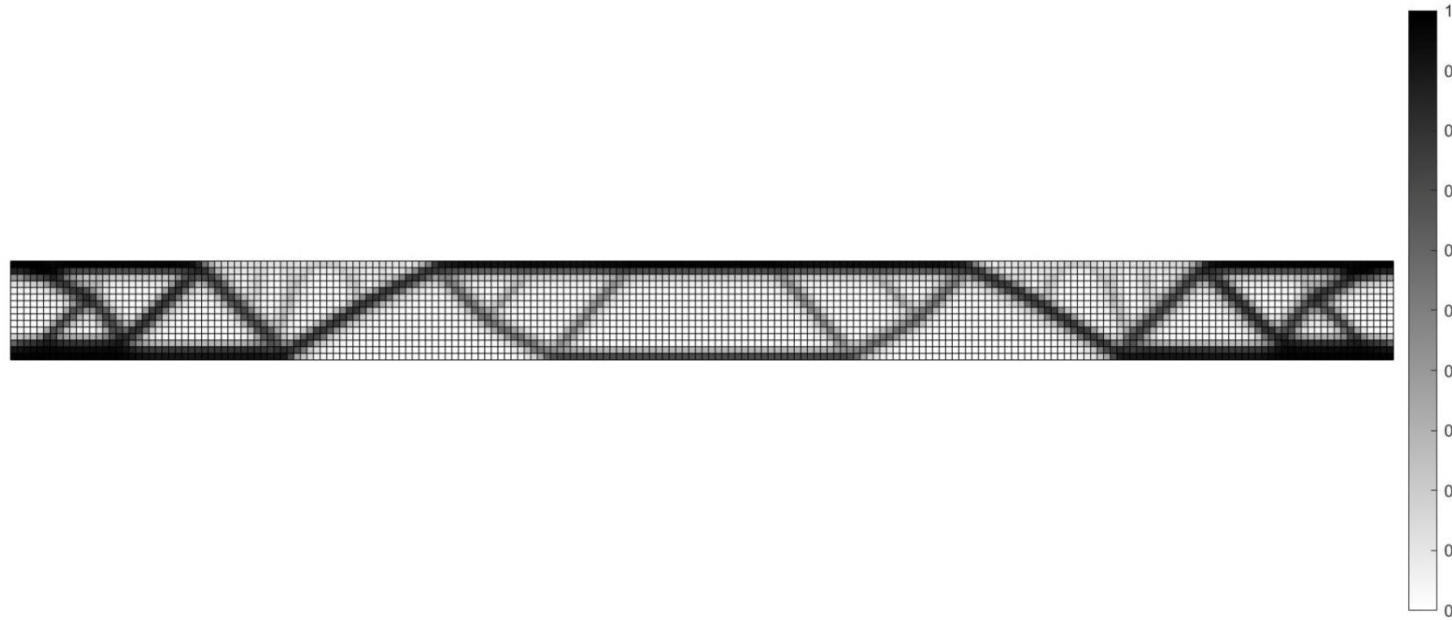
	Equilibrium*	Min element dimension/ filtering*	Volume	Compliance	Deflection	Principal stresses	Drucker - Prager	Annealing & Manufacturing (dmax)
Objectives								
Compliance	✓	✓	✓		✓	✓	✓	✓
Volume	✓	✓		✓	✓	✓	✓	✓

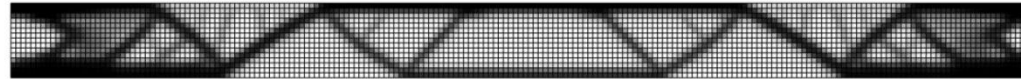


Compliance minimization

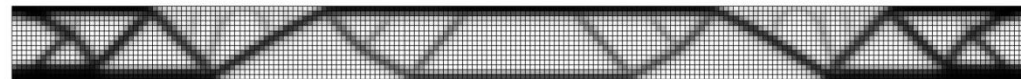


Volume minimization





Compliance minimization



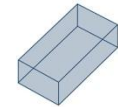
Volume minimization



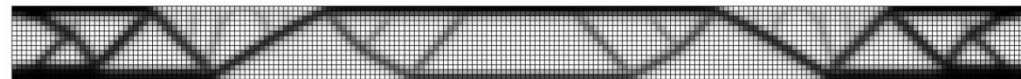
Comparison



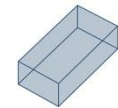
Compliance minimization



1259.1



Volume minimization



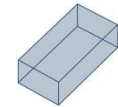
935.8



Comparison



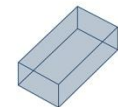
Compliance minimization



1259.1



Volume minimization



935.8



Case Study Application
Design exploration



Glass composition



Design domain



Fabrication method

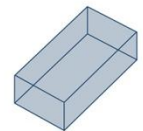
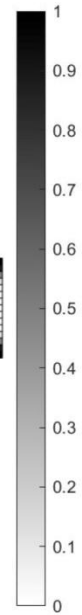
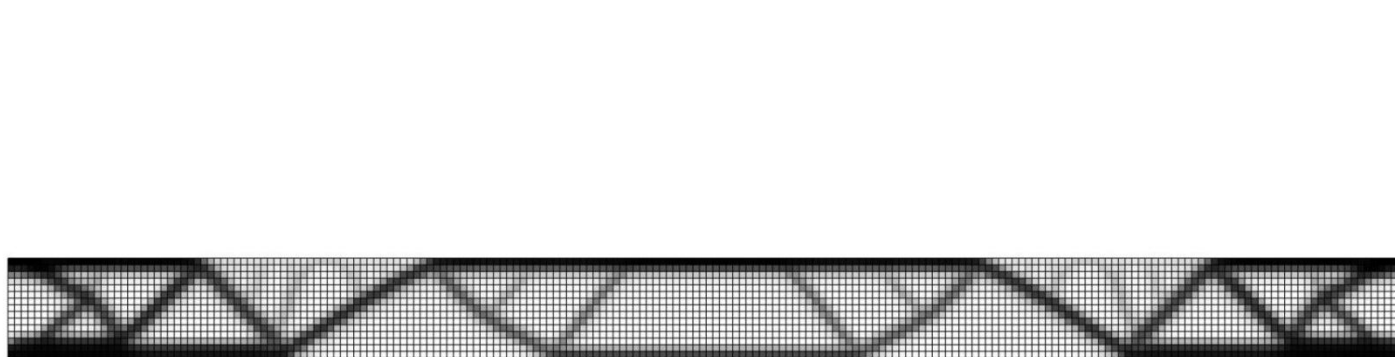


Boundary conditions

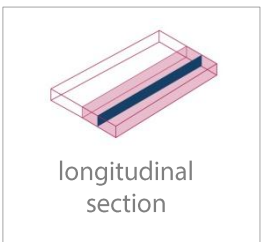




Soda lime

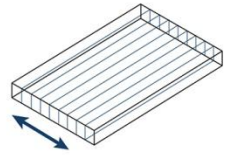


937.3

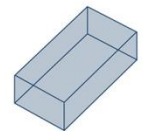
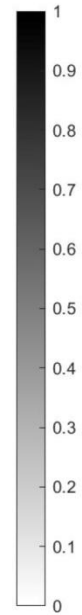
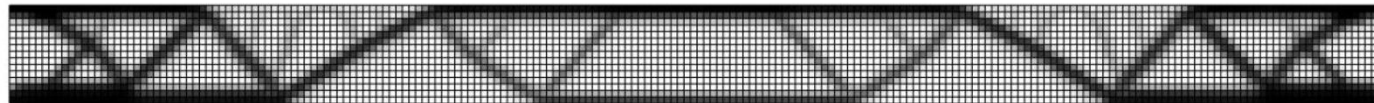


longitudinal
section

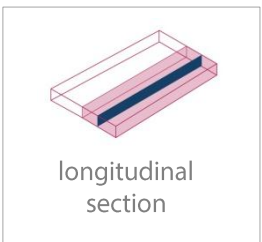




Borosilicate



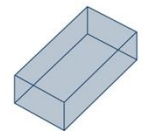
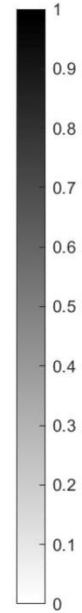
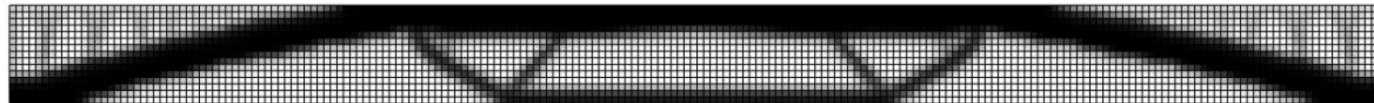
914.7



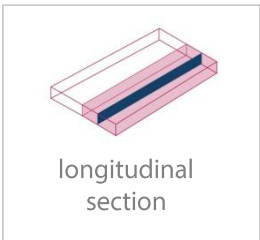
Design exploration



Borosilicate



1500.2

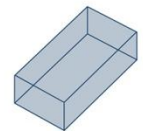
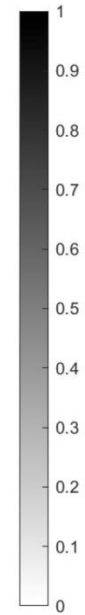
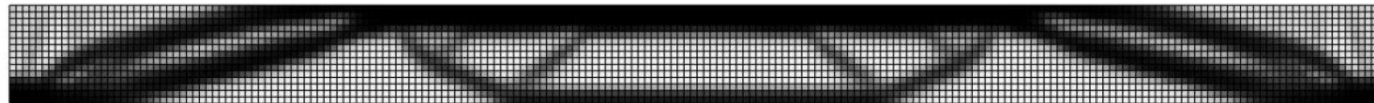


longitudinal section

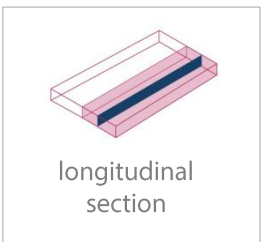




Soda lime

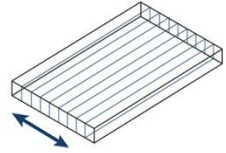


1604.5

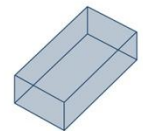
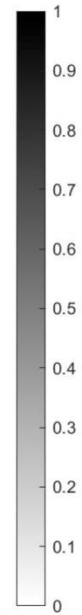
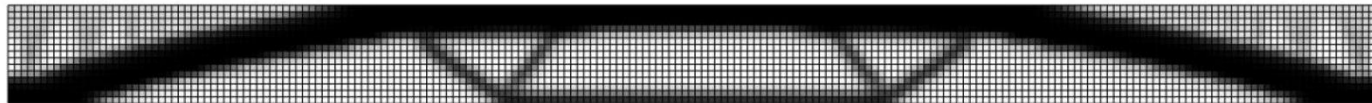


longitudinal
section

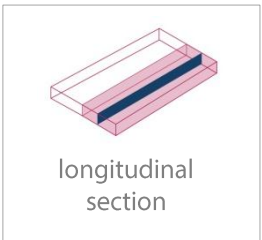




Borosilicate



1381.8

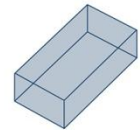
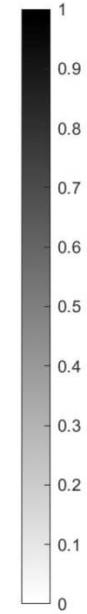
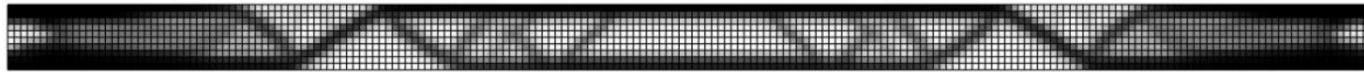


longitudinal section





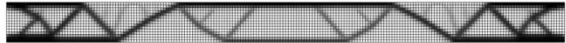
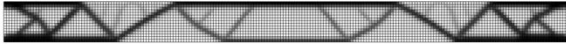





Borosilicate



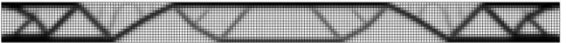
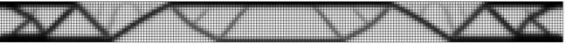





1066.1



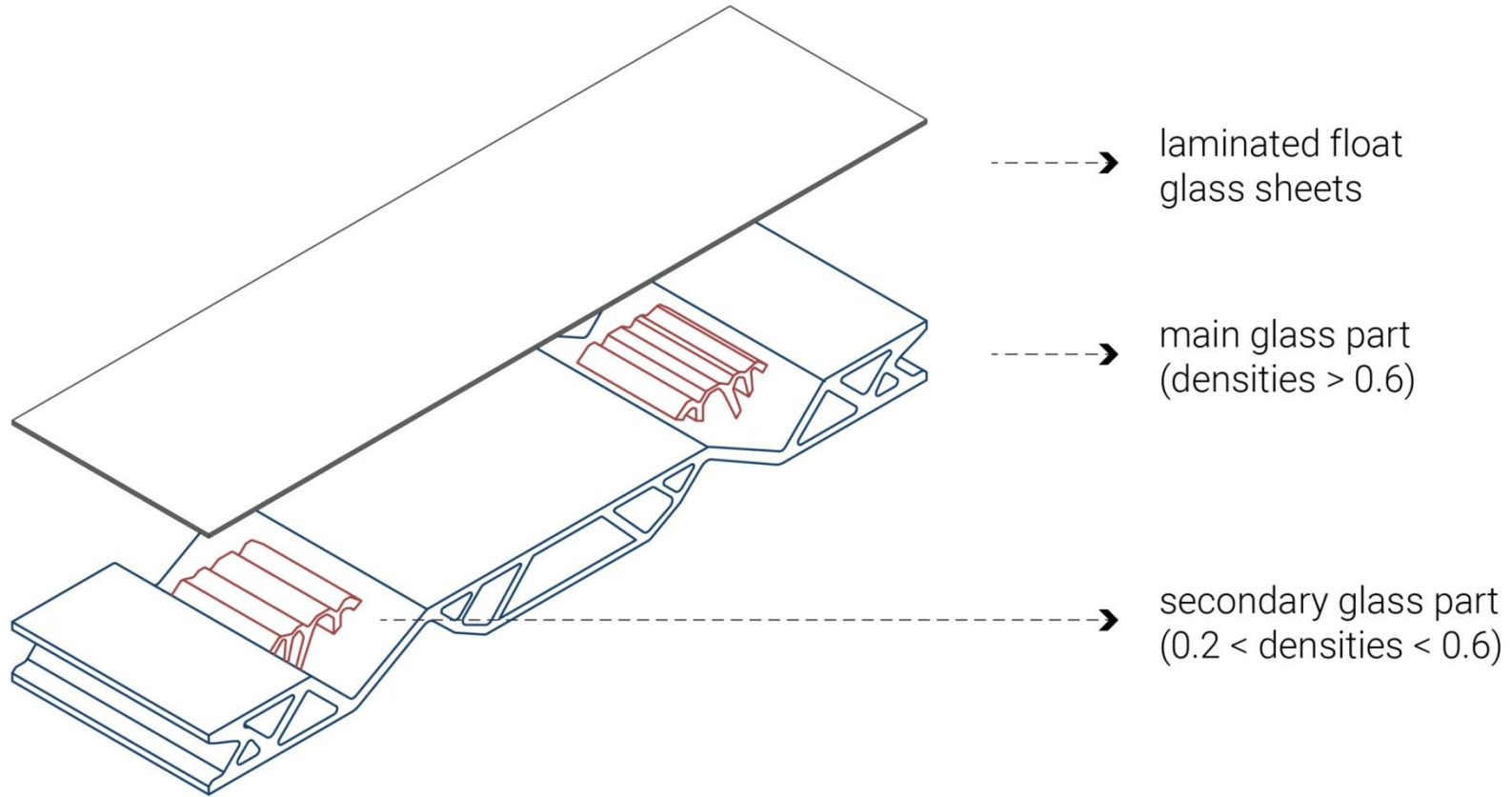
Variations

	Result	Volume
Casting Edge Supports Borosilicate		935.8
Casting Edge Supports Soda Lime		937.3
Stacking Edge Supports Borosilicate		914.7
Casting Point Supports Borosilicate		1500.2
Casting Point Supports Soda lime		1604.5
Stacking Point Supports Borosilicate		1381.3
Casting Edge Supports Borosilicate (20cm)		1066.1

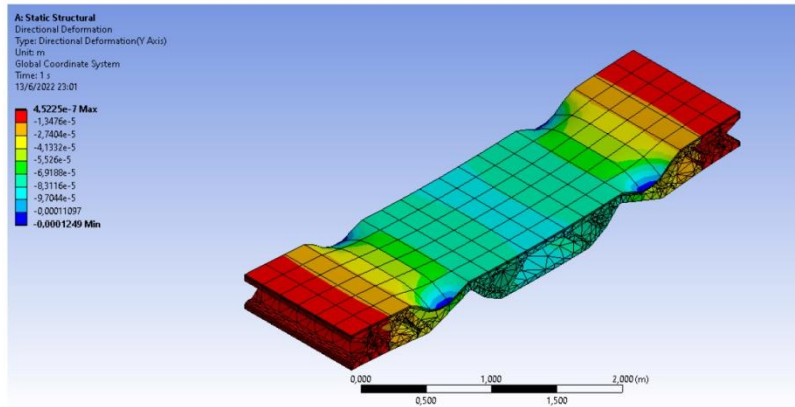
Variations

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Casting Point Supports Borosilicate		1500.2
Casting Point Supports Soda lime		1604.5
Stacking Point Supports Borosilicate		1381.3
Casting Edge Supports Borosilicate (20cm)		1066.1

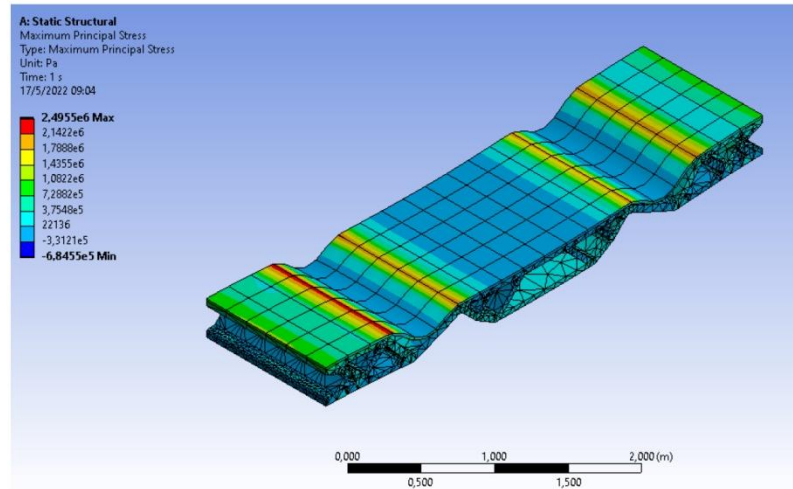
Case Study Application
Final Design



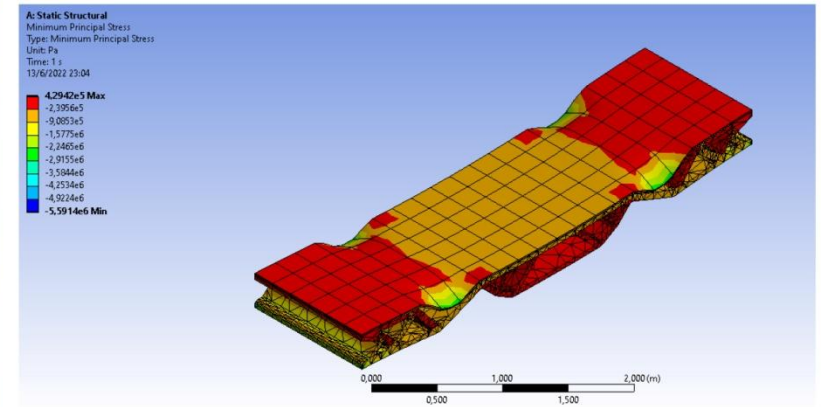
Structural verification



Displacement



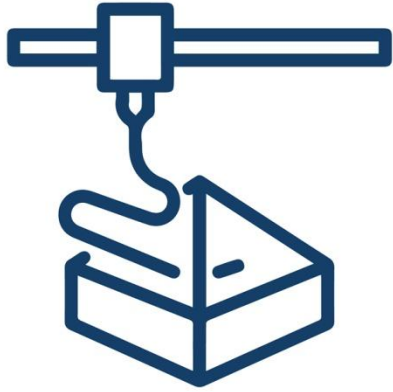
Maximum principal stress



Minimum principal stress



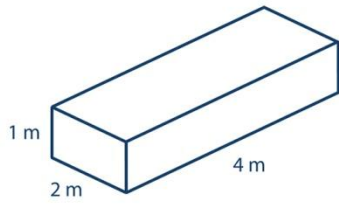
Fabrication



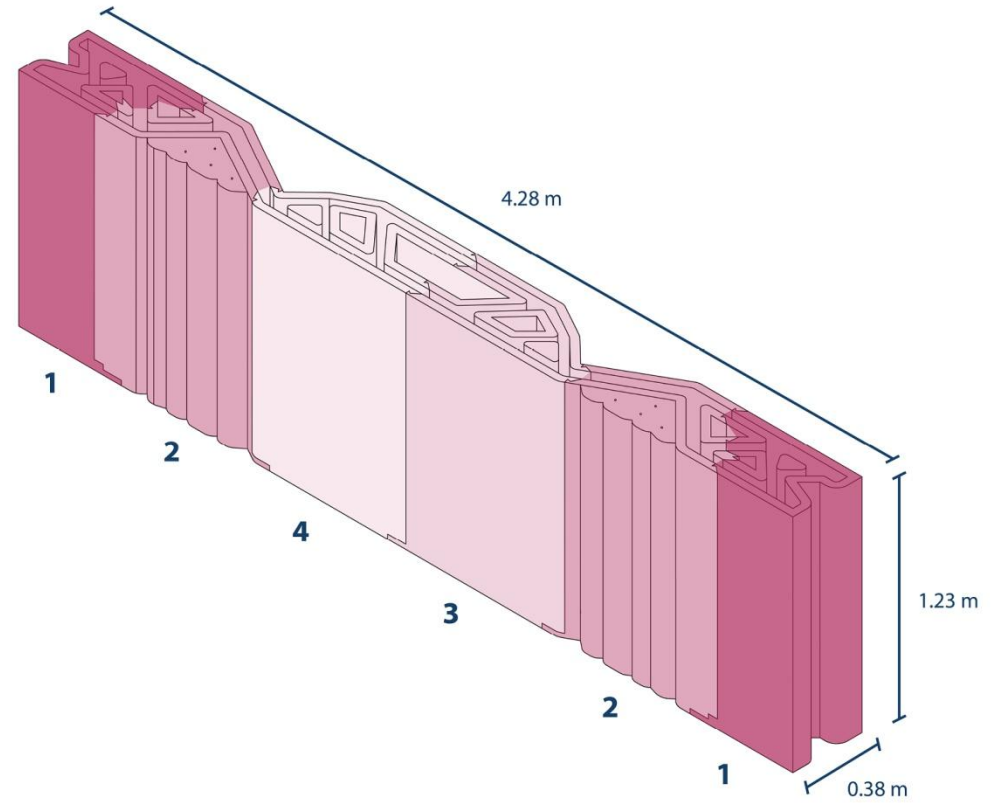
3d printed sand



Damen, W. (2019). Topologically Optimised Cast Glass Grid Shell Nodes

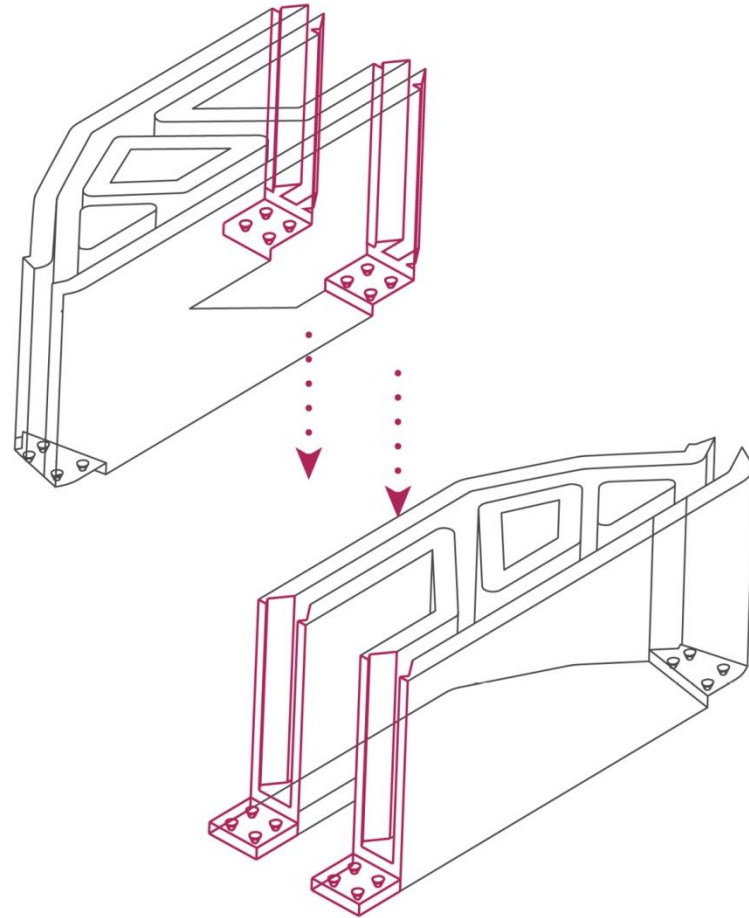


Maximum mould size

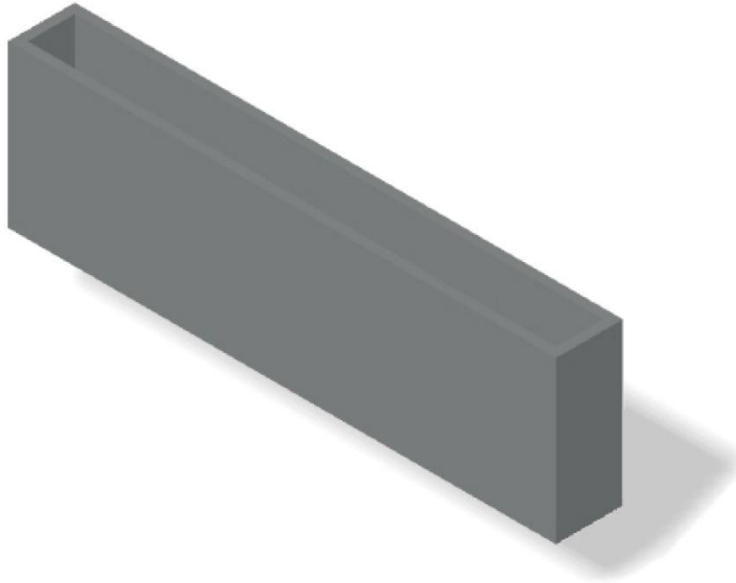


Mould division

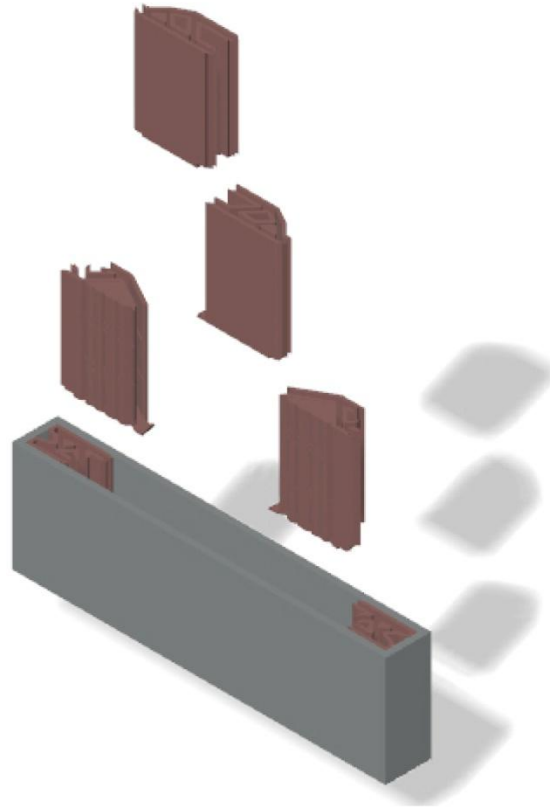




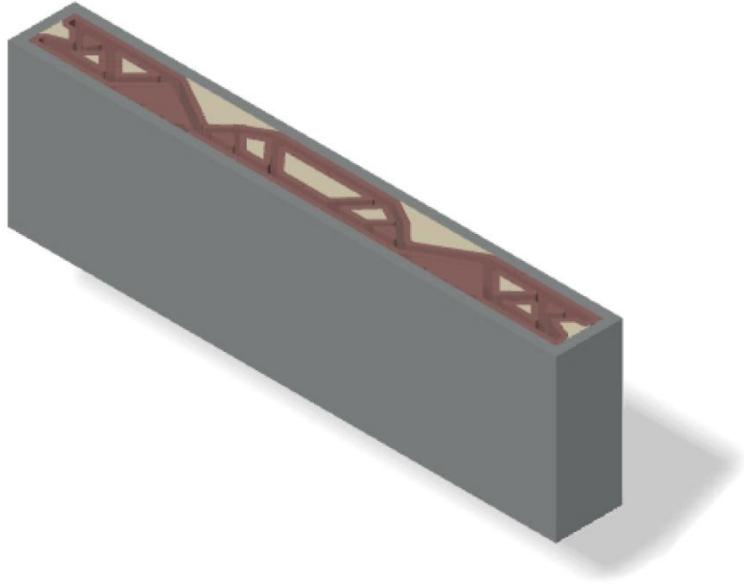
Concrete mould base



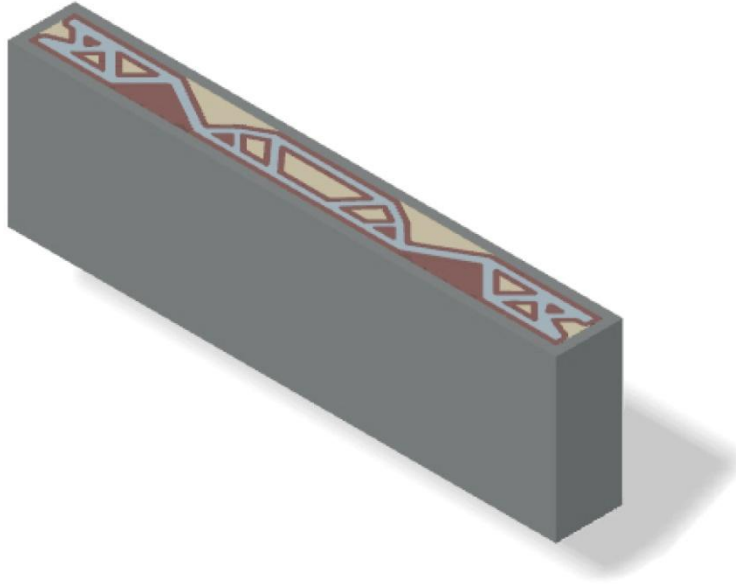
Placement of the
3d printed sand pieces



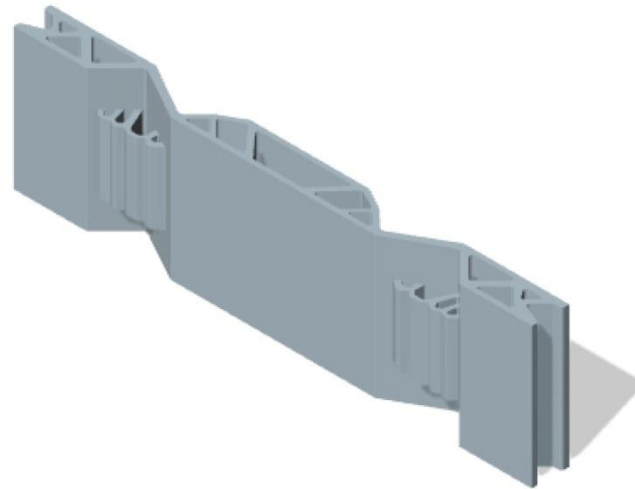
Infill with sand



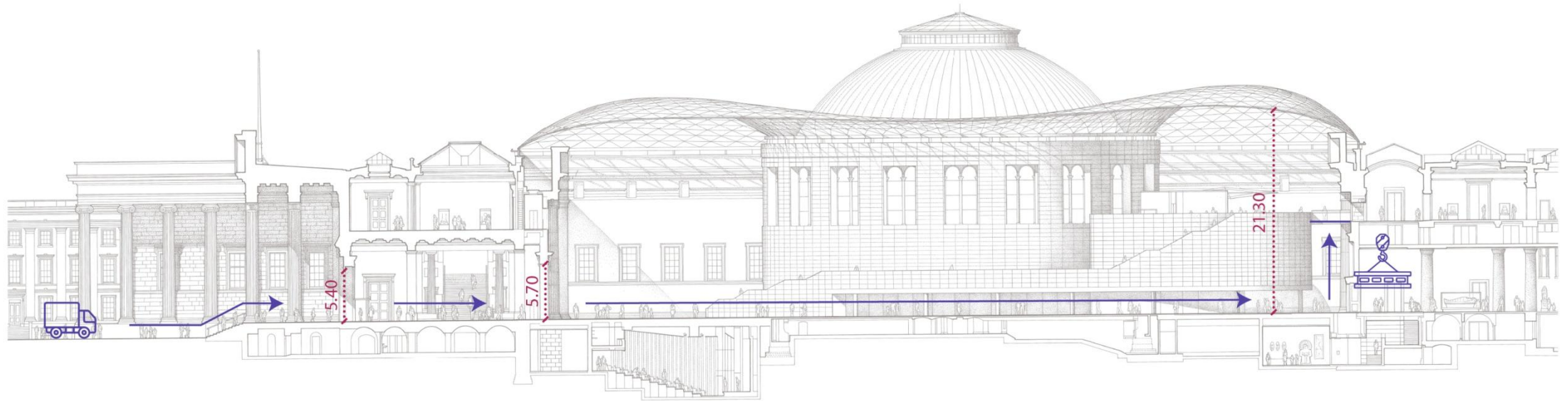
Casting with kiln-casting
technique

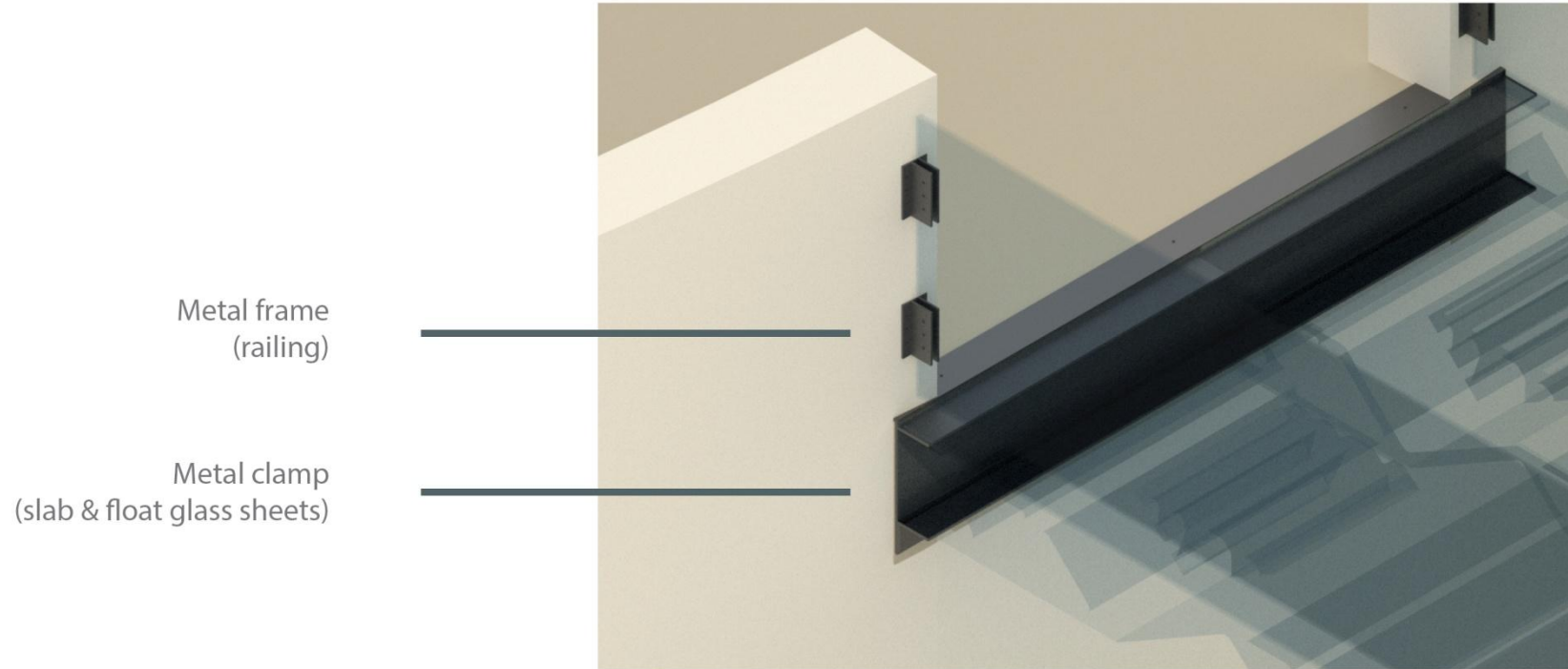


Mould removal
Post-processing

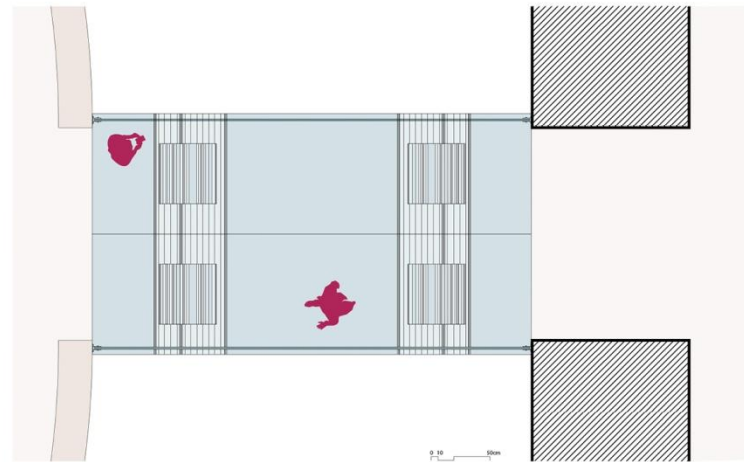
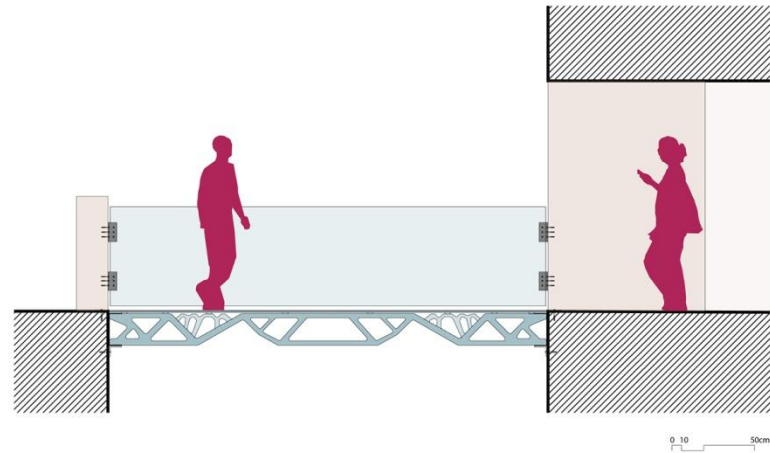


Building integration





Installation IV: Final result



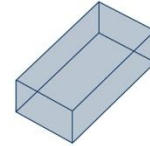
Reflection

Annealing time reduction



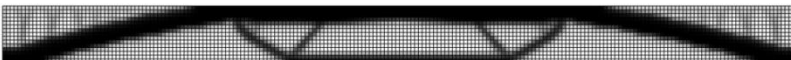
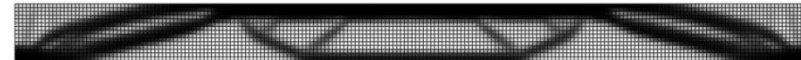
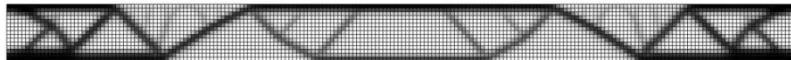
80%

Volume reduction



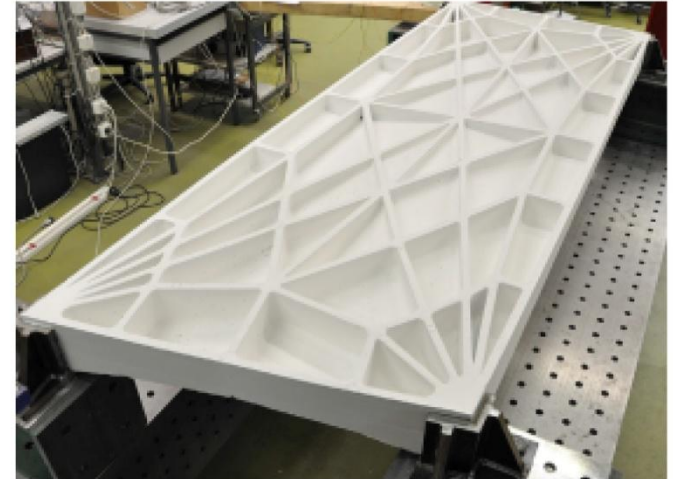
70%

Design exploration

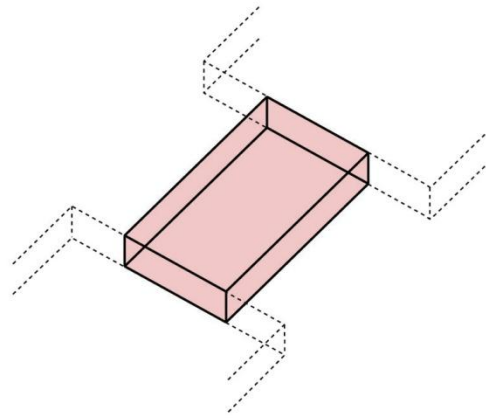




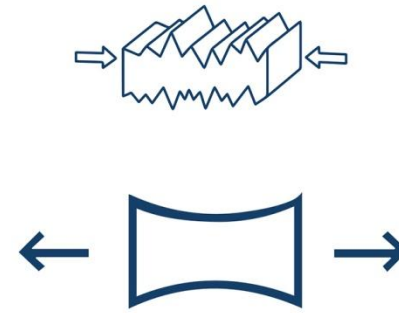
Unreinforced concrete



3d printed sand



3-dimensional code



Testing of structural performance

