

Kinetic Thin Glass Façade

A study on the feasibility of a water- and airtight kinetic façade with a bending-active thin glass element

Özhan Topçu | 4510674 | P5

Context

- Transparency in buildings is an increasing trend



Hiroshi Senju Museum, Karuizawa, Japan



Chanel Amsterdam, Amsterdam, Netherlands



Apple Fifth Avenue, New York City, USA

Context

- Transparency in buildings is an increasing trend
- Rapid development of research and production techniques

"Initially, it was not the architects who took architecture into the modern age, but rather engineers and planners from so called non-artistic disciplines"

Mirko Baum

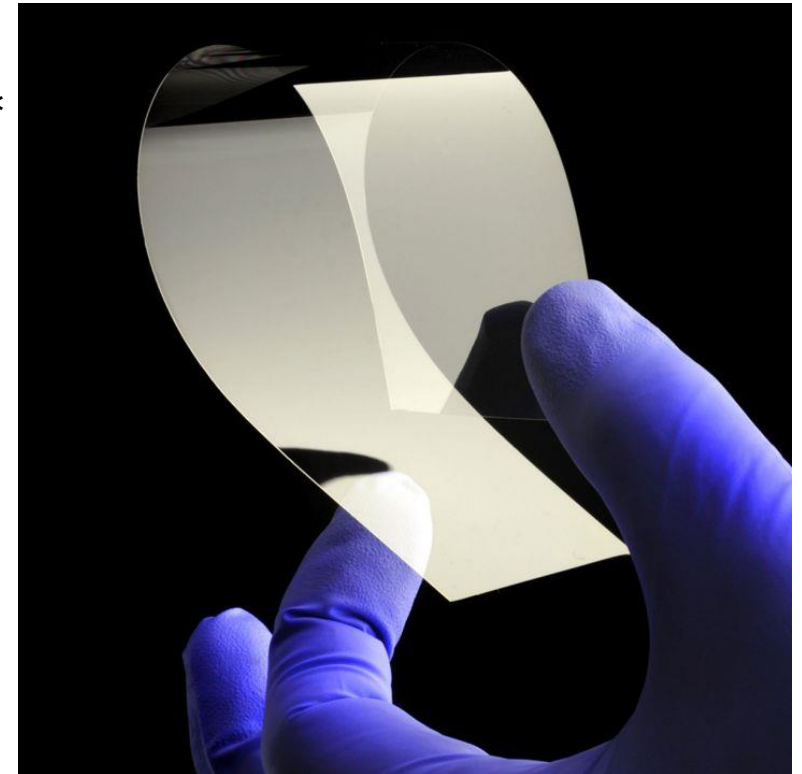
Context

- Transparency in buildings is an increasing trend
- Rapid development of research and production techniques

→ alternative product: chemically strengthened (ultra) thin glass*

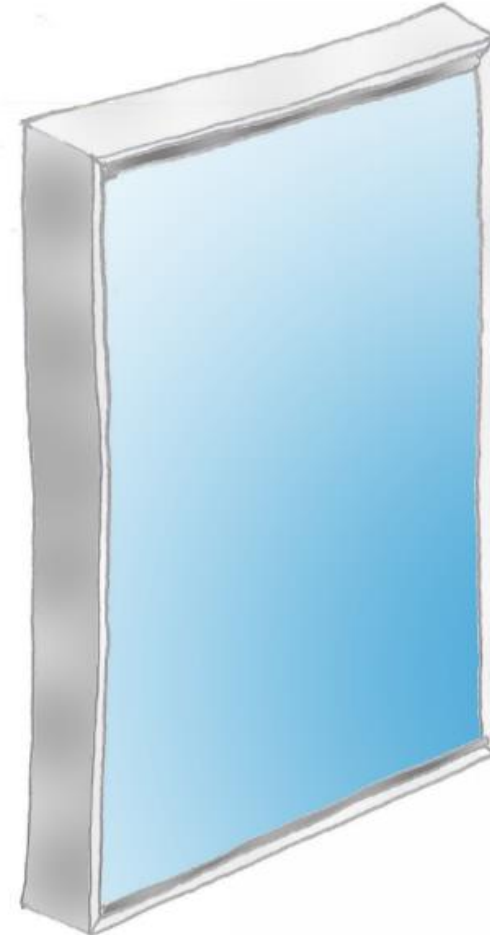
* *Thin glass* → $t < 2 \text{ mm}$

Ultra thin glass → $t < 0.1 \text{ mm}$



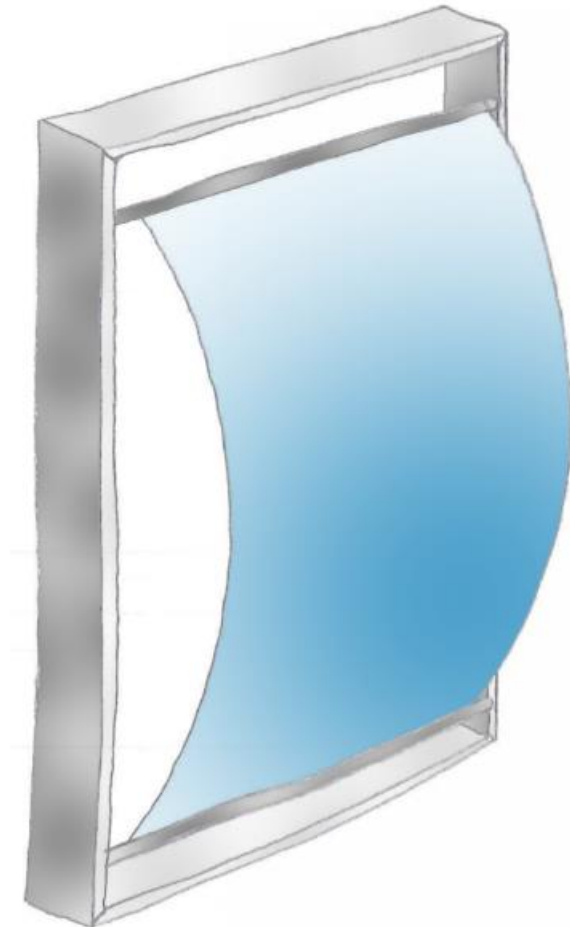
Possible design

bending-active, kinetic thin glass element



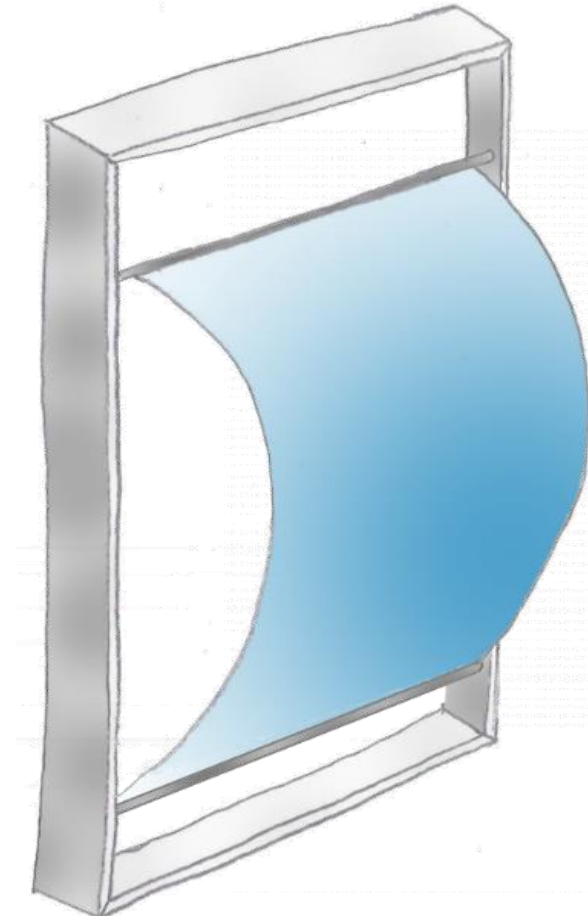
Possible design

bending-active, kinetic thin glass element



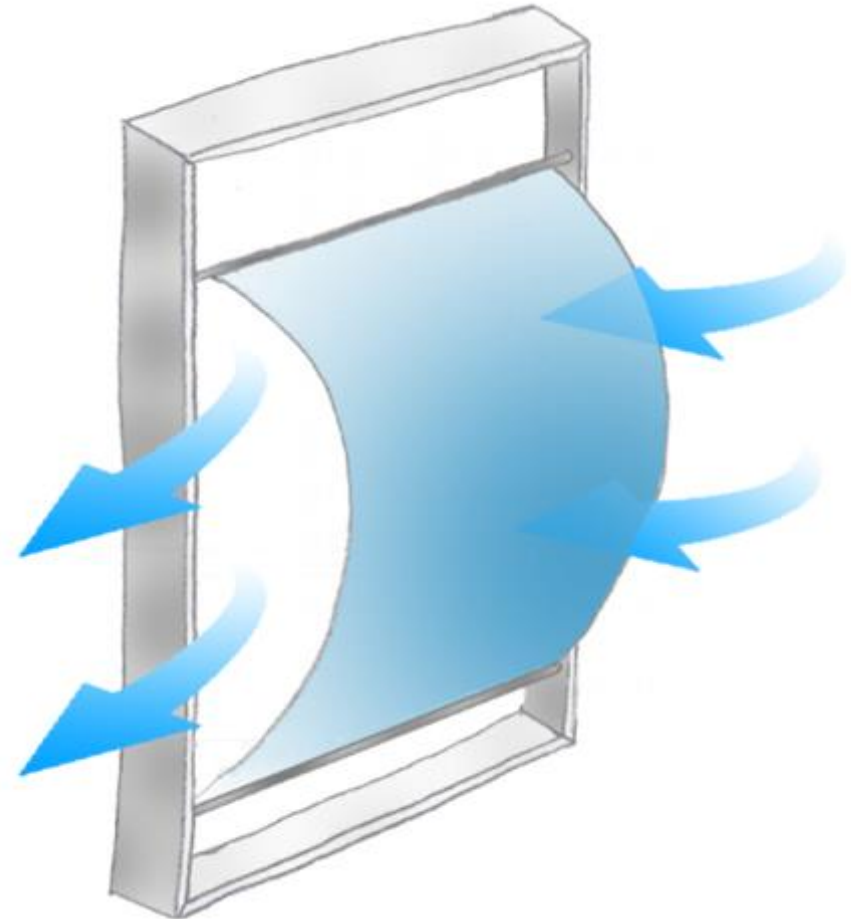
Possible design

bending-active, kinetic thin glass element



Possible design

bending-active, kinetic thin glass element

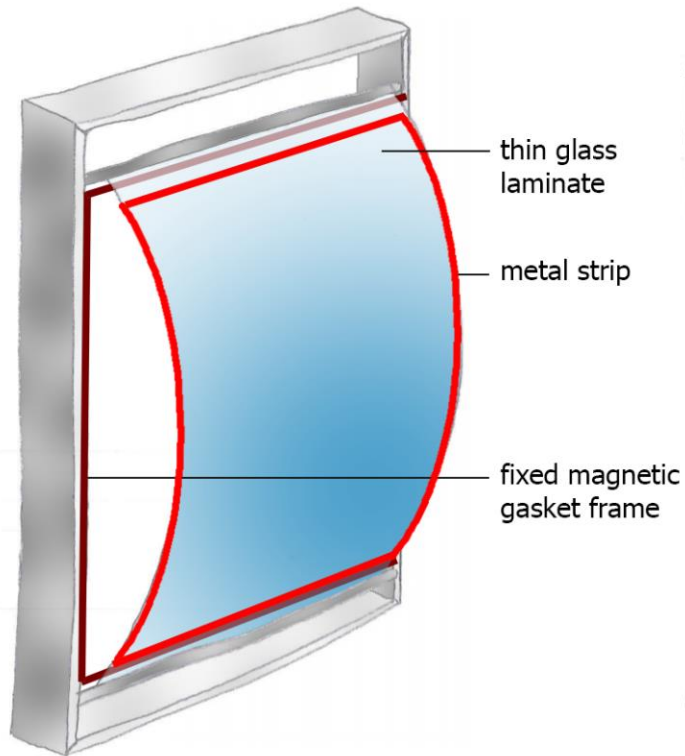


Research Question

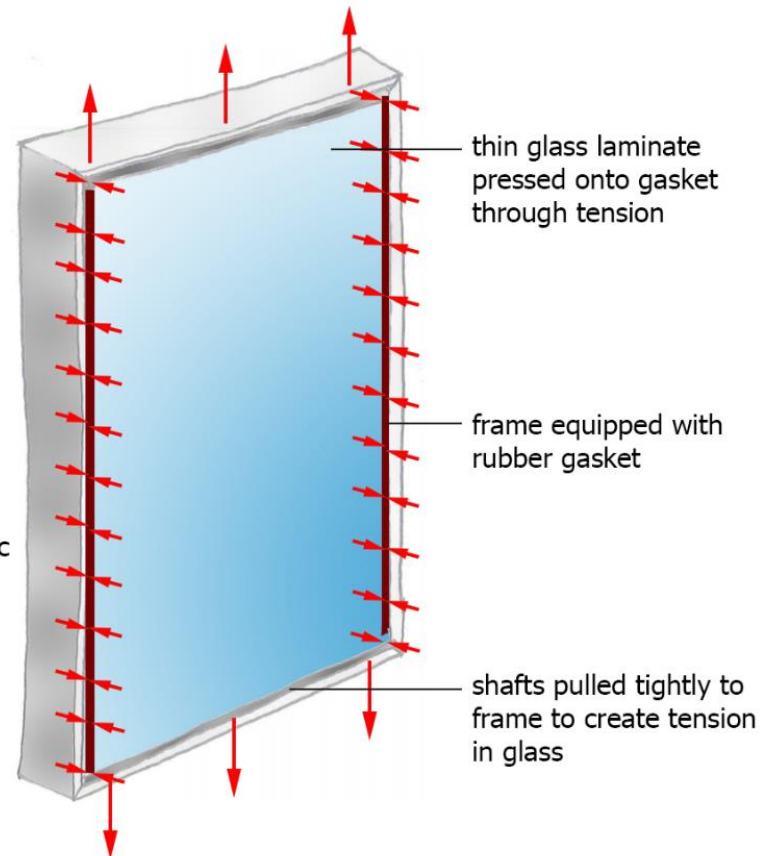
“How can a kinetic façade element featuring a bendable thin glass panel be designed to be water- and airtight in closed condition?”

Design Choice

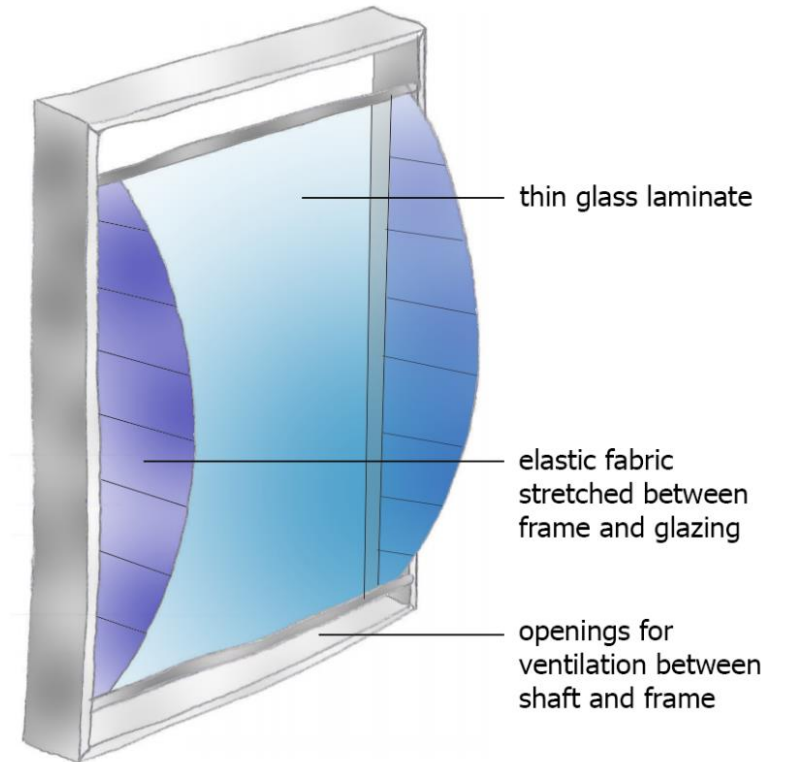
Option 1: Magnetic Force



Option 2: Tensile Force



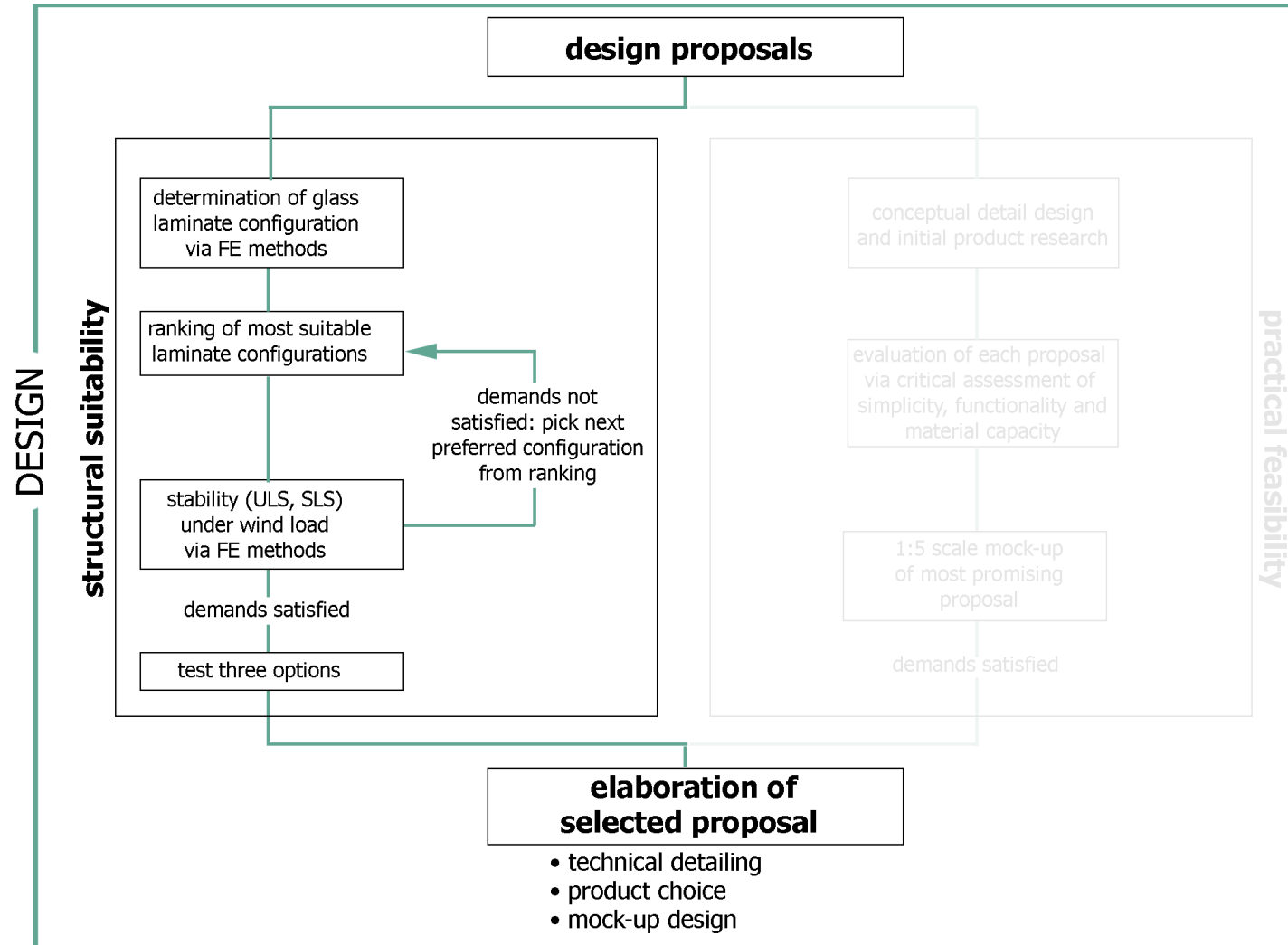
Option 3: Elastic Fabric



Approach and Methodology



Approach and Methodology



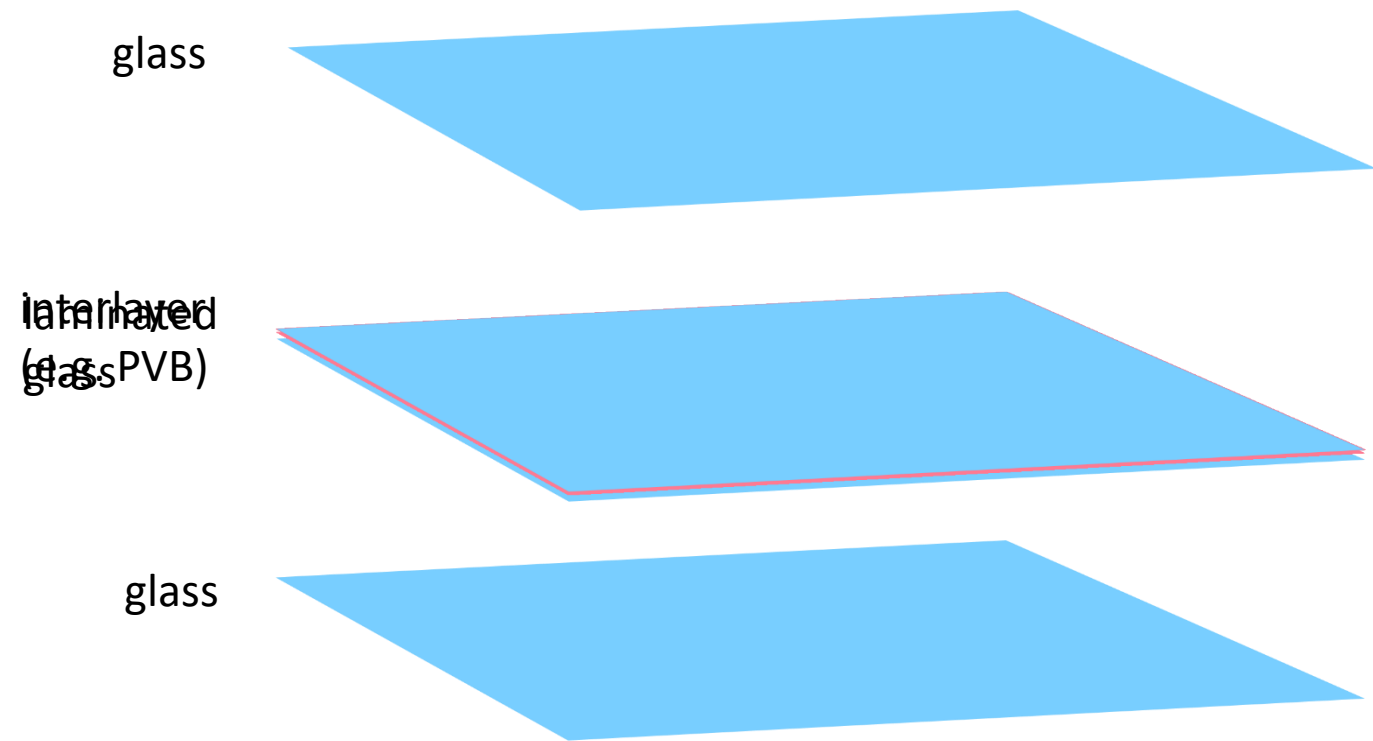
Structural Suitability

Glass Laminate Configuration

Structural Suitability

Glass Laminate Configuration

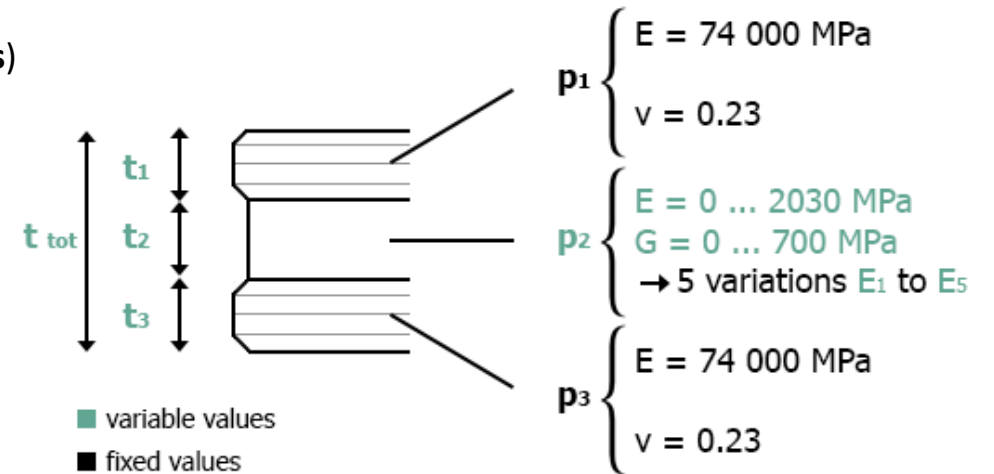
- Safety Regulations
- Adding stiffness
etc.



Structural Suitability

Glass Laminate Configuration

- **smallest radius** that can be achieved by controlled bending (**lowest stress**)
- highest **stability** of the glass laminate against external loads (e.g. wind)
- **minimum** required **force** to achieve the radius



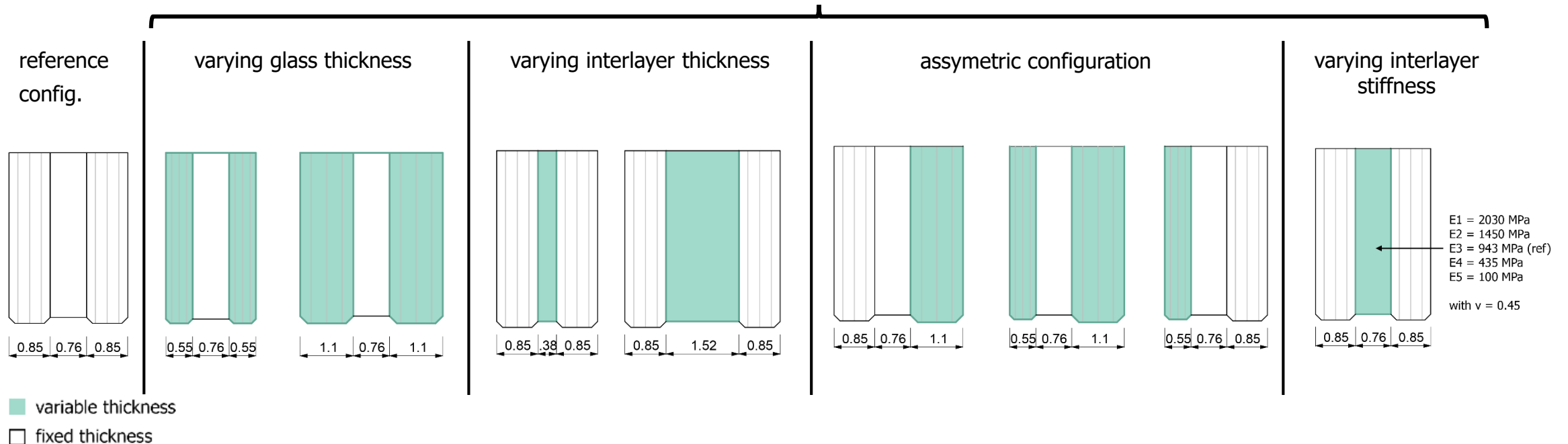
$t_1 / t_3 =$	0.55	0.85	1.1	[mm]
$t_2 =$	0.38	0.76	1.52	[mm]
$P_2 =$	E_1	E_2	E_3	E_4 E_5
			ref	

Structural Suitability

Glass Laminate Configuration

- **smallest radius** that can be achieved by controlled bending (**lowest stress**)
- highest **stability** of the glass laminate against external loads (e.g. wind)
- **minimum** required **force** to achieve the radius

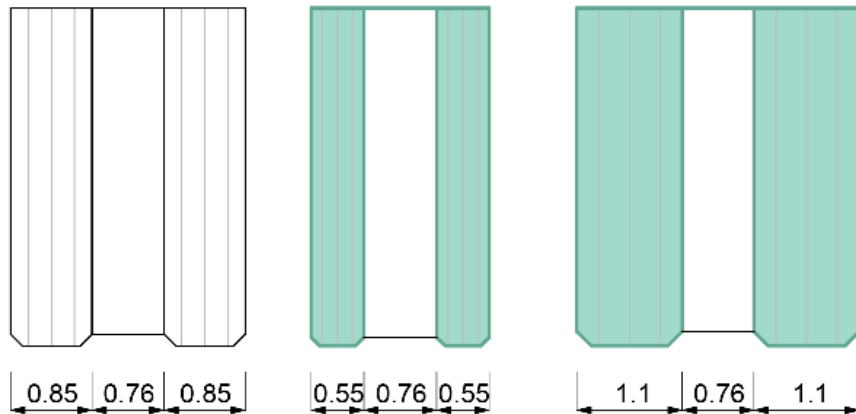
90 possible configurations!



Structural Suitability

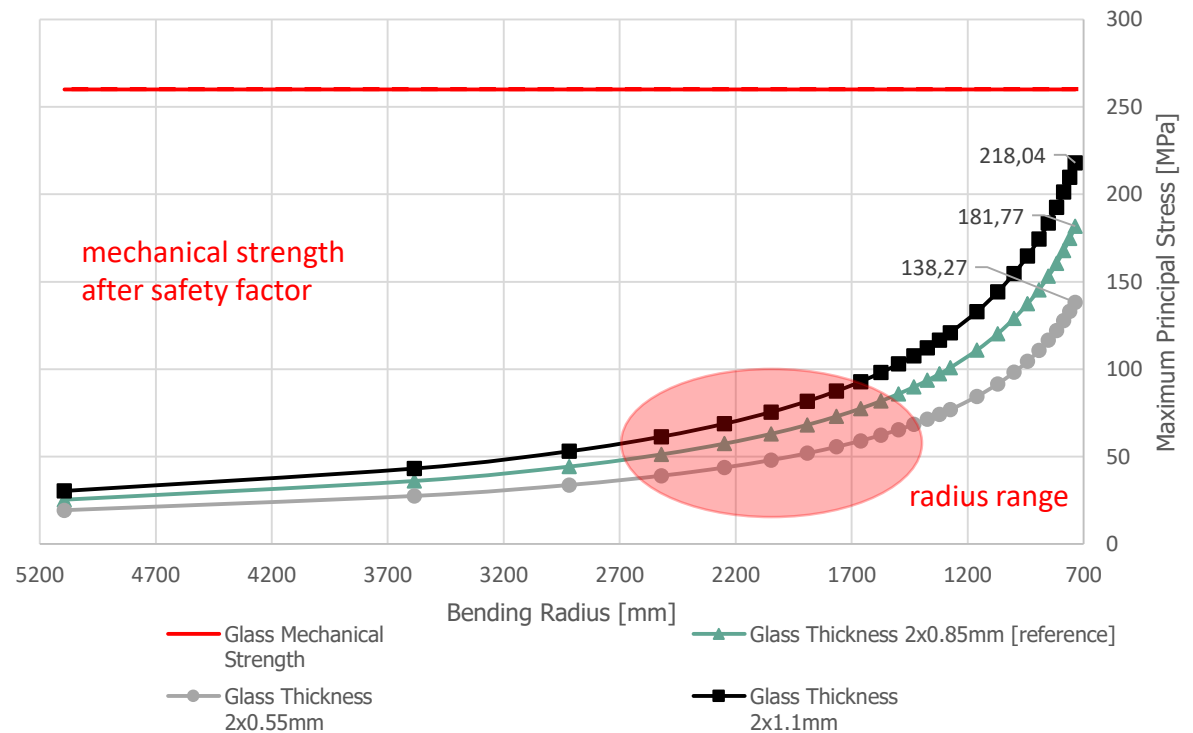
Evaluation of Results: Glass Thickness Effect

The thicker the glass,
the higher the max. principal stresses



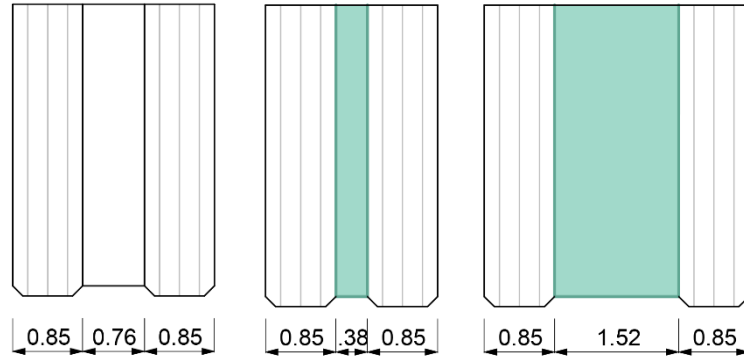
■ variable thickness
□ fixed thickness

Glass-Thickness-Dependent Maximum Principal Stress at Edge of Outer Surface as Function of Bending Radius

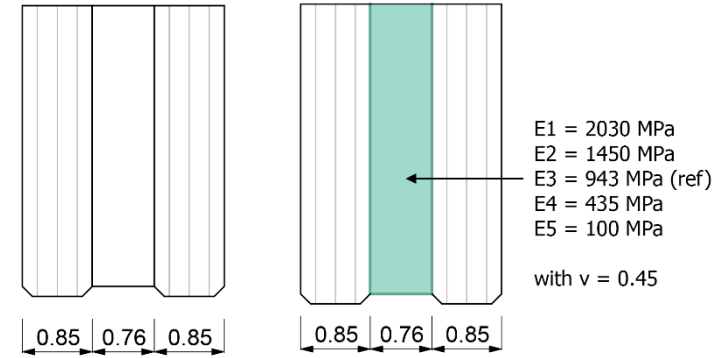


Structural Suitability

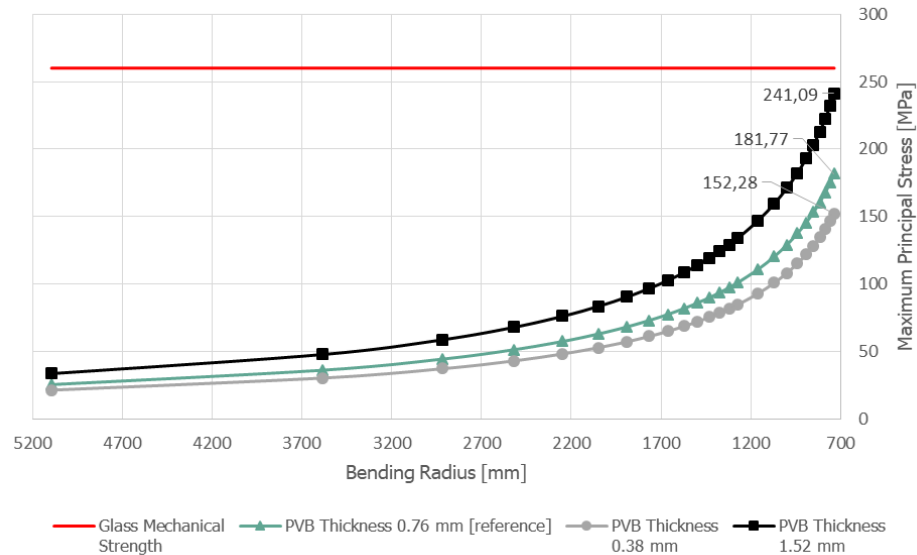
Interlayer Thickness



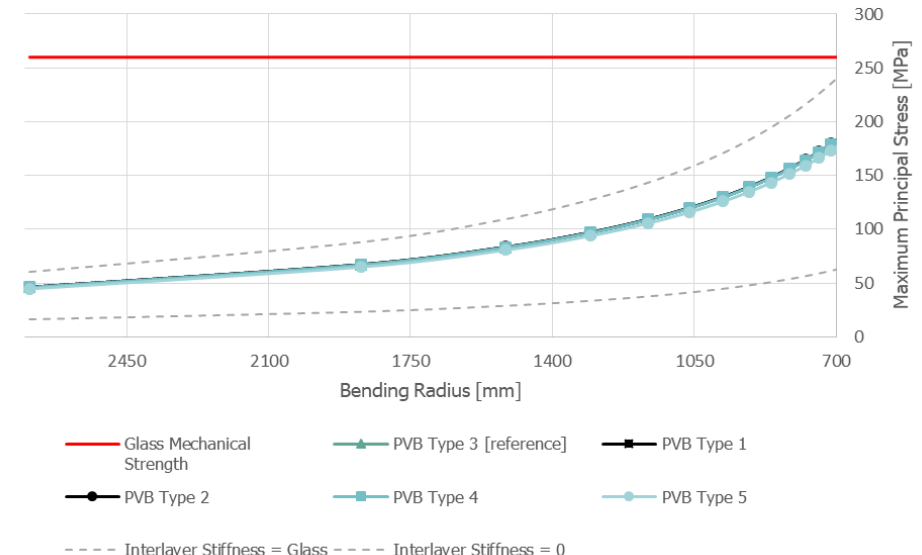
Interlayer Stiffness



PVB-Thickness-Dependent Maximum Principal Stress at Edge of Outer Surface as Function of Bending Radius



PVB-Type-Dependent Maximum Principal Stress as Function of Bending Radius

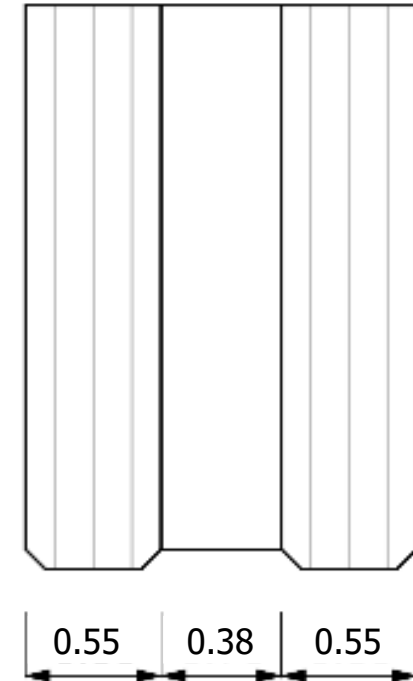


Structural Suitability

Evaluation of Results: Ranking

Choice No.	1st glass thickness t ₁ [mm]	PVB thickness t ₂ [mm]	2nd glass thickness t ₃ [mm]	PVB Type p ₂	final value [%]
1	0.55	0.38	0.55	E5	-43,8
2	0.55	0.38	0.55	E4	-40,6
3	0.55	0.38	0.55	E3	-40,4
4	0.55	0.38	0.55	E2	-40,35
5	0.55	0.38	0.55	E1	-40,33
6	0.85	0.38	0.55	E5	-37,4
7	0.85	0.38	0.55	E4	-34,2
8	0.85	0.38	0.55	E3	-34
9	0.85	0.38	0.55	E2	-33,95
10	0.85	0.38	0.55	E1	-33,93
11	1.1	0.38	0.55	E5	-30,9
12	1.1	0.38	0.55	E4	-27,7
13	0.55	0.76	0.55	E5	-27,6
14	1.1	0.38	0.55	E3	-27,5
15	1.1	0.38	0.55	E2	-27,45
16	1.1	0.38	0.55	E1	-27,43
17	0.55	0.76	0.55	E4	-24,4
18	0.55	0.76	0.55	E3	-24,2
19	0.55	0.76	0.55	E2	-24,15
20	0.55	0.76	0.55	E1	-24,13

preferred



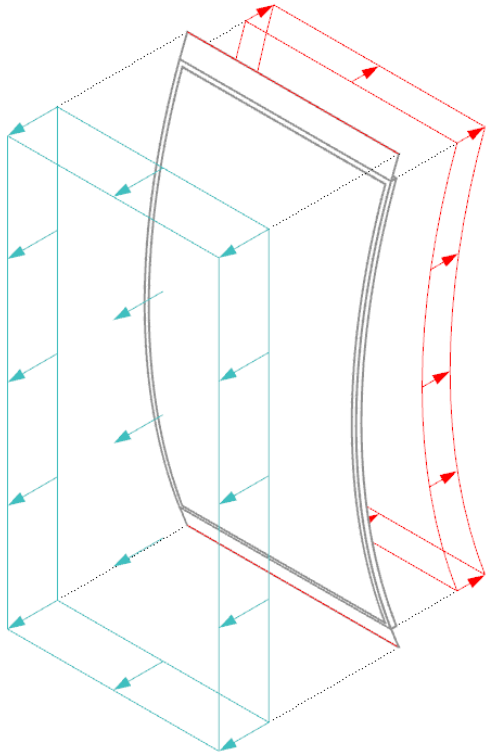
0.55 0.38 0.55

softest interlayer

Structural Suitability

3 Options under Wind Load

Option 1: Magnetic Force



Option 2: Tensile Force
Option 3: Elastic Fabric
Option 4: Elastic Fabric



- wind load
- support reactions

Structural Suitability

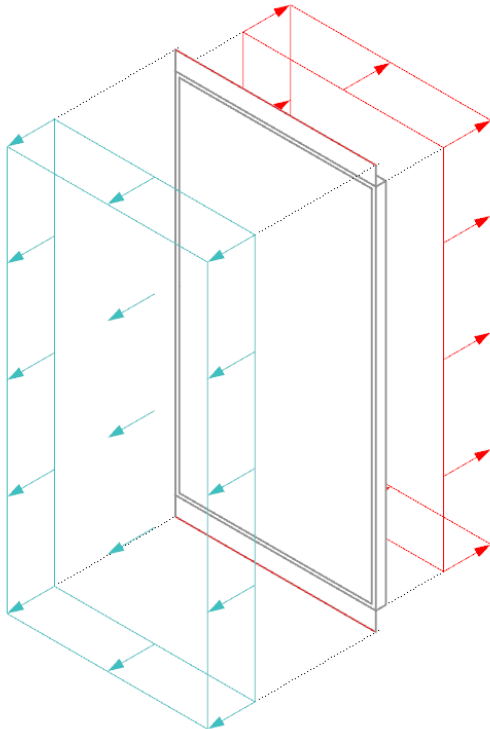
Option 1: Magnetic Force

Method: Wind suction on glass surface supported by magnetic force

Decisive properties:

- Max. deformation under wind load

Flat glass



A: Glass Laminate

Directional Deformation 2

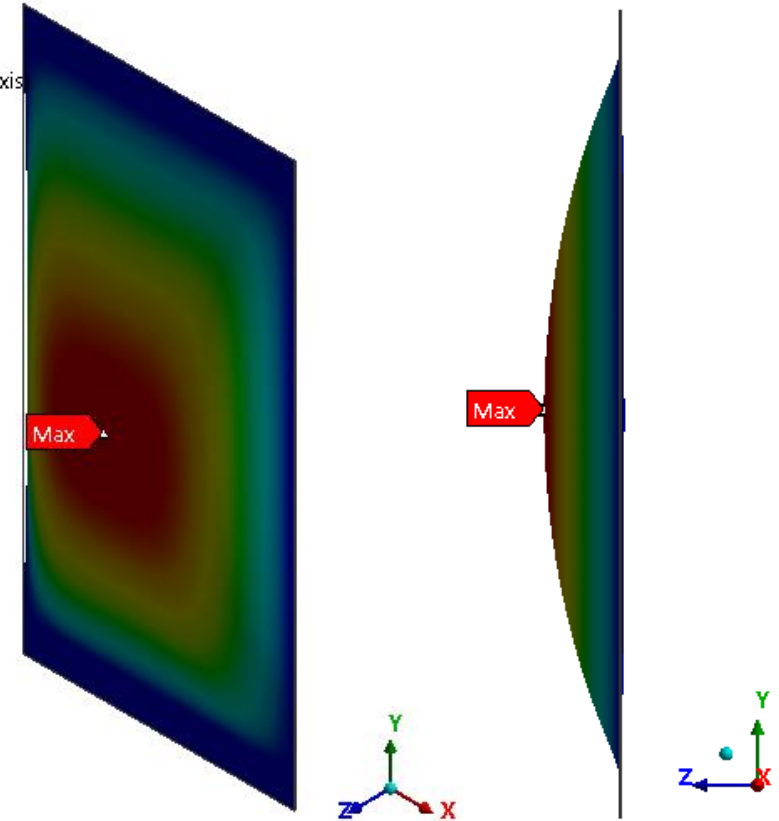
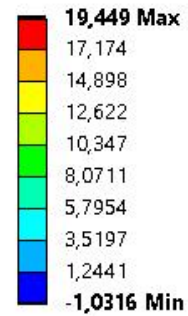
Type: Directional Deformation(Z Axis)

Unit: mm

Global Coordinate System

Time: 5

24.04.2017 15:29



→ max. deformation = 19.5 mm

Structural Suitability

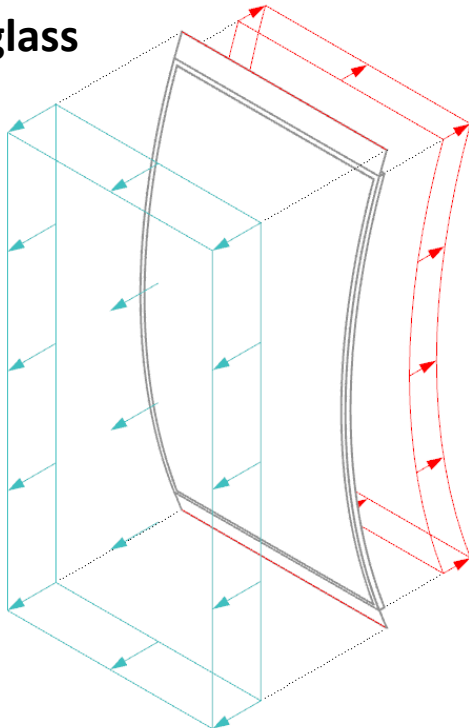
Option 1: Magnetic Force

Method: Wind suction on glass surface supported by magnetic force

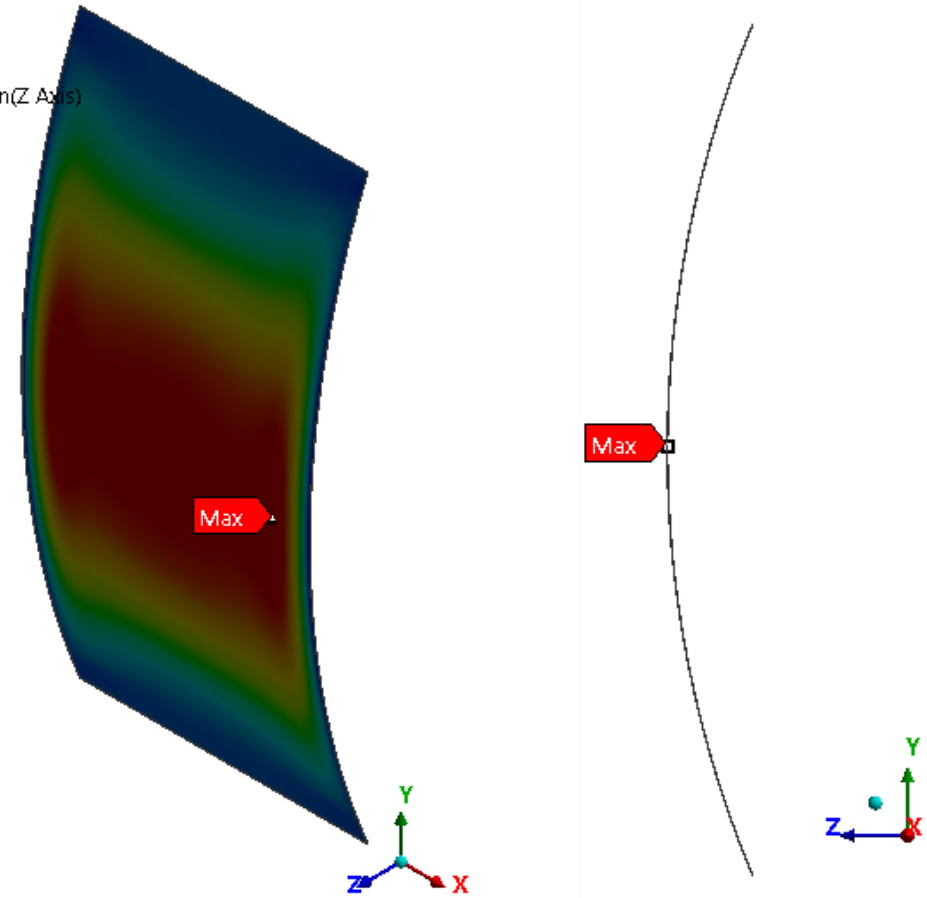
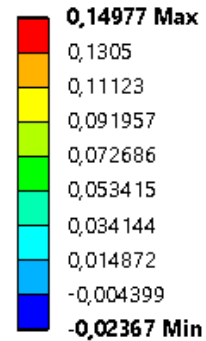
Decisive properties:

- Max. deformation under wind load

Curved glass



A: Glass Laminate
Directional Deformation 2
Type: Directional Deformation(Z Axis)
Unit: mm
Global Coordinate System
Time: 5
24.04.2017 16:03

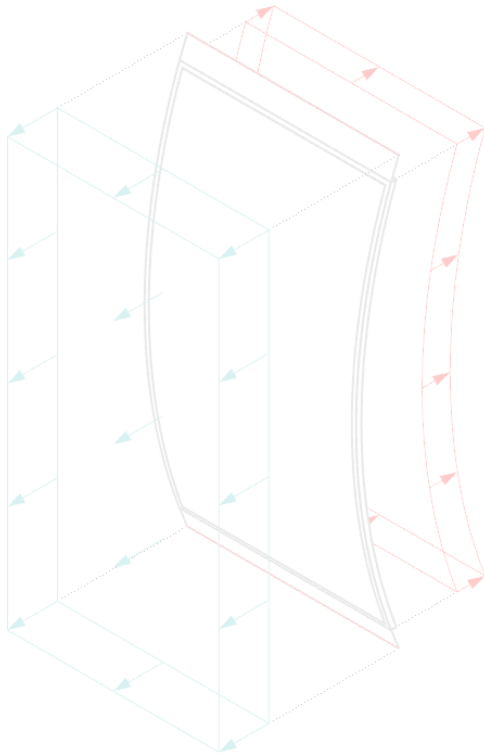


→ max. deformation < 1 mm (!)

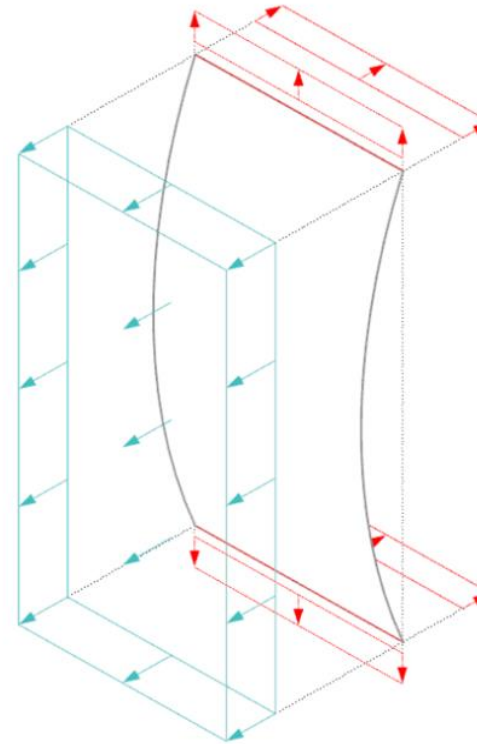
Structural Suitability

3 Options under Wind Load

Option 1: Magnetic Force



Option 2 + 3: Tensile Force / Elastic Fabric



- wind load
- support reactions

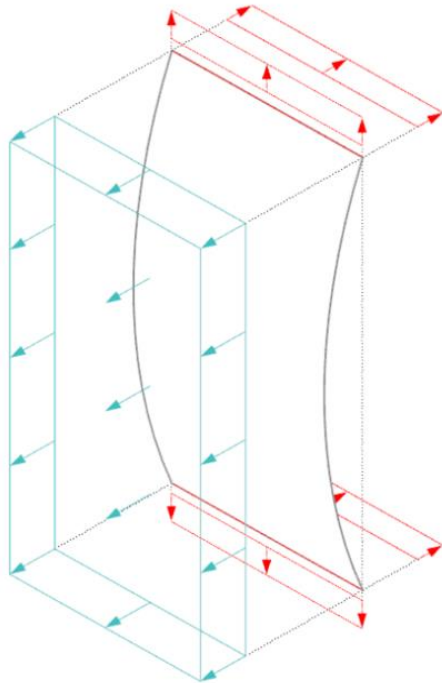
Structural Suitability

Option 2+3

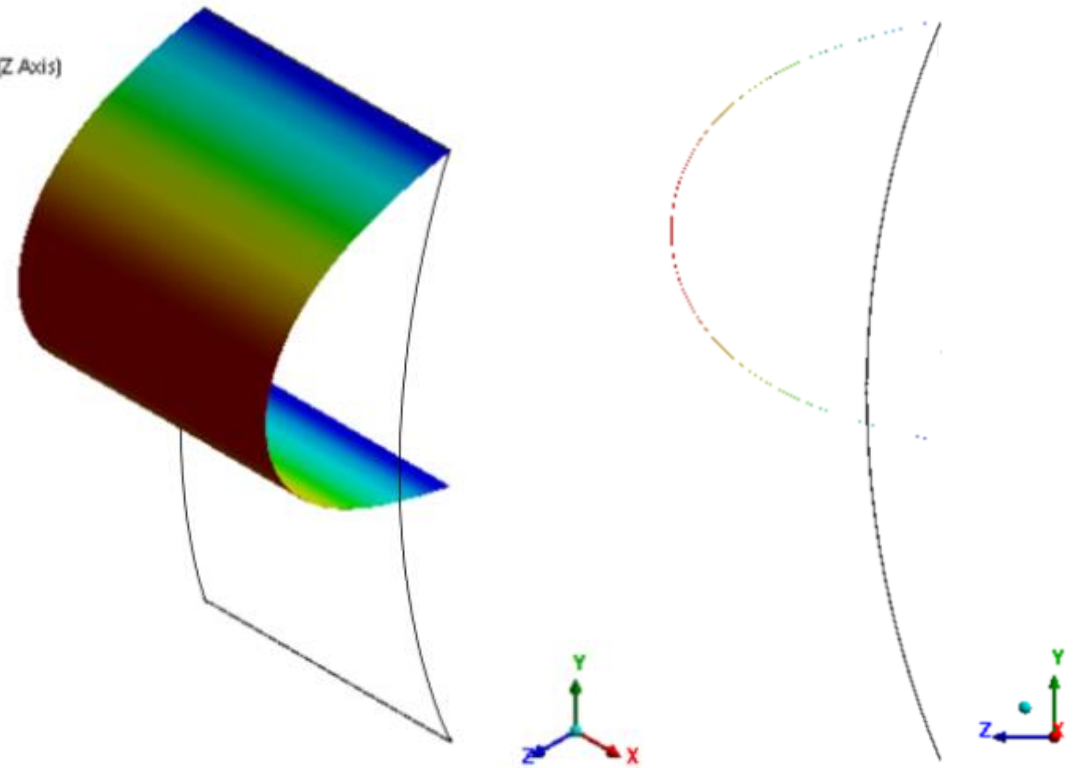
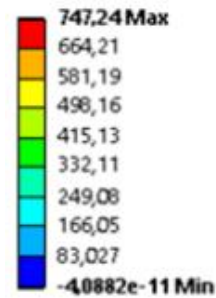
Method: Wind suction on curved glass supported by two shafts

Decisive properties:

- Max. deformation under wind load



A: Glass Laminate
Directional Deformation 2
Type: Directional Deformation(Z Axis)
Unit: mm
Global Coordinate System
Time: 5
24.04.2017 17:45

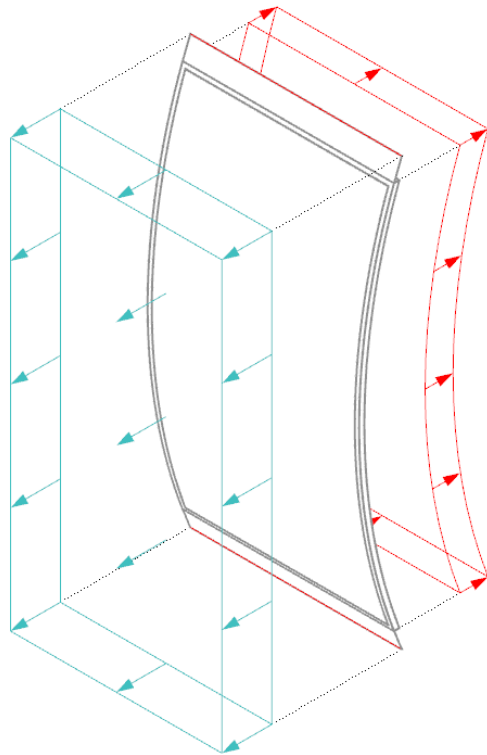


→ tensile force of **2550 N** required to keep stable!

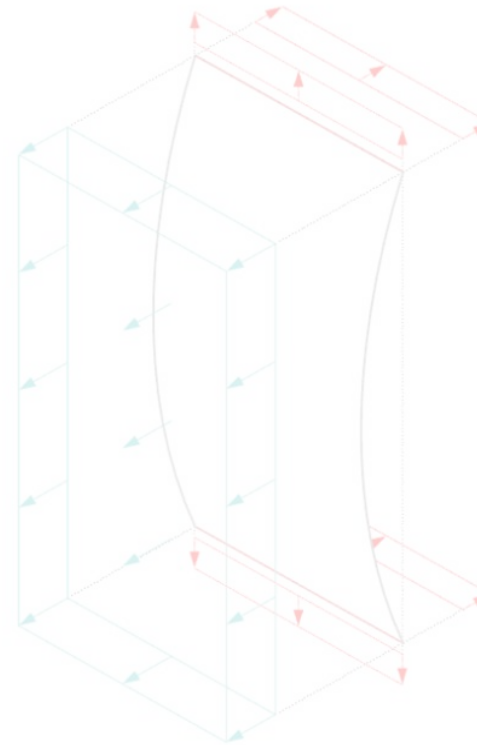
Structural Suitability

3 Options under Wind Load

Option 1: Magnetic Force



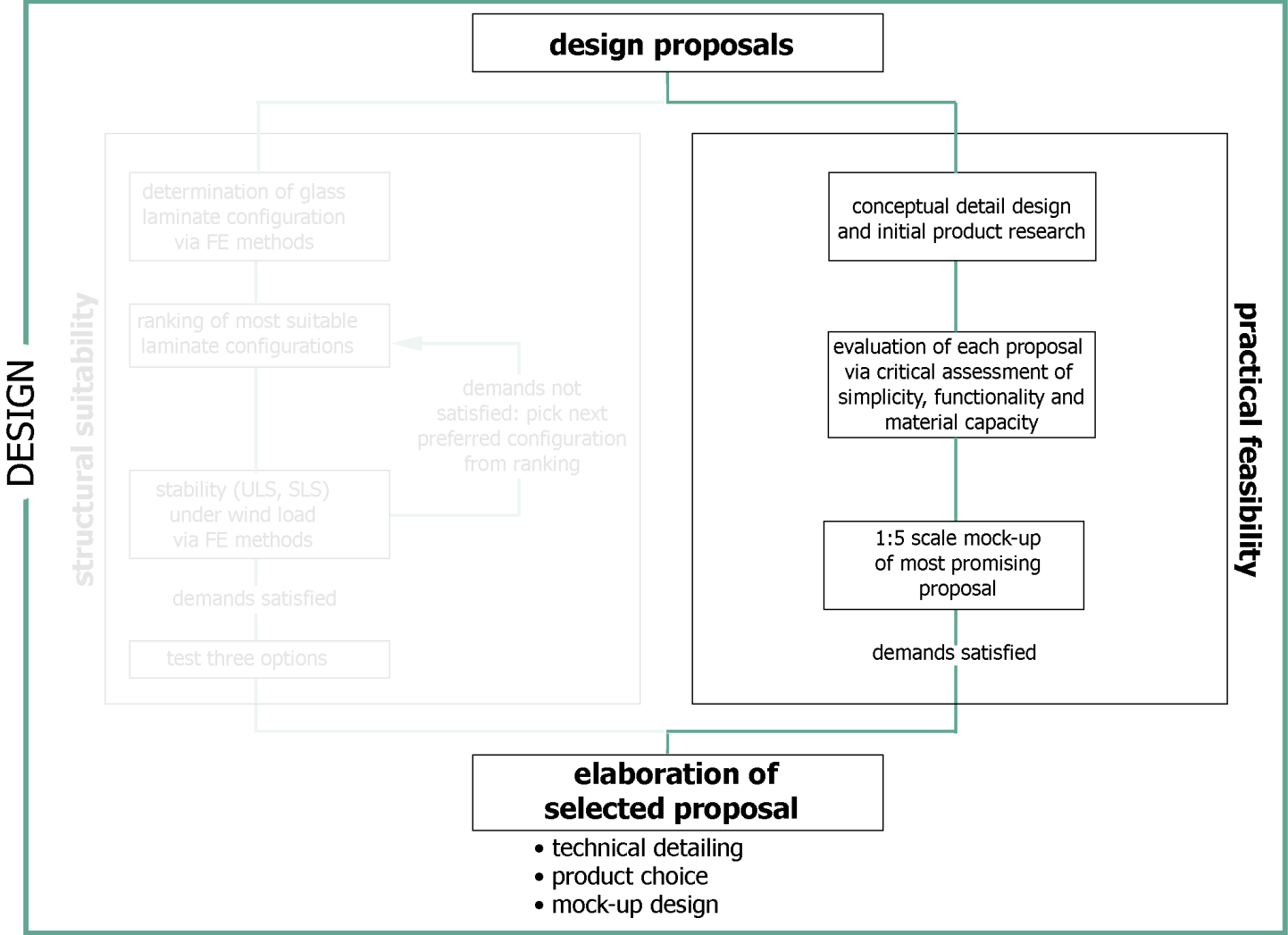
Option 2 + 3: Tensile Force / Elastic Fabric



■ wind load

■ support reactions

Approach and Methodology



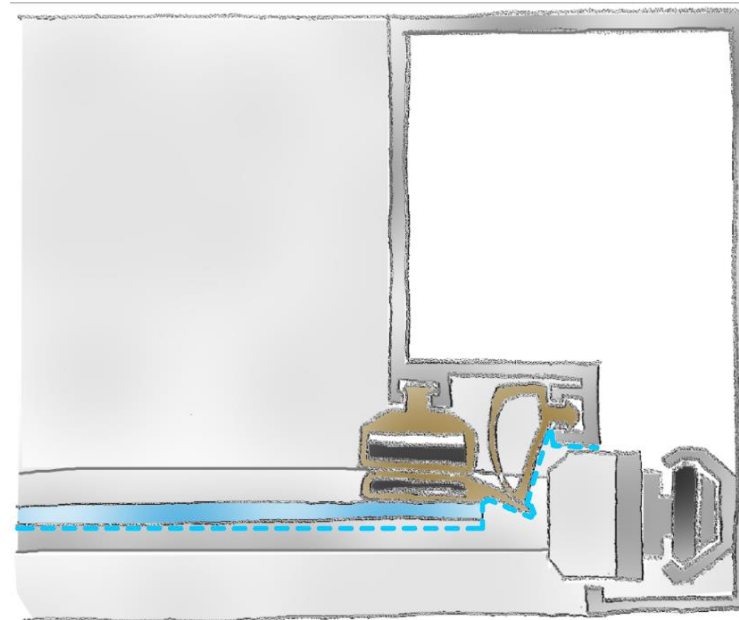
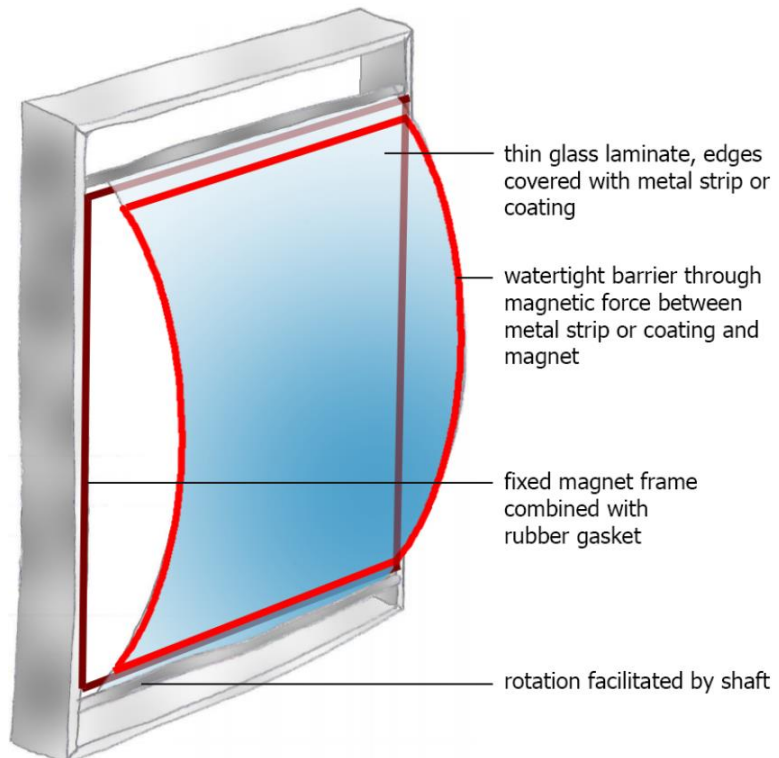
Practical Feasibility

Option 1: Magnet

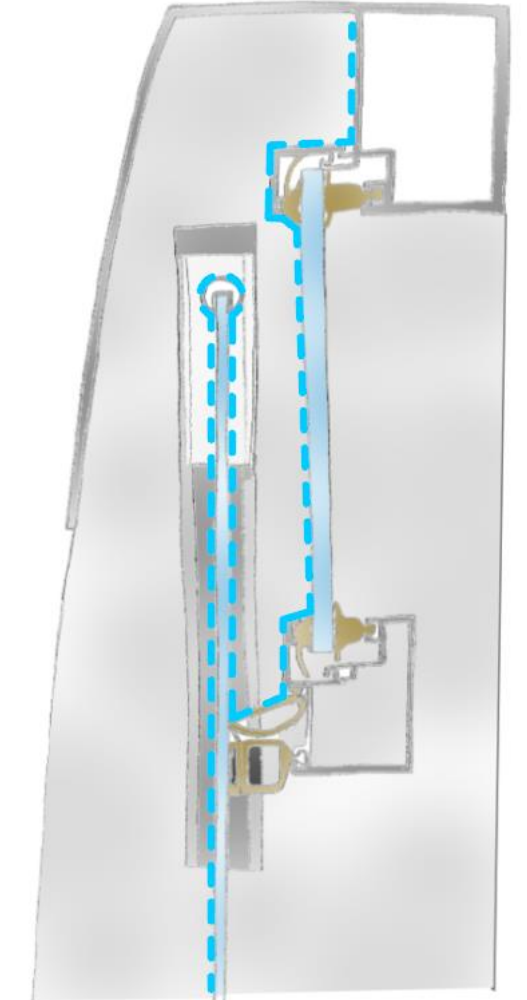
Practical Feasibility

Option 1: Magnet

Water- airtightness possibly achievable with elaboration of conceptual details



lines of defence



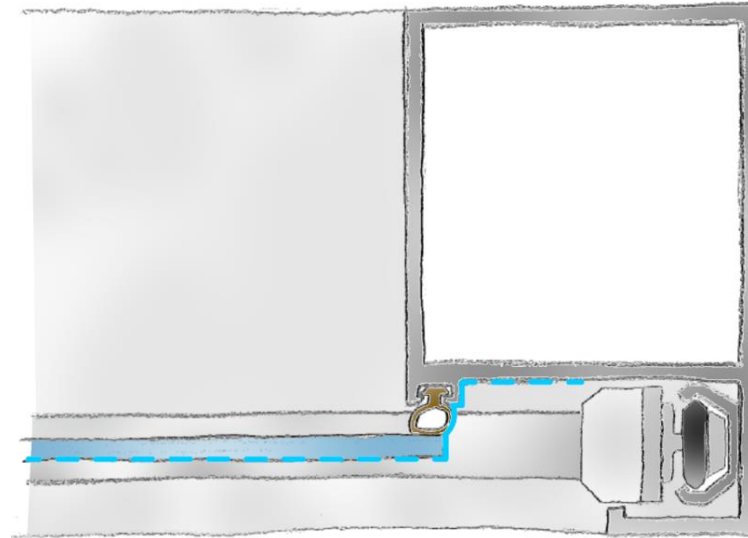
Practical Feasibility

Option 2: Tension

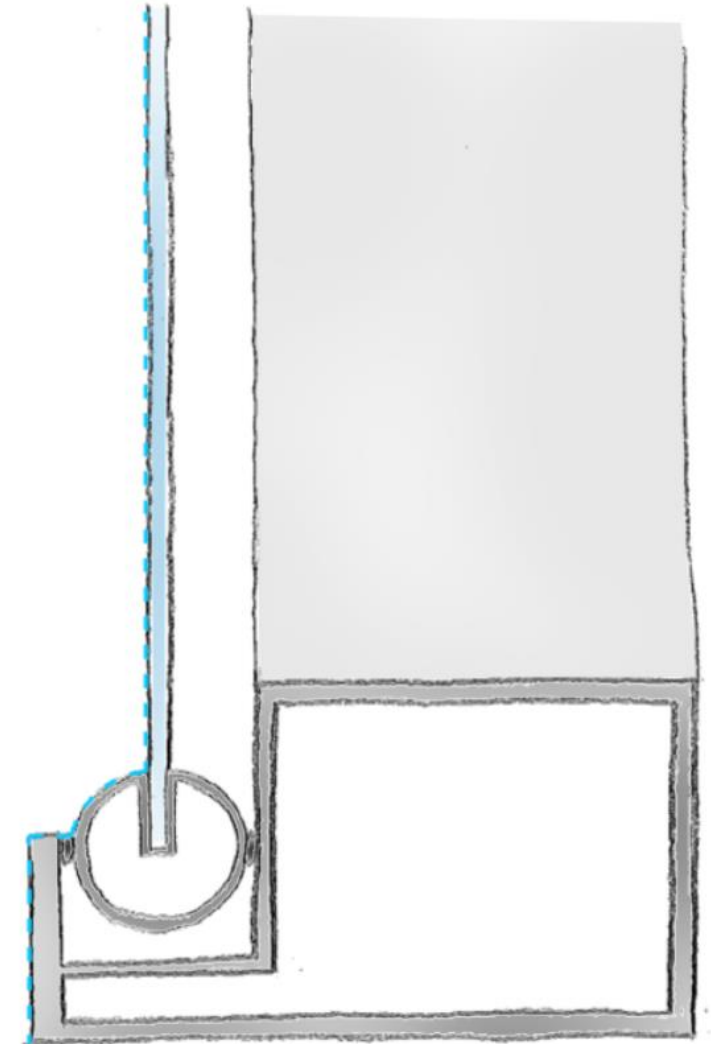
Practical Feasibility

Option 2: Tension

- gaps in corner joints
→ would require similar solution
as magnet



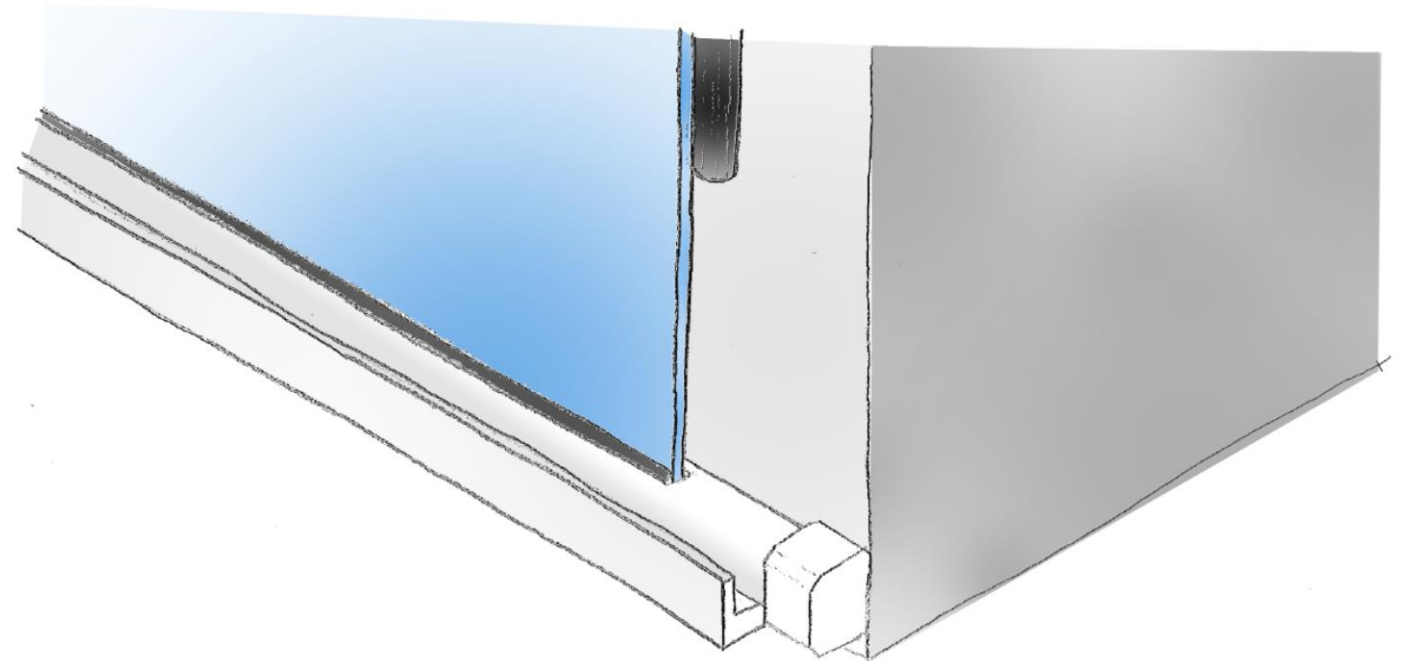
lines of defence



Practical Feasibility

Option 2: Tension

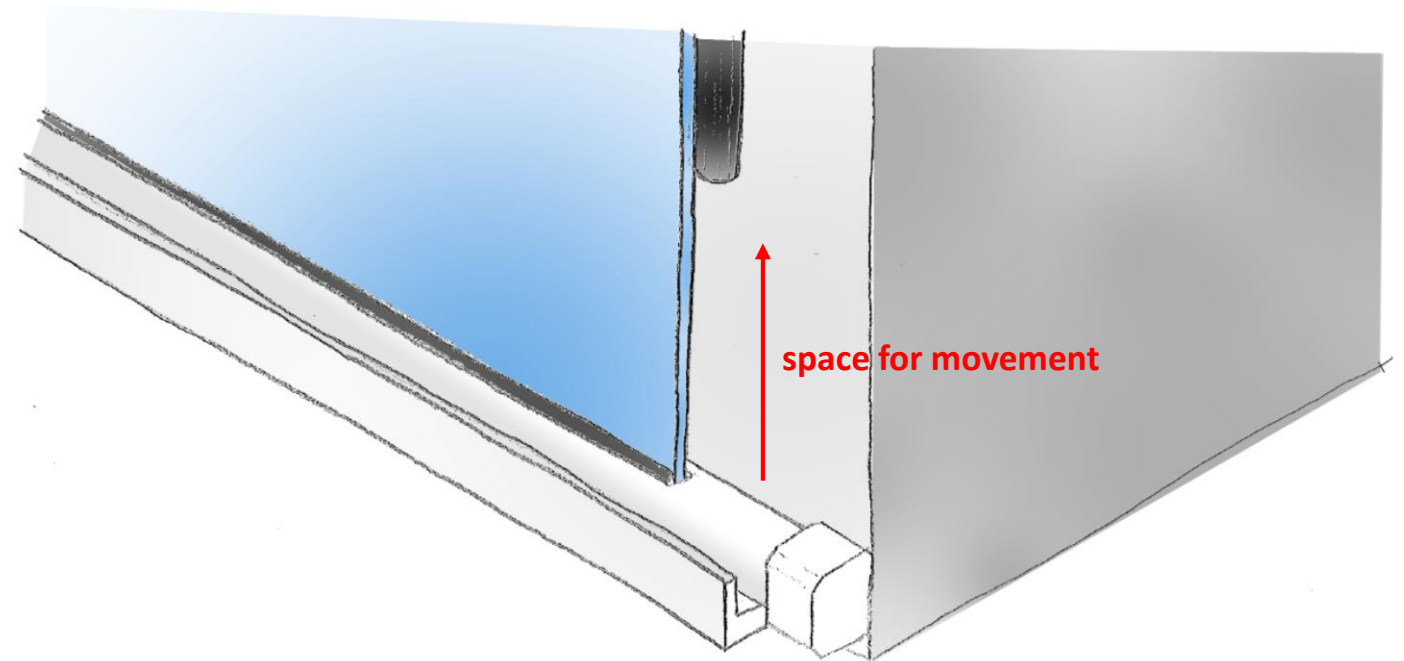
- gaps in corner joints
→ would require similar solution
as magnet



Practical Feasibility

Option 2: Tension

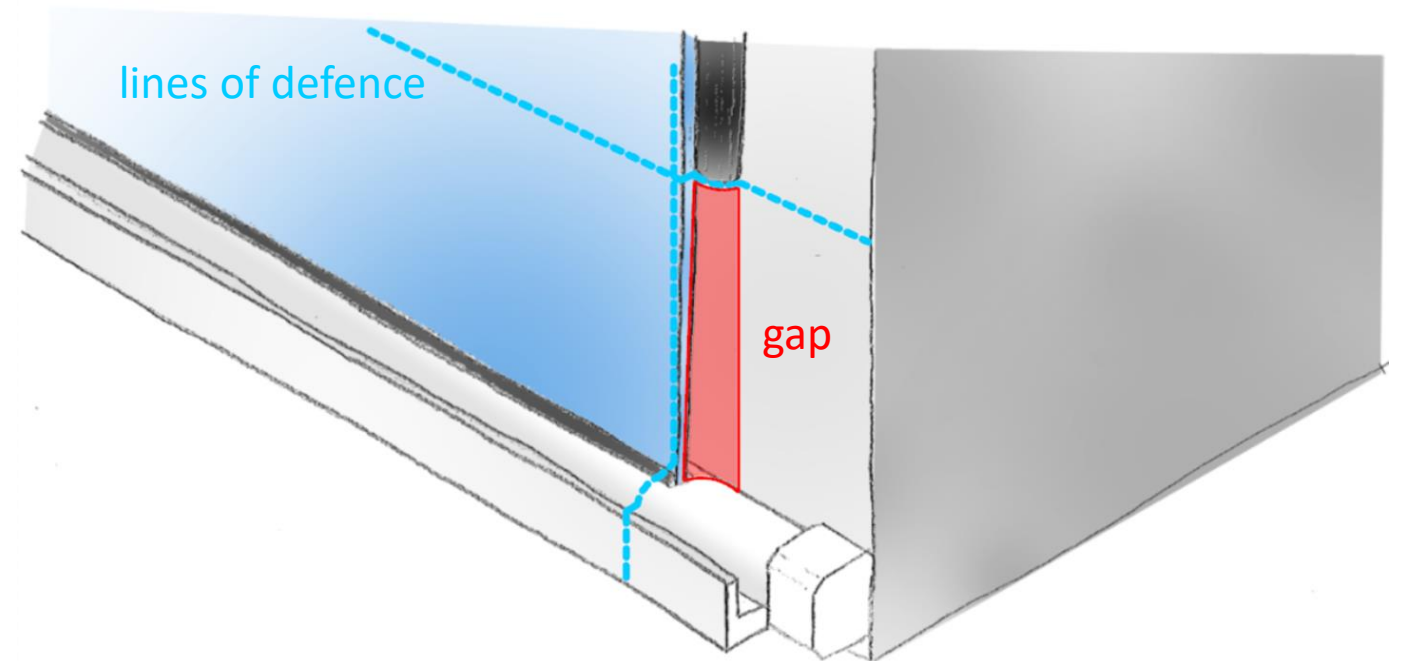
- gaps in corner joints
→ would require similar solution
as magnet



Practical Feasibility

Option 2: Tension

- gaps in corner joints
→ would require similar solution
as magnet



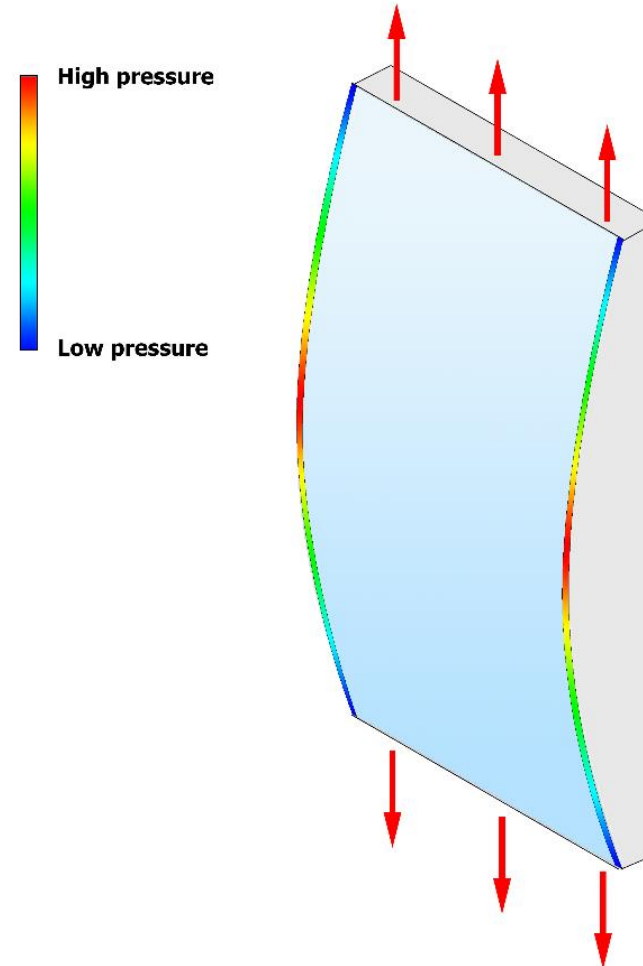
Practical Feasibility

Option 2: Tension

- gaps in corner joints
→ would require similar solution
as magnet

Further concerns:

- Large force required against wind load
- Pressure not likely to be equally distributed

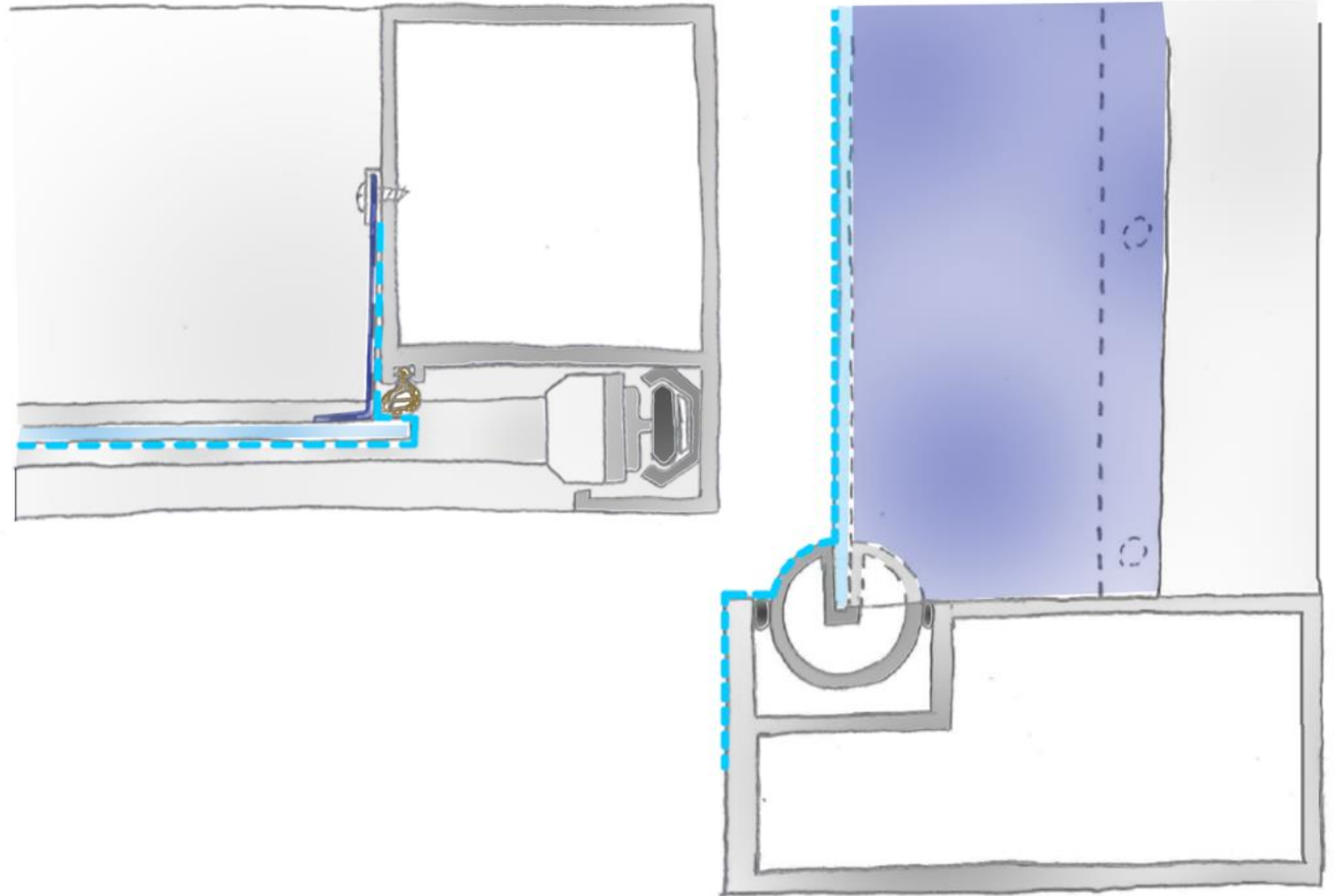


Option 3: Elastic Fabric

Practical Feasibility

Option 3: Elastic Fabric

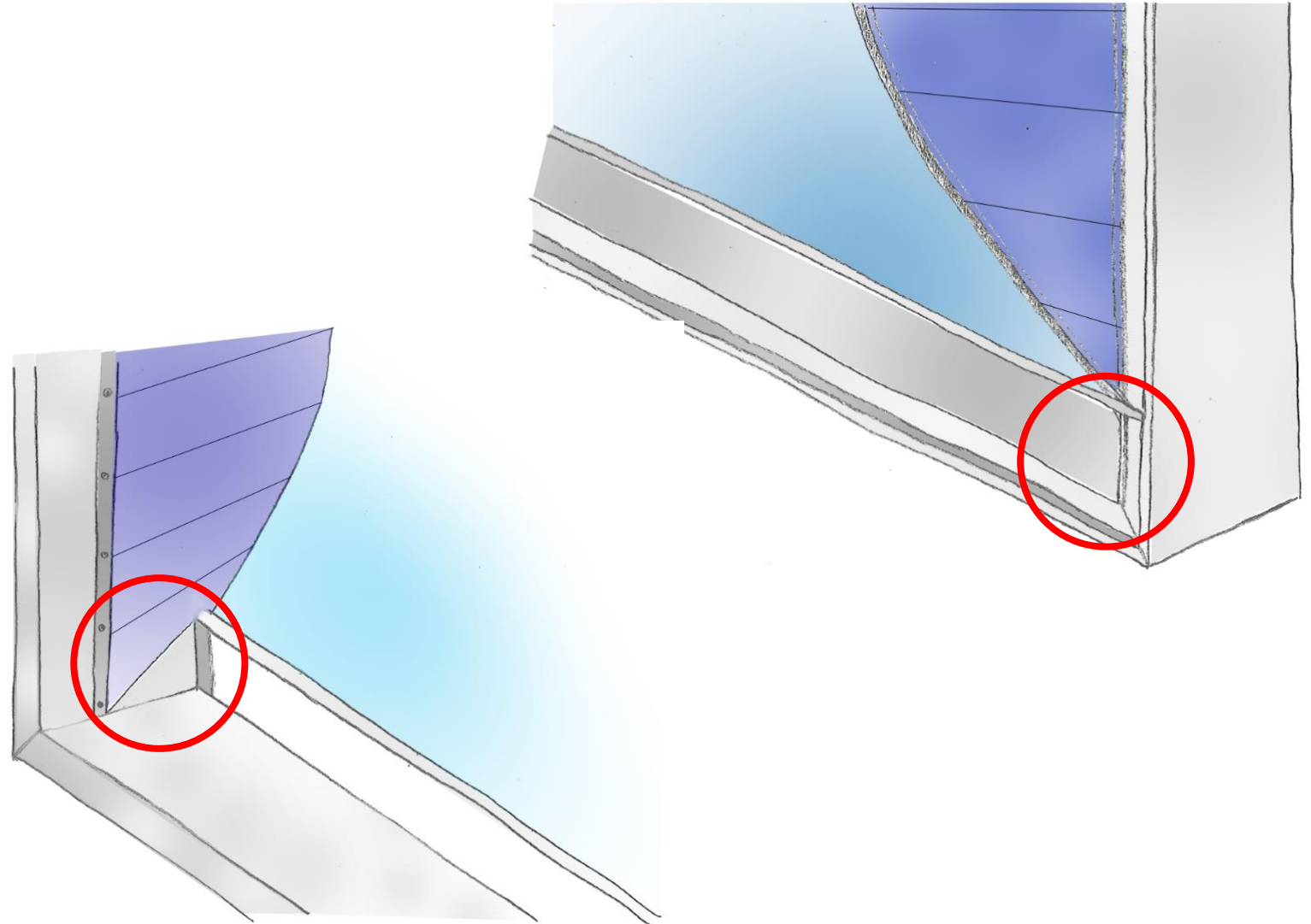
- Leakage at corner joint



Practical Feasibility

Option 3: Elastic Fabric

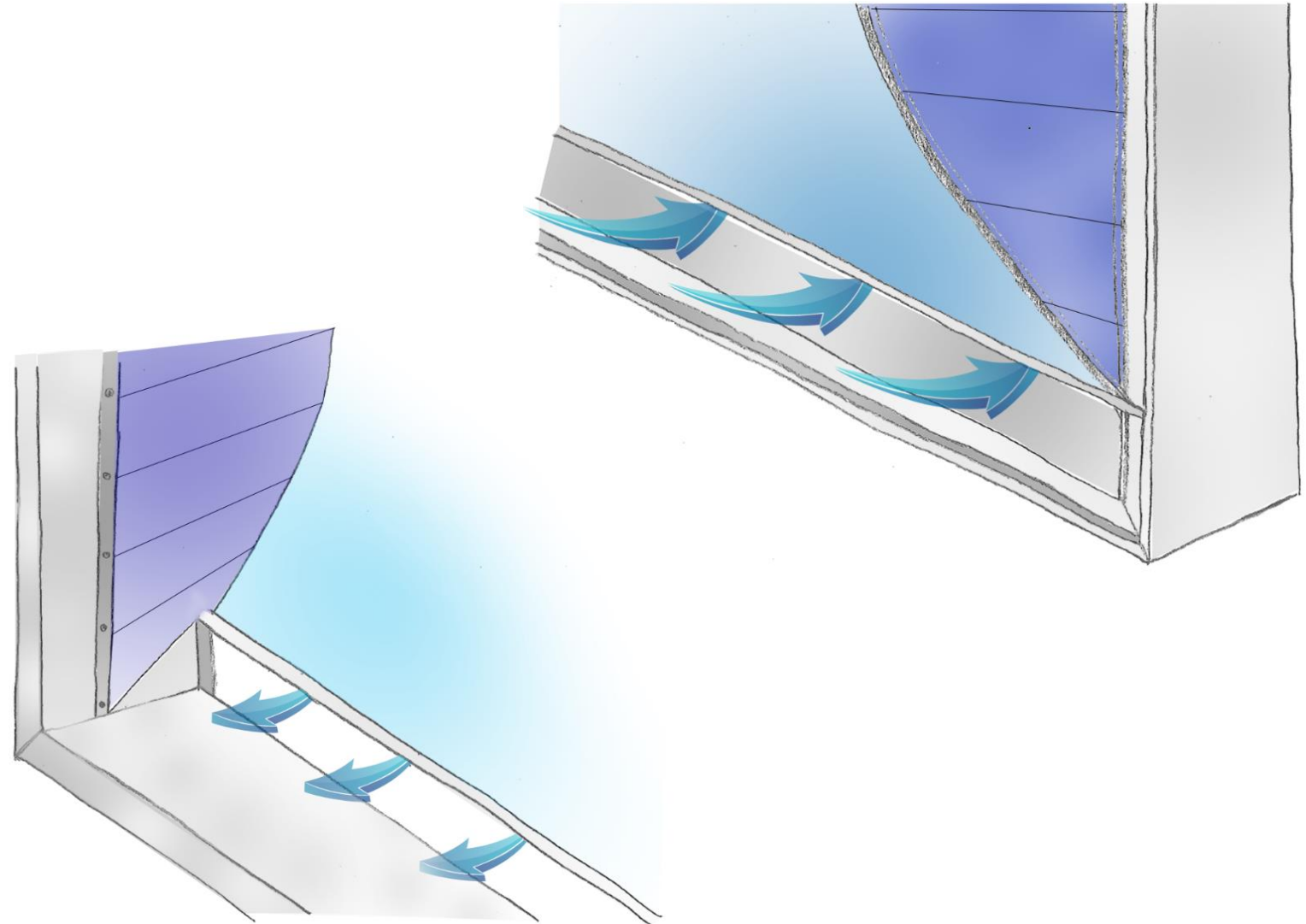
- Leakage at corner joint



Practical Feasibility

Option 3: Elastic Fabric

- Leakage at corner joint
- Ventilation gap limited



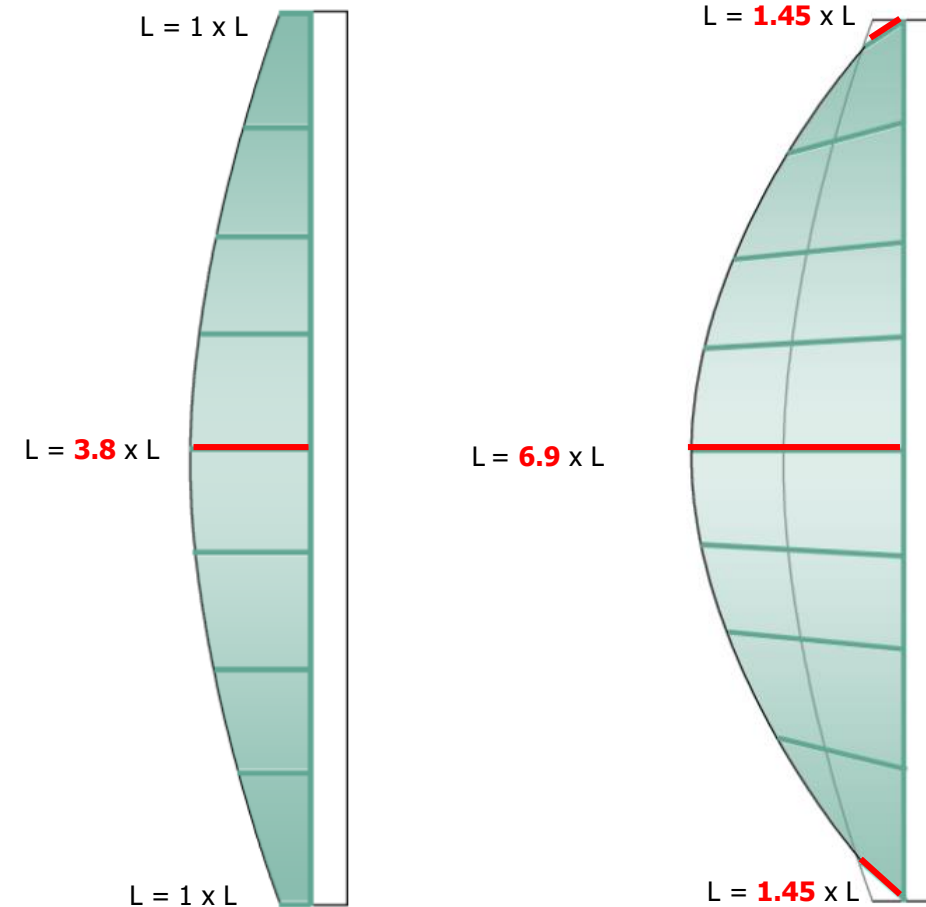
Practical Feasibility

Option 3: Elastic Fabric

- Leakage at corner joint
- Ventilation gap limited

Further concerns:

- High elasticity required + unequal stretching
- Obstruction of view

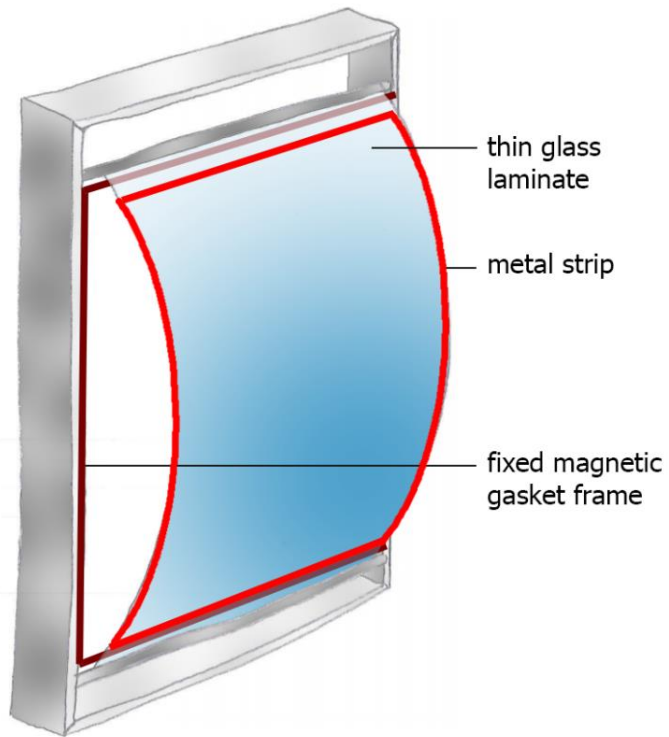


Selection of Design

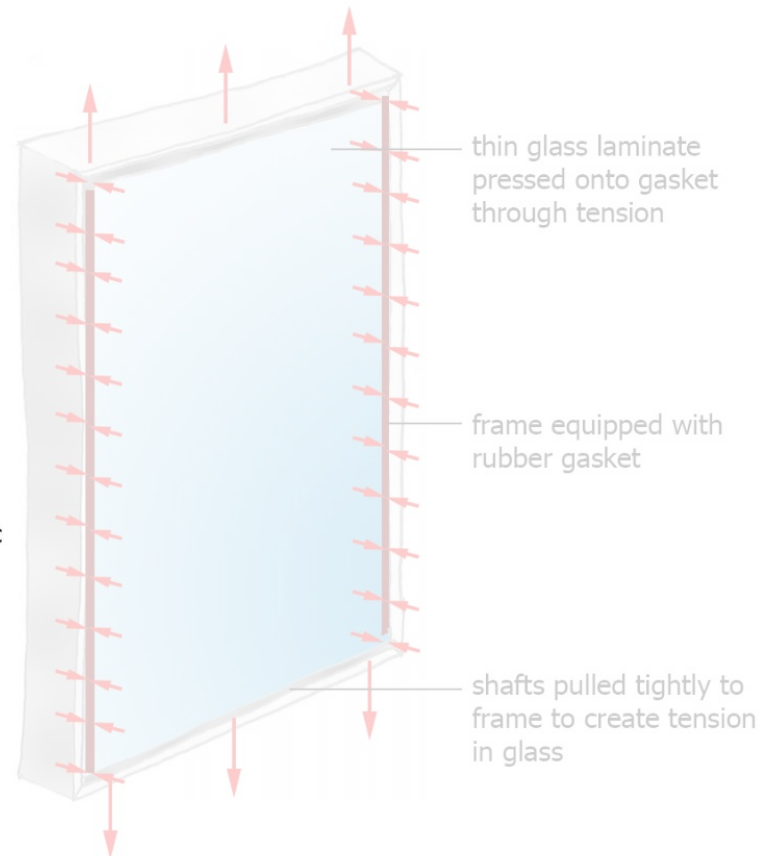
	Option 1		Option 2		Option 3	
practical feasibility	<p style="text-align: center;">+</p> <ul style="list-style-type: none"> o magnet can provide enough pulling force for water- airtightness o magnet pulling force adjustable 	<p style="text-align: center;">-</p> <ul style="list-style-type: none"> o additional horizontal frames required o abrupt opening movement due to magnetic holding force (only if permanent magnet) 	<p style="text-align: center;">+</p> <ul style="list-style-type: none"> o simple gasket detail possible 	<p style="text-align: center;">-</p> <ul style="list-style-type: none"> o unequally distributed pressure o additional horizontal frames required o extra force required to keep water- and airtight 	<p style="text-align: center;">+</p> <ul style="list-style-type: none"> o bent edges permanently sealed 	<p style="text-align: center;">-</p> <ul style="list-style-type: none"> o limited ventilation gap o leakage at corners o possible abrasion of fabric due to over-stretching o obstruction of view
structural suitability	<ul style="list-style-type: none"> o magnetic pulling force can also be used against wind suction 			<ul style="list-style-type: none"> o large force required to keep glazing shut o applied force may result in bending of shafts 		<ul style="list-style-type: none"> o large force required to keep glazing shut o applied force may result in bending of shafts o fabric may pull back edges of glazing with tendency to return to original length

Design Choice

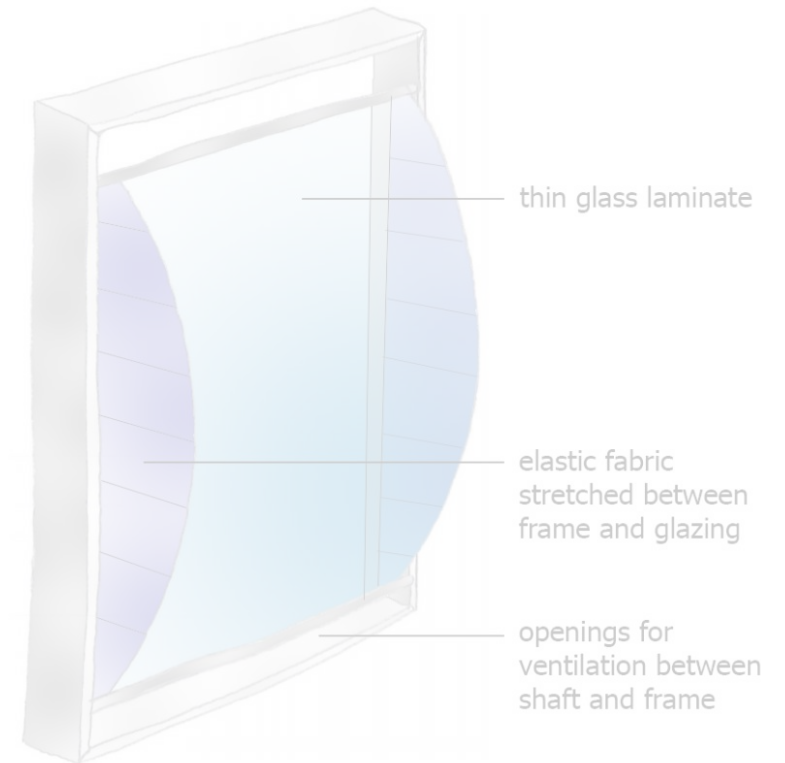
Option 1: Magnetic Force



Option 2: Tensile Force



Option 3: Elastic Fabric



Expected Performance of the Proposed Design

Requirements / Qualities	
watertightness	✓
airtightness	✓
thermal insulation	✗
acoustic insulation	✗
safety	✓
stiffness under high wind load	✗
natural ventilation	✓
transparency / optical quality	✓
cost-effectiveness	✗

Case Study

Possible Applications



Greenhouse/
Botanical Garden

Double Skin Facade
Glass Roof/
Application

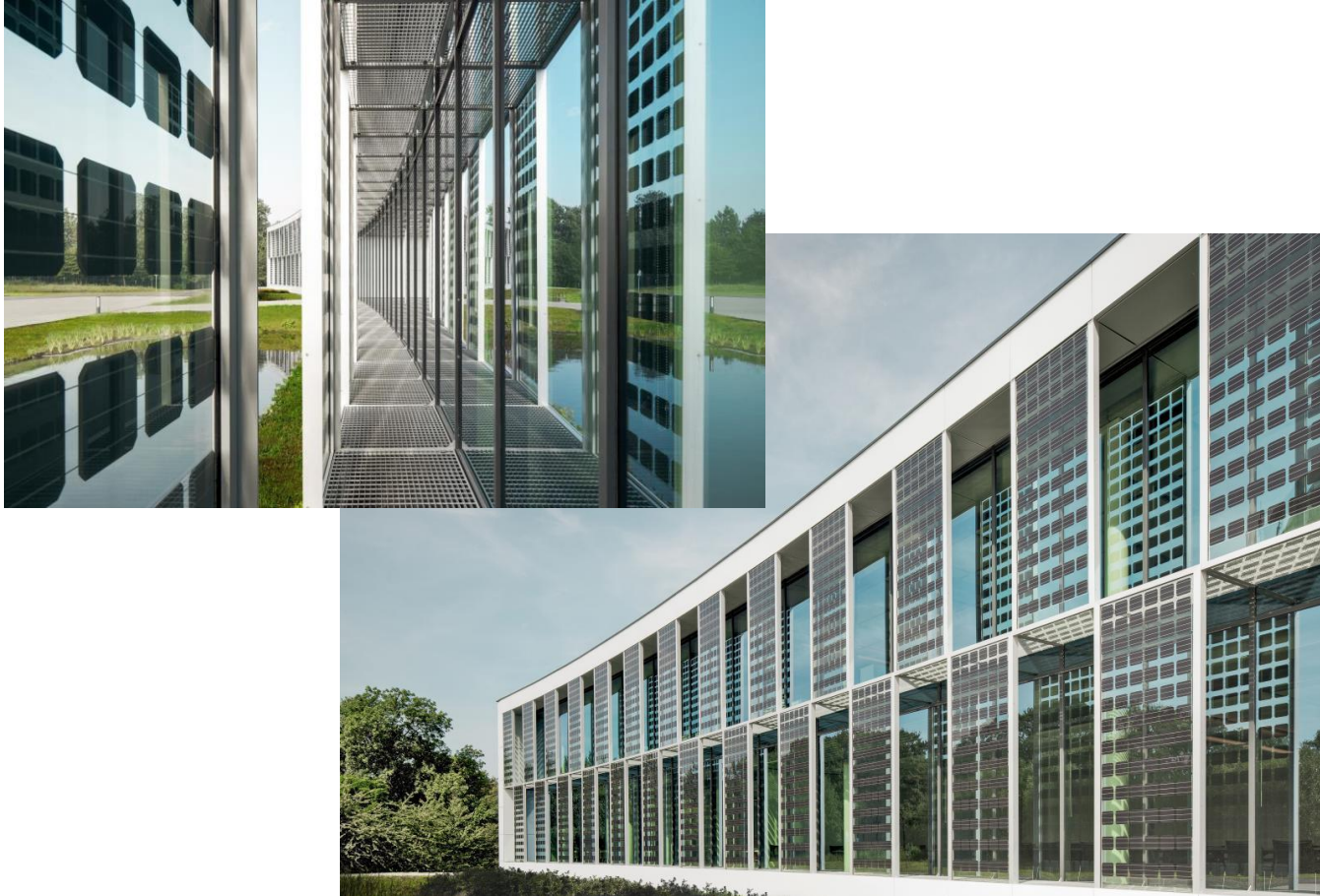


Requirements / Qualities

thermal insulation (only if heated and unheated spaces are divided)	✗
acoustic insulation	✗
safety	✓
transparency / optical quality	✓
transparency / optical quality	✓
showcasing the innovation	✗

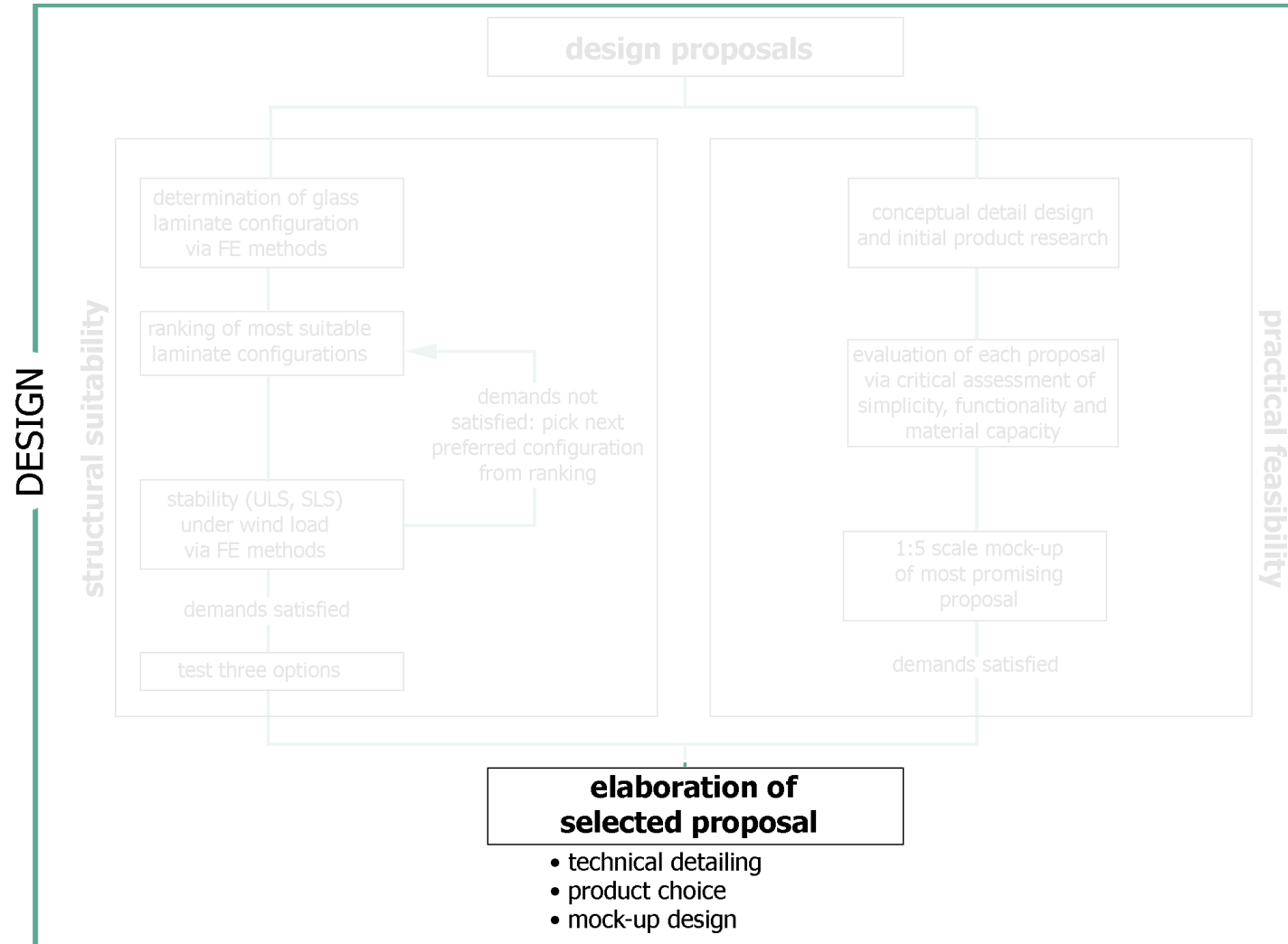
Case Study

AGC Technovation Center, Gosselies, Belgium



- Outer skin of open double-skin façade
 - No thermal and acoustic insulation
 - Functions solely as sun-protective layer and for power generation
 - “Show room” for company’s innovative product range
- Alternative design: closed cavity façade

Approach and Methodology



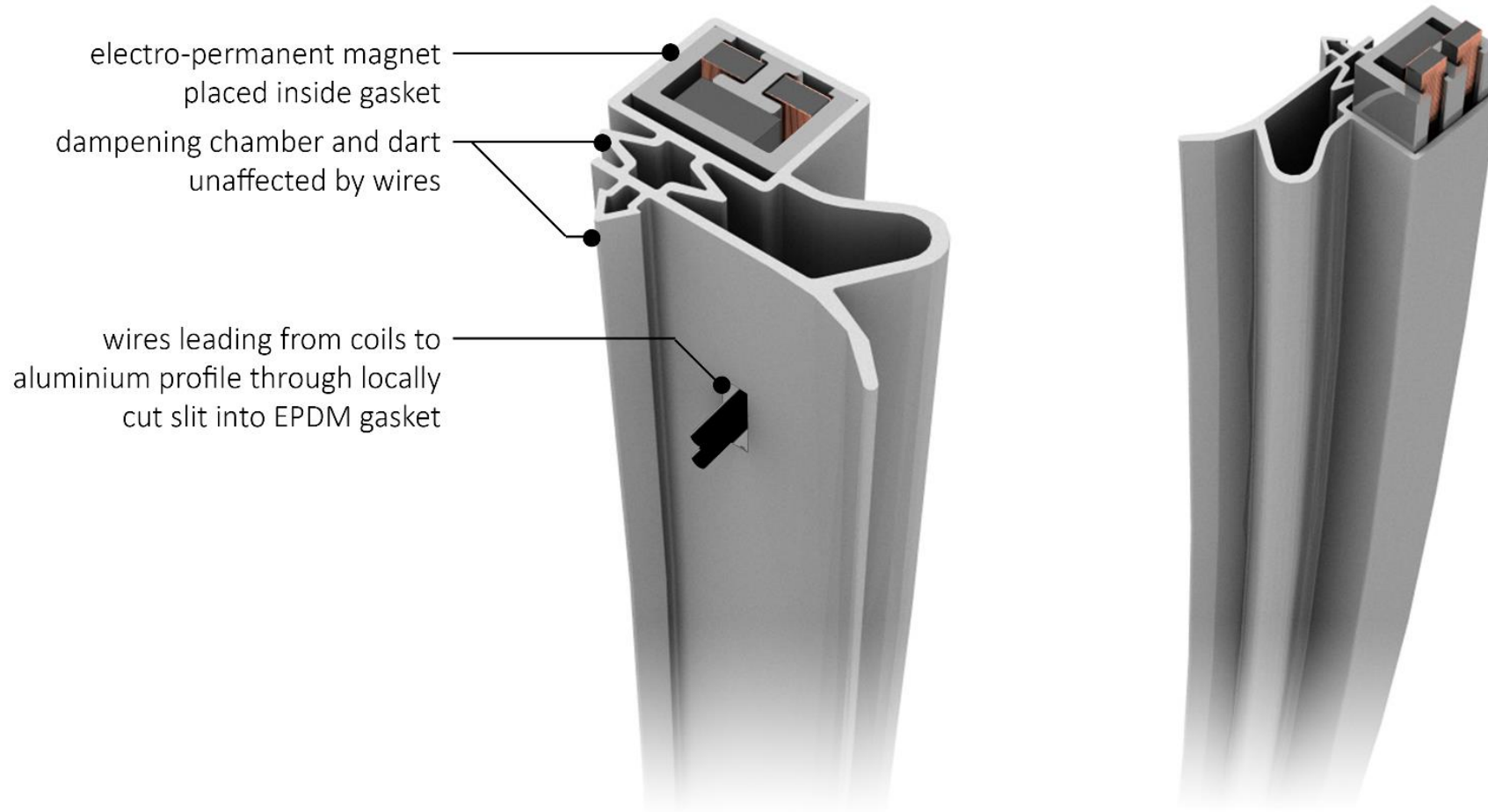
Elaboration of Selected Design

Focuses:

- Magnet-gasket design
- Mode of operation (kinetics)
- Facade profile design
- Manufacturing, assembly

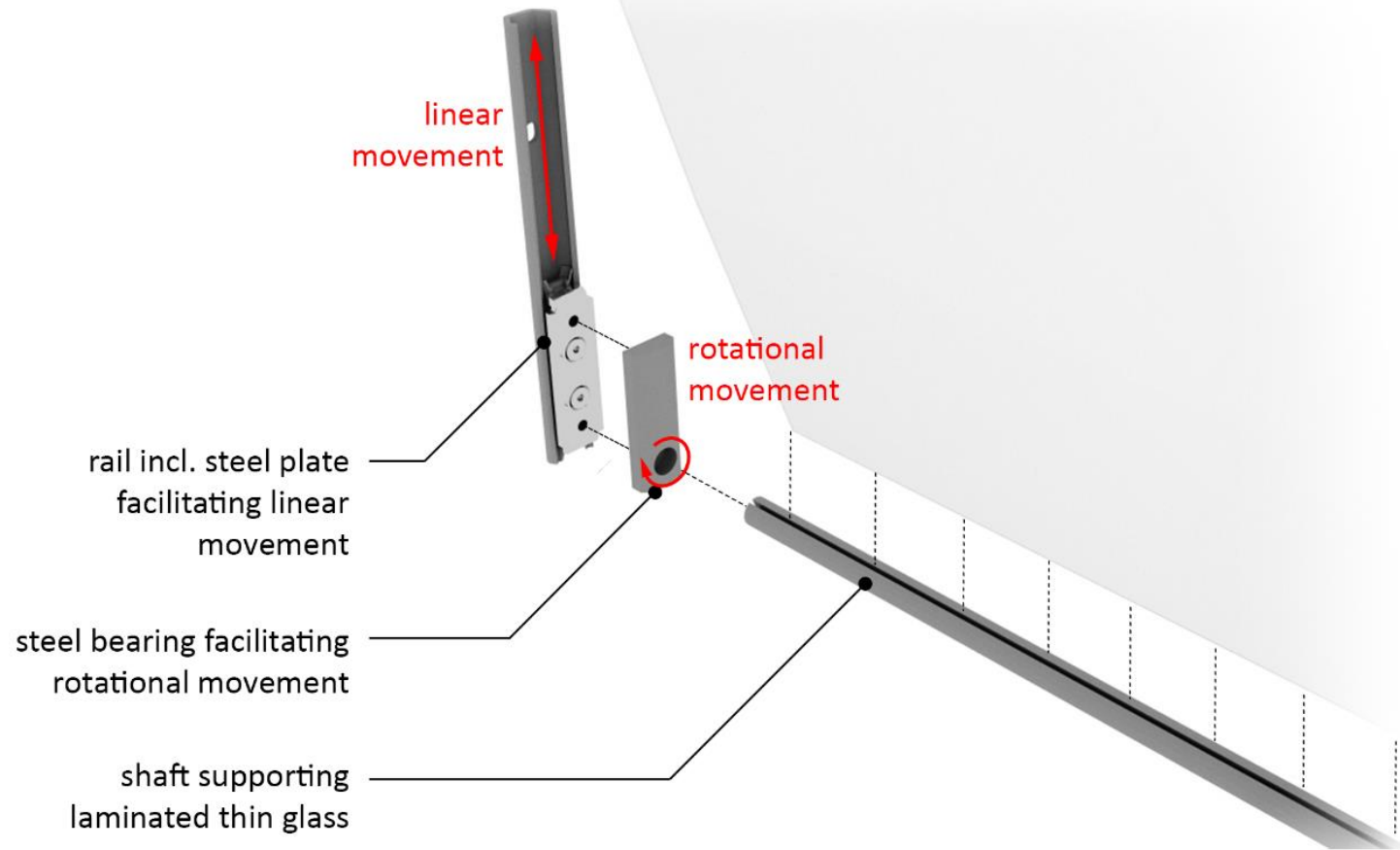
Elaboration of Selected Design

Gasket with Embedded Switchable Magnet



Elaboration of Selected Design

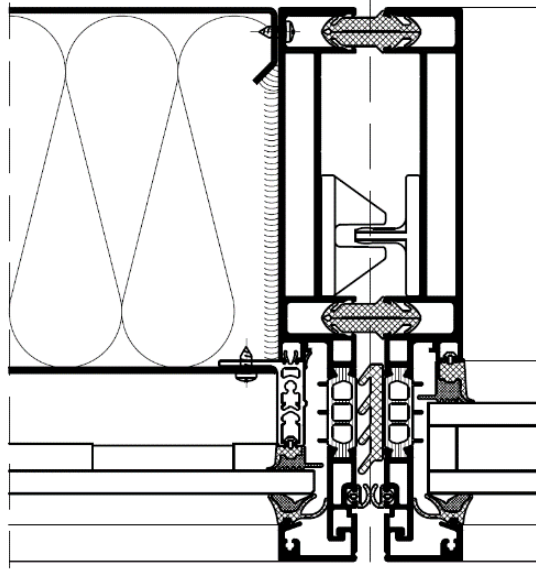
Mode of Operation



Elaboration of Selected Design

Façade Profile Design

- Unitised system

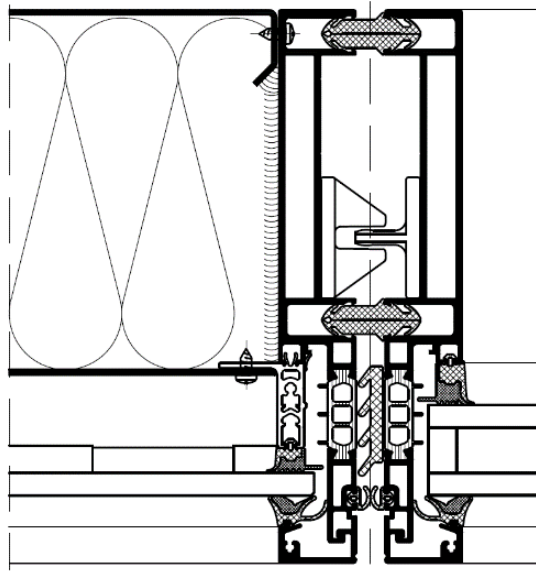


Schüco USC 65 unitised system

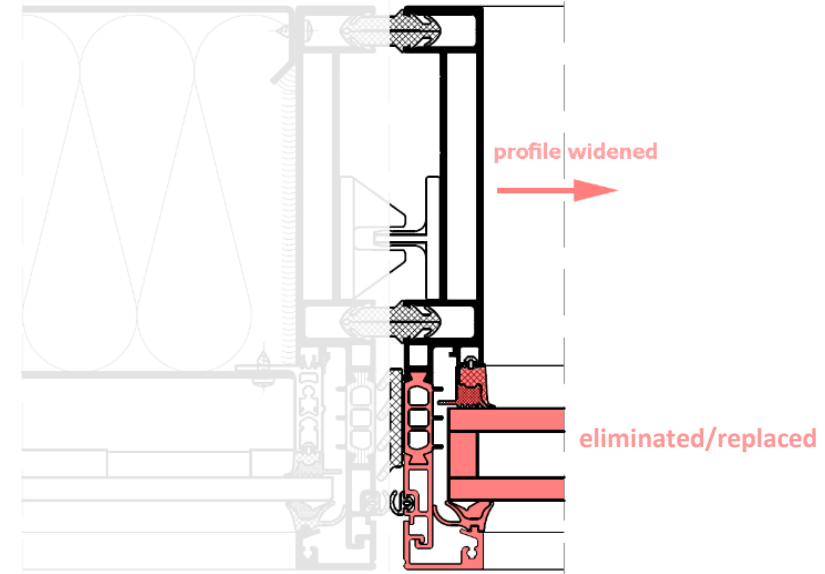
Elaboration of Selected Design

Façade Profile Design

- Unitised system
- Adjustments made to fit design



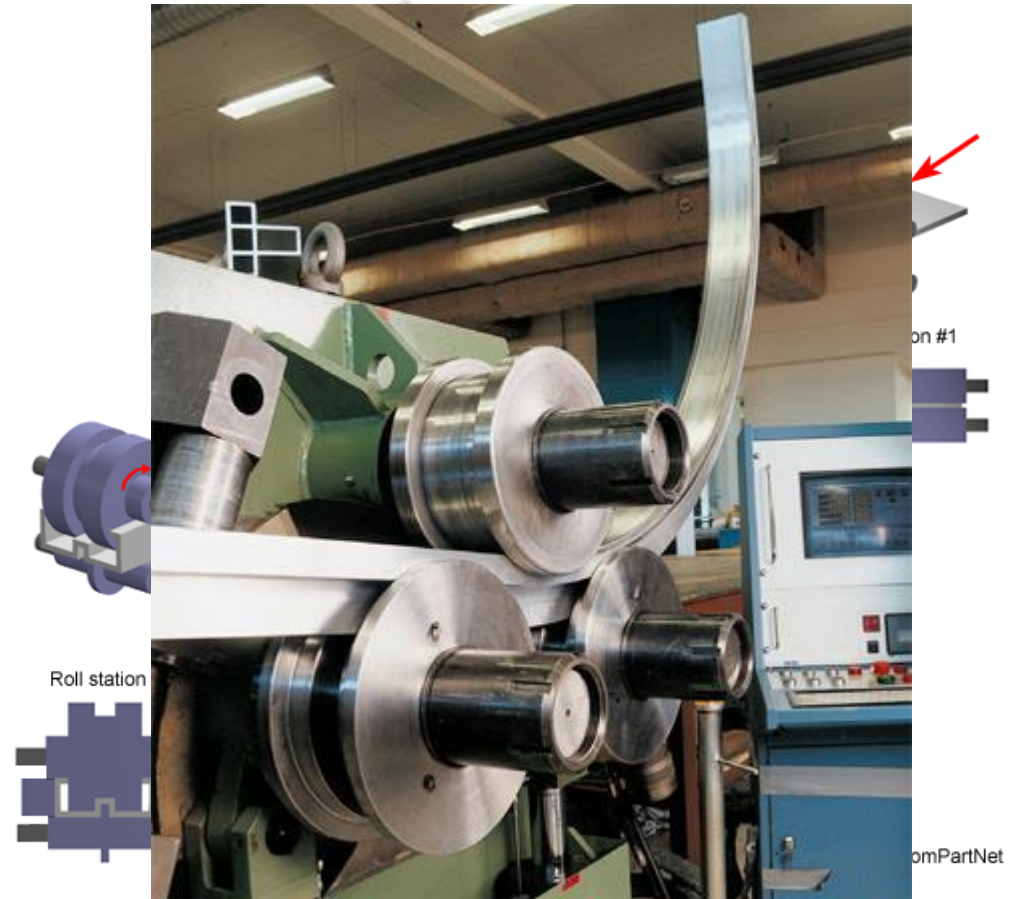
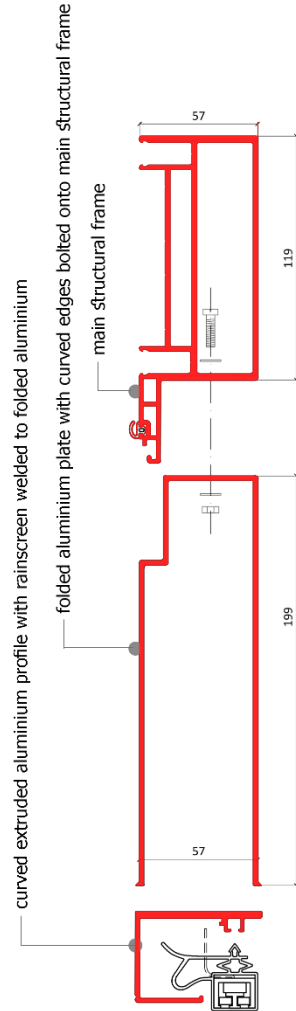
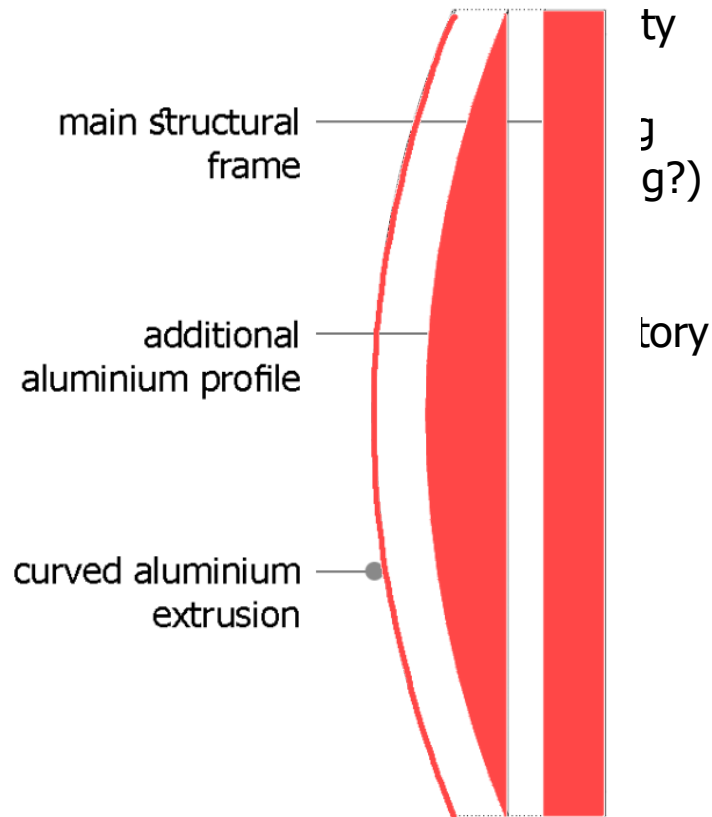
Schüco USC 65 unitised system



- Profile widened (to house rail, magnetic gasket etc.)
- Outer gasket eliminated (now single sided)
- Insulating layer eliminated (double-skin facade)

Elaboration of Selected Design

Façade Profile Design

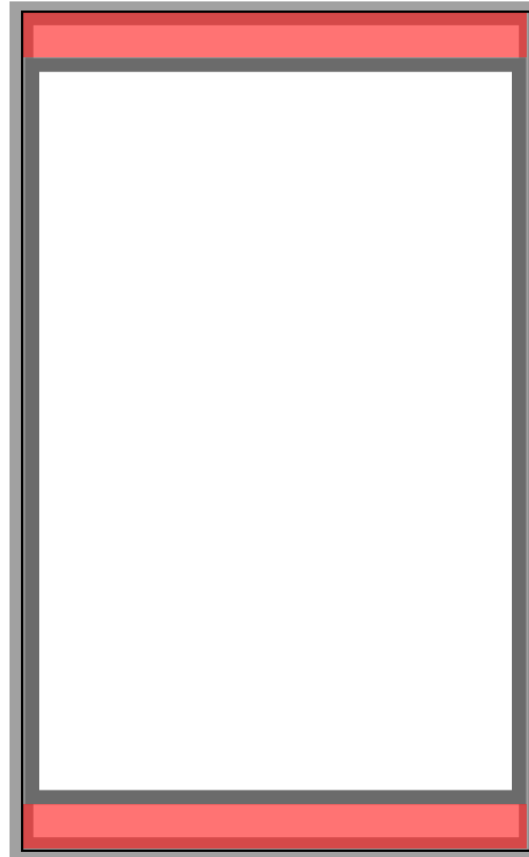


(source: www.aluminiumdesign.us.com)

Elaboration of Selected Design

Façade Profile Design

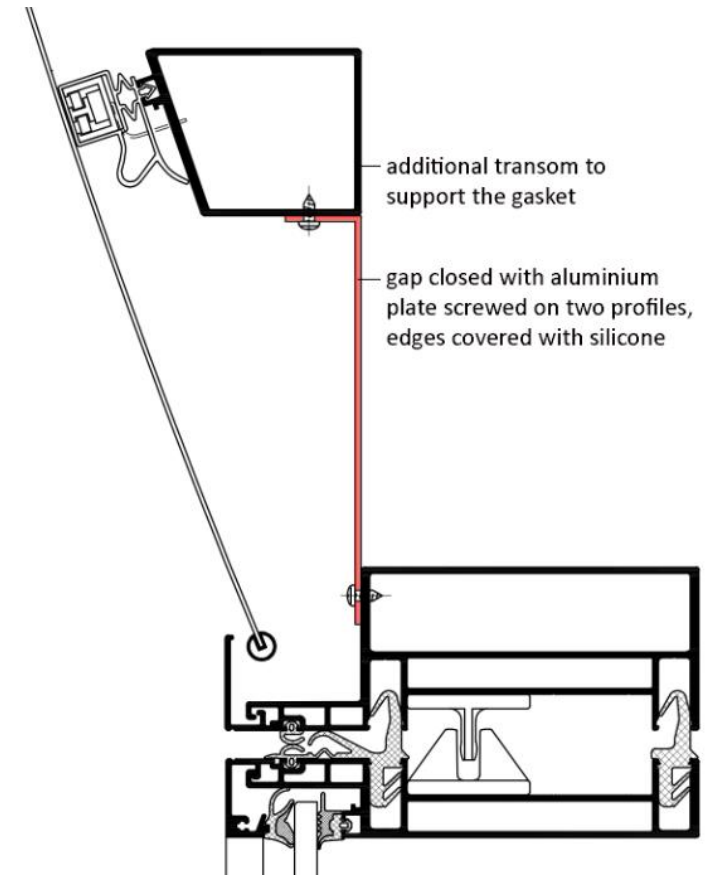
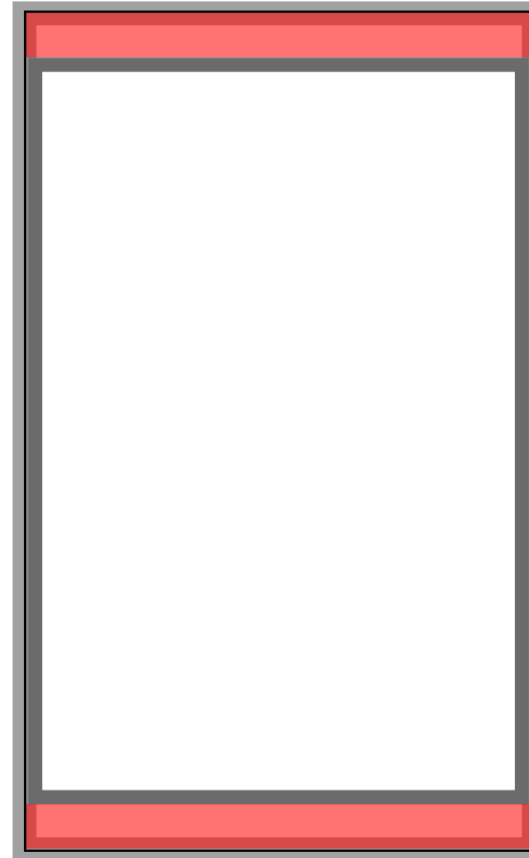
- Gap between main frame and additional transom



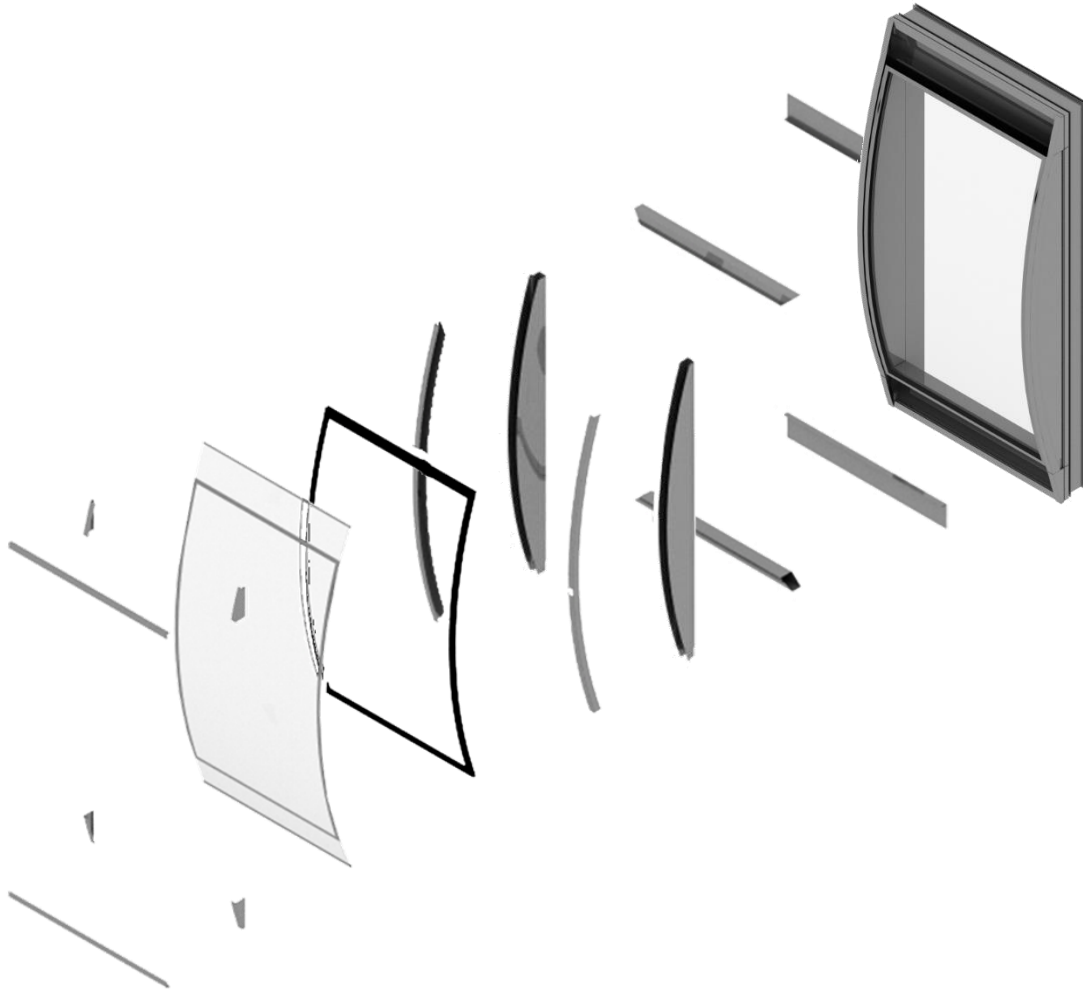
Elaboration of Selected Design

Façade Profile Design

- Gap between main frame and additional transom
- covered with aluminium plate, edges made airtight with silicone



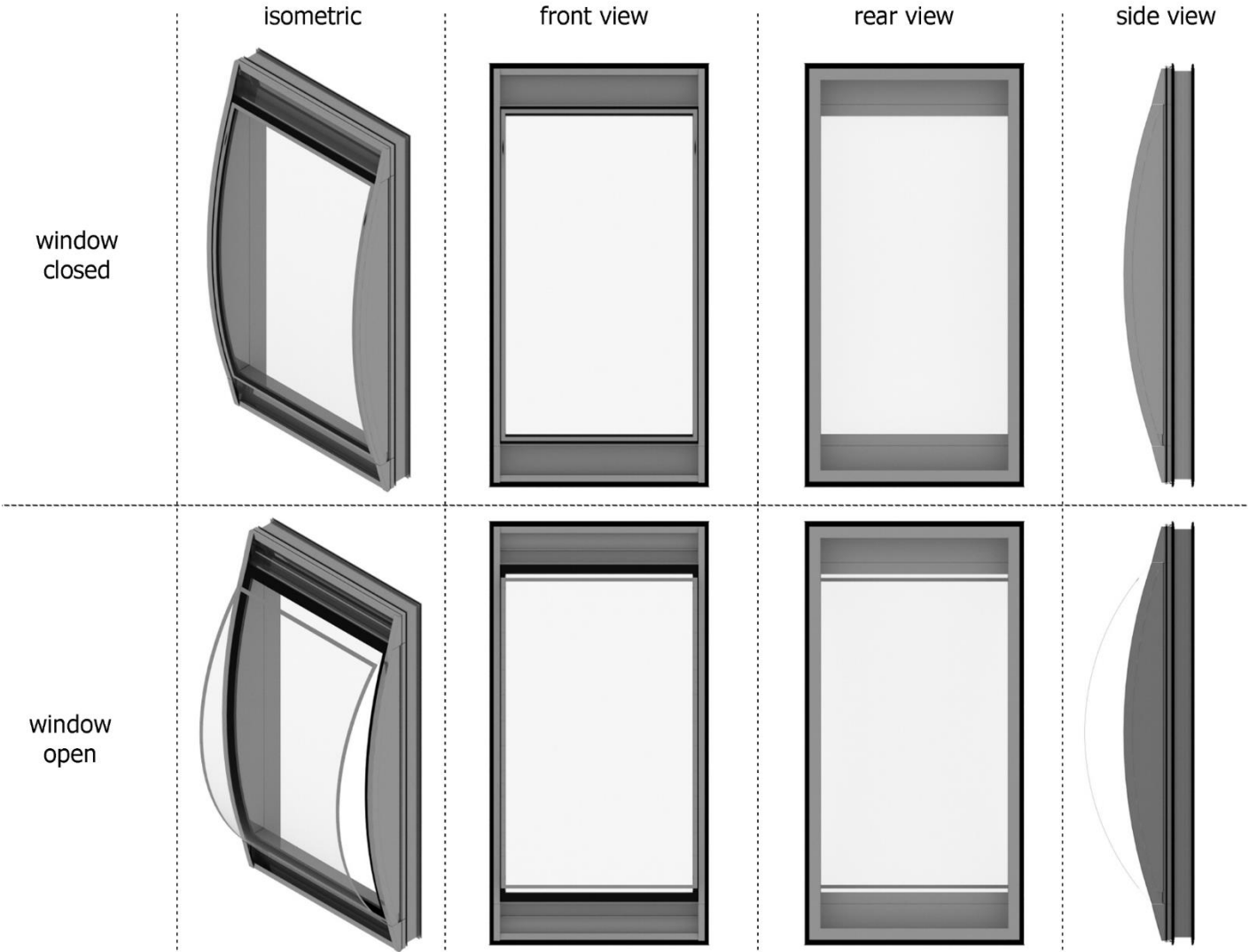
Final Design



Final Design

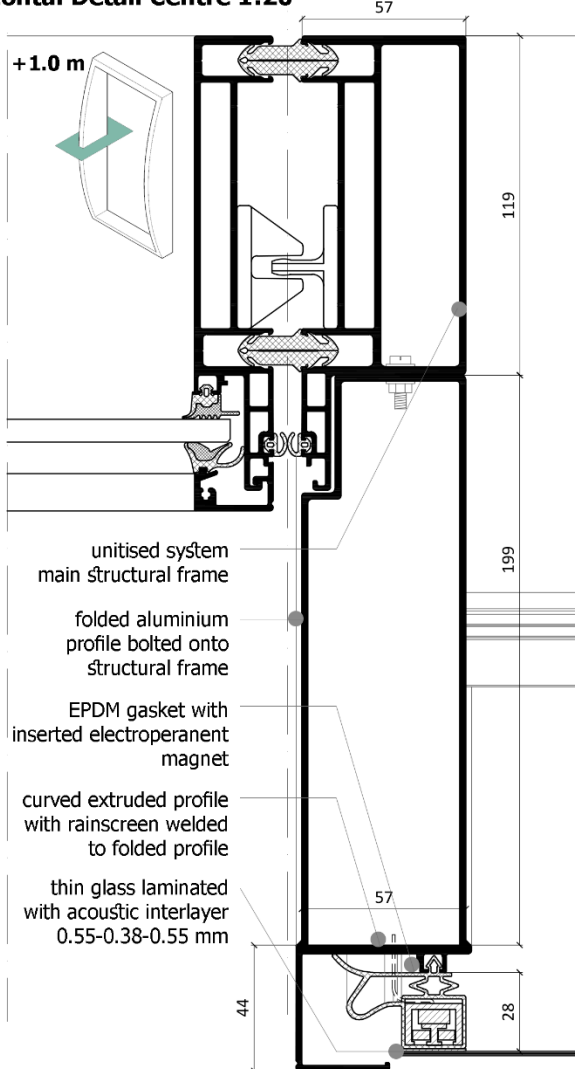


Final Design



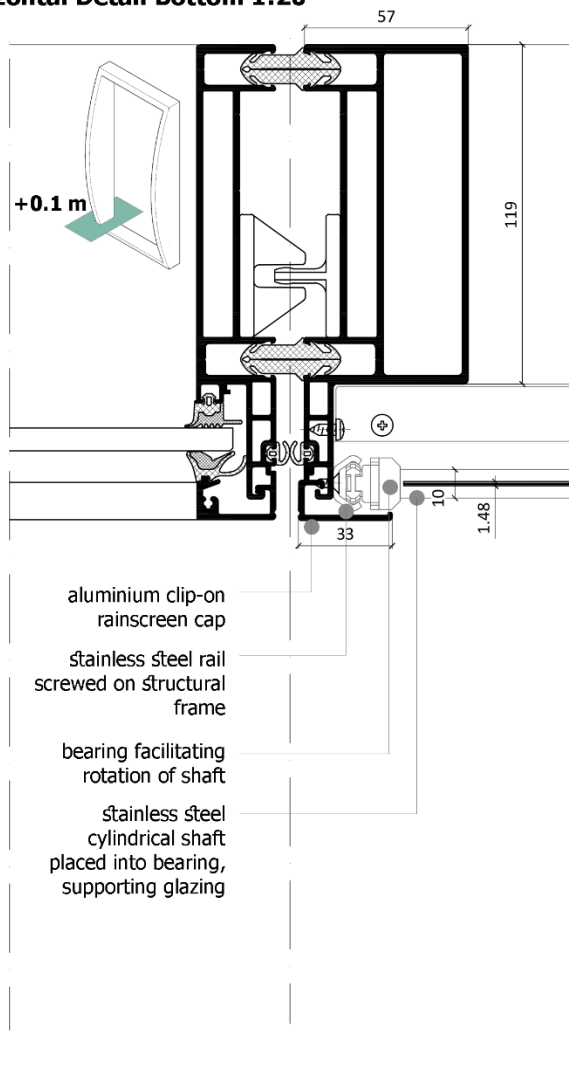
Final Design

Horizontal Detail Centre 1:20



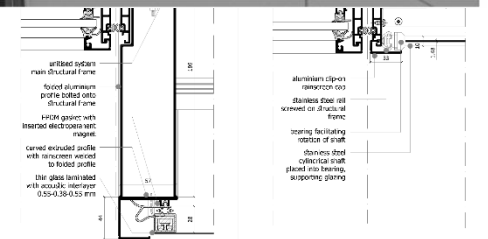
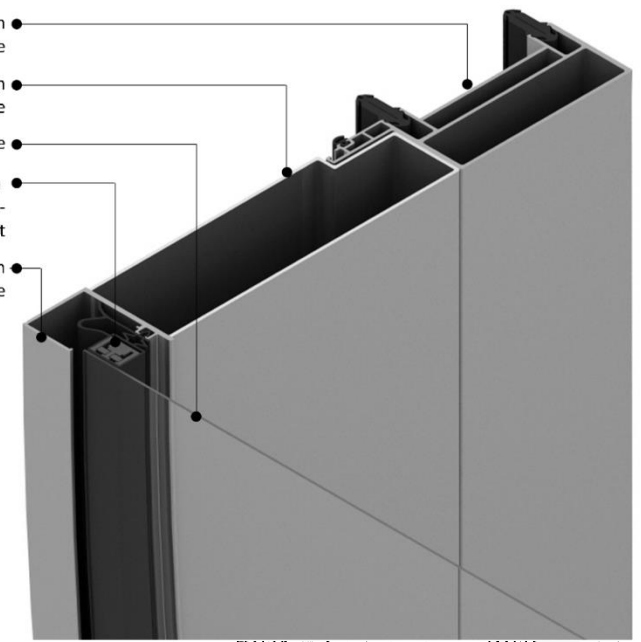
- unitised system main structural frame
- folded aluminium profile bolted onto structural frame
- EPDM gasket with inserted electropermanent magnet
- curved extruded profile with rainscreen welded to folded profile
- thin glass laminated with acoustic interlayer 0.55-0.38-0.55 mm

Horizontal Detail Bottom 1:20

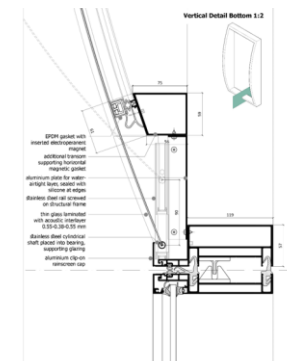
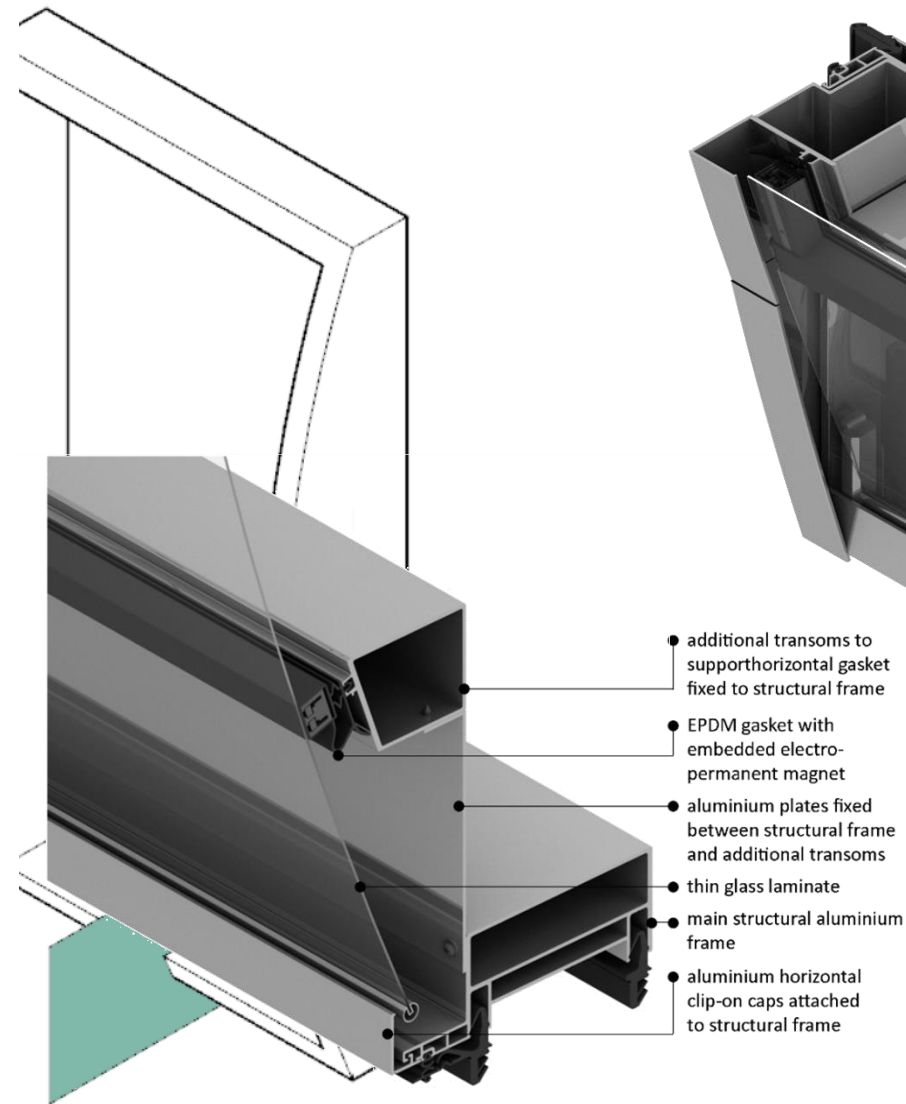
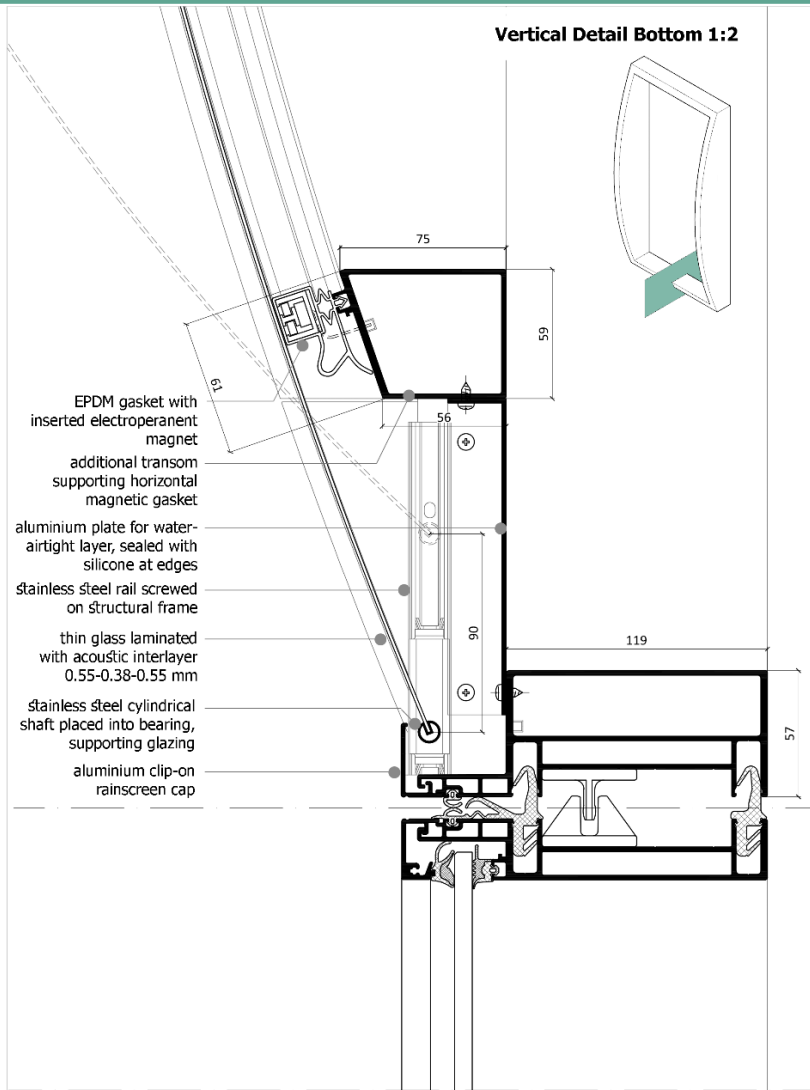


- aluminium clip-on rainscreen cap
- stainless steel rail screwed on structural frame
- bearing facilitating rotation of shaft
- stainless steel cylindrical shaft placed into bearing, supporting glazing

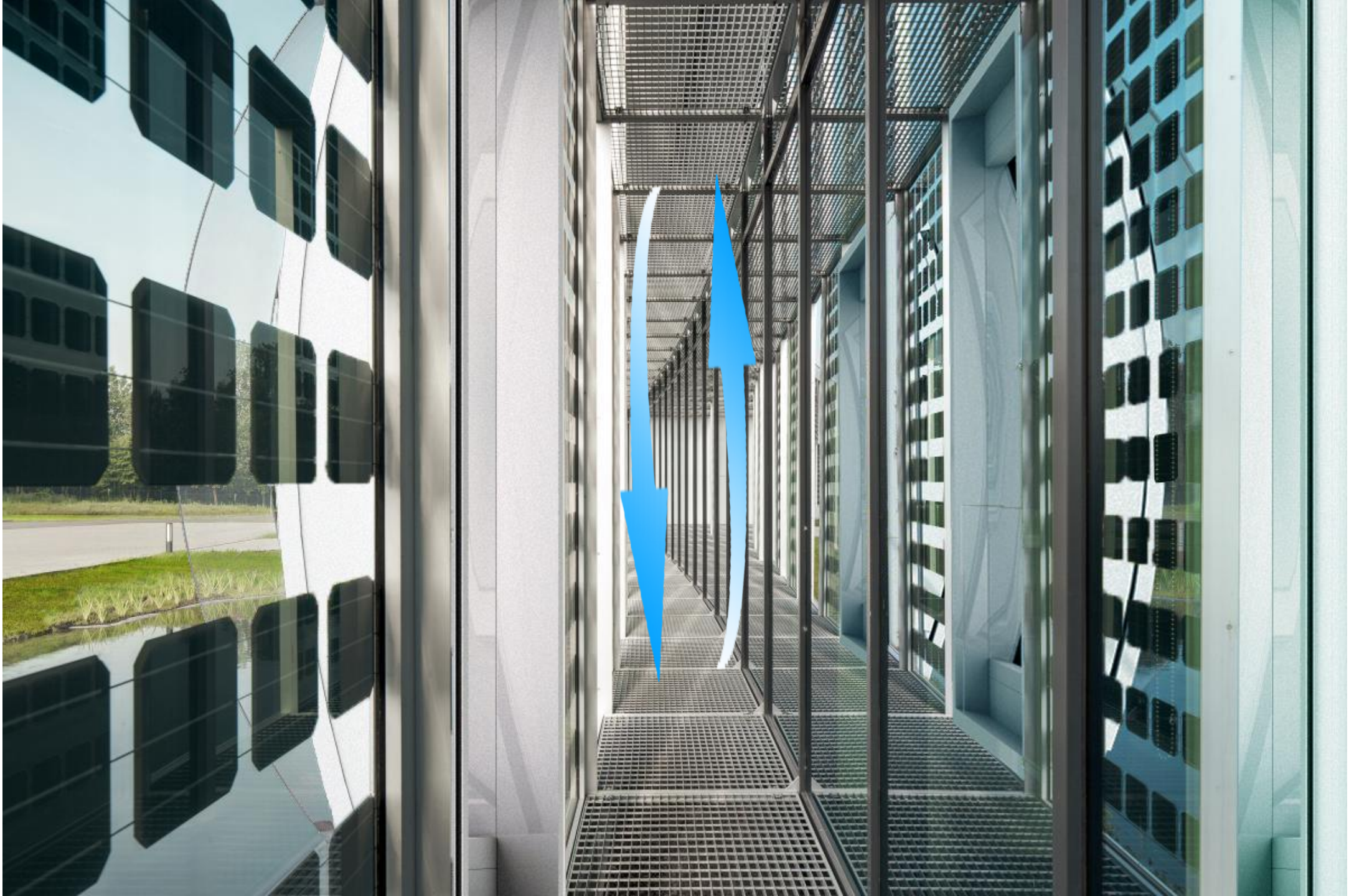
- extruded aluminium structural frame
- folded aluminium profile
- thin glass laminate
- EPDM gasket with embedded electropermanent magnet
- curved extrusion aluminium profile



Final Design







Conclusion

Answer to Main Research Question:

“How can a kinetic façade element featuring a bendable thin glass panel be designed to be water- and airtight in closed condition? ”

Design involves:

- Glazing consisting of two thin glass elements (0.55 mm) laminated with acoustic interlayer (0.38 mm) with metallic strip attached
- Switchable electro-permanent magnets placed inside the gasket
- Principle of active bending (1D-linear movement to 2D-deformation)
- Bespoke facade profiles designed to accommodate requirements

Discussion

- Research does not present optimal or only possibility to achieve the goal
- Meant to offer new **insights** into the field and form a **basis for further research**
- Many choices made during the process are **subjective**, although supported by numerical data and arguments from previous literature

→ main objectives fulfilled within theoretical framework:

- 1) Addition of a **second layer of glazing** to comply with safety regulations
- 2) Investigation of possibilities to combine the bending of thin glass with **water- and airtightness** properties

Reflection & Recommendations

Possibilities & Limitations

- **Sustainability** (reduced use of raw materials, lightweight loadbearing structures)
→ increased use of aluminium for stiffness
- **Cost reduction** (reduced use of raw materials, lightweight loadbearing structures)
→ chemical strengthening process, necessity of bespoke elements
- **New architectural impressions**
→ large variety of new possibilities, new architectural era?

Recommendations for further research

- Investigation of **other possible uses** for thin glass in architecture
 - for bending: sun shading, solar power generation, structural (load reduction)
 - building parts/types: glass roof, greenhouse, interior glazing, single skin
- Possibility to make **insulating glass unit** (double glazing)

Thank you for your attention!