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**DOI**

[10.1016/j.joule.2021.01.007](https://doi.org/10.1016/j.joule.2021.01.007)

**Publication date**

2021

**Document Version**

Accepted author manuscript

**Published in**

Joule

**Citation (APA)**

Ozden, A., Wang, Y., Li, F., Luo, M., Sisler, J., Thevenon, A., Rosas-Hernández, A., Burdyny, T., Lum, Y., & More Authors (2021). Cascade CO<sub>2</sub> electroreduction enables efficient carbonate-free production of ethylene. *Joule*, 5(3), 706-719. <https://doi.org/10.1016/j.joule.2021.01.007>

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# 1 **Cascade CO<sub>2</sub> electroreduction enables efficient carbonate-free** 2 **production of ethylene**

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17 **SUMMARY**

18 **CO<sub>2</sub> electroreduction (CO<sub>2</sub>RR) to multi-carbon products such as ethylene (C<sub>2</sub>H<sub>4</sub>)**  
19 **provides a route to produce valuable products and reduce CO<sub>2</sub> emissions. Despite**  
20 **improvements in catalytic performance, the direct transformation of CO<sub>2</sub>-to-C<sub>2</sub>H<sub>4</sub> suffers**  
21 **from CO<sub>2</sub> loss to carbonate. This CO<sub>2</sub> reactant loss is a major driver of cost, consuming**  
22 **up to 72% of total energy input. A cascade approach – coupling a solid-oxide CO<sub>2</sub>-to-CO**  
23 **electrochemical cell (SOEC) with a CO-to-C<sub>2</sub>H<sub>4</sub> membrane electrode assembly (MEA)**  
24 **electrolyser – would eliminate CO<sub>2</sub> loss to carbonate. However, this approach requires**  
25 **CO-to-C<sub>2</sub>H<sub>4</sub> in an MEA electrolyser with energy efficiency well beyond demonstrations**  
26 **to date. Focusing on the MEA, we find that the organic film produced from the reduction**  
27 **of N-tolylpyridinium to N-tolyl-tetrahydro-bipyridine improves the stabilization of key**  
28 **reaction intermediates, while an SSC ionomer enhances CO transport to the Cu surface,**  
29 **allowing for the stable production of C<sub>2</sub>H<sub>4</sub> at higher selectivities. We achieve a C<sub>2</sub>H<sub>4</sub>**  
30 **Faradaic efficiency (FE) of 65% at a current density of 166 mA cm<sup>-2</sup> over 110 hours of**  
31 **operation. Demonstrating a full cascade SOEC-MEA approach, we achieve CO<sub>2</sub>-to-C<sub>2</sub>H<sub>4</sub>**  
32 **with no loss of CO<sub>2</sub> to carbonate and a total energy requirement of ~138 GJ (tonne C<sub>2</sub>H<sub>4</sub>)<sup>-1</sup>**  
33 **, which represents a ~48% reduction in energy intensity compared to the direct route.**  
34 **We further couple CORR with glucose electrooxidation that enables carbonate**  
35 **formation-free C<sub>2</sub>H<sub>4</sub> production with a full-process energy requirement of ~89 GJ (tonne**  
36 **C<sub>2</sub>H<sub>4</sub>)<sup>-1</sup>.**

37 **Keywords**

38 CO electroreduction, carbon utilization, ethylene electrolysis, electrolyser, membrane  
39 electrode assembly, solid oxide electrolyser, catalyst design, molecular catalyst, energy  
40 efficiency.

41

42

## 43 INTRODUCTION

44 Global annual ethylene ( $C_2H_4$ ) production reached 185 Mt in 2018, exceeding that of any  
45 other organic chemical.<sup>1</sup> Production of  $C_2H_4$  involves steam cracking of fossil fuel-derived  
46 long-chain hydrocarbons – a process that releases 2-3 tonnes of  $CO_2$  per tonne of  $C_2H_4$   
47 produced before the in-plant  $CO_2$  capture.<sup>2</sup> The net process releases  $\sim 200$  Mt of  $CO_2$  annually,<sup>1</sup>  
48 accounting for 0.6% of total anthropogenic emissions.<sup>3</sup>

49  $CO_2$  electroreduction ( $CO_2RR$ ) using renewable electricity holds promise for low-carbon  
50  $C_2H_4$  production.<sup>4</sup> Present day  $CO_2RR$  has reached Faradaic efficiencies (FEs) of 70-80%  
51 towards  $C_2H_4$ <sup>5-7</sup> and energy efficiencies (EEs) over 30% at current densities over  $100\text{ mA cm}^{-2}$   
52 <sup>2,5</sup> However, due to the formation of carbonate during  $CO_2RR$  (Figure S1), concerns regarding  
53 the consequent penalty in energy consumption and production cost have risen.<sup>8,9</sup>

54 To assess the energy and cost associated with  $CO_2$  reactant loss to carbonate, we performed  
55 energy and techno-economic assessments (TEA) for benchmark neutral and alkaline  $CO_2RR$   
56 systems from literature, with the ideal and base case scenarios (Notes S1, S2, Figures S2, S3,  
57 S4, S5 and Tables S1 and S2). Electrolyte regeneration, system operation, and anodic product  
58 separation associated with carbonate formation significantly increases energy consumption and  
59 cost. The regeneration of alkaline electrolyte induces a penalty of  $\sim 278$  GJ per tonne  $C_2H_4$   
60 produced, accounting for 60-70% of the total energy requirement (Figures 1A, B). Membrane  
61 electrode assembly (MEA) electrolyzers result in less carbonate formation. However, six moles  
62  $CO_3^-$  for every mole of  $C_2H_4$  is produced, leading to a  $4\times$  increase in membrane resistance,<sup>10</sup>  
63 pH-gradient induced high voltages,<sup>11</sup> and 60-90 GJ of additional energy consumption per tonne  
64  $C_2H_4$  – a process energy penalty of  $\sim 35\%$  (Figures 1A, B and Tables S1, S2).

65 Encouraged by recent advances in  $CO$  electroreduction,<sup>8,9</sup> we took the view that carbonate-

66 free conversion of CO<sub>2</sub> to C<sub>2</sub>H<sub>4</sub> could be realized through two cascading steps (Figure 1C): (I)  
67 CO<sub>2</sub> reduction to CO in a high-temperature CO<sub>2</sub>-to-CO electrochemical cell (SOEC) which  
68 avoids carbonate formation<sup>12</sup> and (II) CO reduction to C<sub>2</sub>H<sub>4</sub> (CORR-to-C<sub>2</sub>H<sub>4</sub>) in an MEA  
69 electrolyser (Figure S6). Despite the cascade approach requiring additional energy input for  
70 separation and heating, as well as two separate systems, the cascade route could be competitive  
71 with the direct route (employing best-reported metrics in literature as inputs and assuming  
72 capital costs fixed to \$/kW, Table S1). The cascade approach benefits from high process  
73 efficiency in the SOEC step, as well as the use of an alkaline electrolyte in the CO-to-C<sub>2</sub>H<sub>4</sub>  
74 step, without suffering carbonate formation (Table S1 – Cell Voltage). For both  
75 electroproduction routes, operating potential, FE and current density are the most important  
76 parameters influencing the energy intensity of C<sub>2</sub>H<sub>4</sub> production (Figure S7).

## 77 **RESULTS AND DISCUSSION**

### 78 **CO<sub>2</sub>-to-CO conversion in an SOEC**

79 We established first the performance of CO<sub>2</sub>-to-CO in an SOEC. The SOEC was operated  
80 at 800°C. 95% CO FE and 89% CO EE were achieved at 815 mA cm<sup>-2</sup> and a CO<sub>2</sub> flow rate of  
81 20 sccm (Figure 2A). This is equal to a CO<sub>2</sub>-to-CO single-pass efficiency of ~36%. Utilization  
82 can be further improved by lowering flow rates or increasing current, to the limit imposed by  
83 the CO disproportionation reaction, also referred to as the Boudouard reaction.<sup>13,14</sup> Here, a  
84 maximum CO<sub>2</sub>-to-CO single-pass efficiency of ~55% was obtained (Figure 2B) at a CO FE of  
85 ~77%, current density of 1.25 A cm<sup>-2</sup>. At lower flow rates, considering both CO selectivity and  
86 CO<sub>2</sub> single-pass conversion, the current density vs. CO<sub>2</sub> flow rate ratio of 815:15 (mA cm<sup>-2</sup>:  
87 sccm) was confirmed to be the best condition under which we observed a constant CO FE of  
88 ~91% and CO<sub>2</sub>-to-CO single-pass conversion of ~45% (Figure 2C). The energy input  
89 requirement for this SOEC step was 13.49 GJ/tonne CO.

## 90 **CORR MEA for C<sub>2</sub>H<sub>4</sub> electroproduction**

91 For C<sub>2</sub>H<sub>4</sub> production, our analysis shows that the success of this two-step approach relies  
92 on CO-to-C<sub>2</sub>H<sub>4</sub> in an MEA electrolyser (Figures S3-S5). High C<sub>2</sub>H<sub>4</sub> FE (> 60%) is required in  
93 concert with high current density (>150 mA cm<sup>-2</sup>) and low operating full-cell potential (< 3 V).  
94 To date, the highest FE for CO-to-C<sub>2</sub>H<sub>4</sub> in MEA electrolysers remains below 40%, and the  
95 corresponding C<sub>2</sub>H<sub>4</sub> partial current density ( $j_{\text{C}_2\text{H}_4}$ ) is less than 60 mA cm<sup>-2</sup>.<sup>8</sup> We therefore  
96 sought to develop a high performance CO-to-C<sub>2</sub>H<sub>4</sub> MEA electrolyser that is essential for  
97 efficient, cascade CO<sub>2</sub>-to-C<sub>2</sub>H<sub>4</sub> conversion.

98 We first electrodeposited copper (Cu) catalysts under CO<sub>2</sub>-rich conditions as MEA  
99 cathodes. A CO<sub>2</sub>-rich environment increases Cu(100) exposure,<sup>15</sup> which enhances the  
100 selectivity towards C<sub>2</sub>H<sub>4</sub> in CO<sub>2</sub>RR.<sup>8,16</sup> However, a simple Cu surface has large regions that do  
101 not have ready access to CO on the hydrophilic surface (Figure S8A).<sup>17</sup> We assembled the  
102 MEA – using electrodeposited Cu as the cathode electrode, anion exchange membrane as the  
103 solid state electrolyte, and iridium oxide supported on a titanium mesh as the anode electrode  
104 – and investigated the CORR performance. This catalyst consequently favors H<sub>2</sub> production,  
105 allowing C<sub>2</sub>H<sub>4</sub> production with a maximum FE of only 50% at a low partial current density  
106 ( $j_{\text{C}_2\text{H}_4}$ ) of 60 mA cm<sup>-2</sup> (Figure S8B).

107 Modifying the Cu surface with hydrophobic aliphatic molecules or ionomers has been  
108 demonstrated to increase reactant availability at the catalytic interface<sup>17-19</sup> and improve the  
109 selectivity and activity towards C<sub>2</sub>H<sub>4</sub> electroproduction<sup>20</sup>. We therefore added a  
110 (C<sub>4</sub>HF<sub>7</sub>O<sub>4</sub>S .C<sub>2</sub>F<sub>4</sub>)<sub>x</sub> short-side-chain (SSC) ionomer coating on the Cu surface.<sup>21</sup> We found that  
111 H<sub>2</sub> selectivity was suppressed by 10-30% across the screened cell potential window, and that  
112 the highest  $j_{\text{C}_2\text{H}_4}$  increased to ~155 mA cm<sup>-2</sup> (Figure S9). However, the maximum C<sub>2</sub>H<sub>4</sub> FE  
113 remained ~50%.

114 The strategy we pursued to promote C<sub>2</sub>H<sub>4</sub> at lower potentials was to alter the adsorption of  
115 the key CO\* intermediate via a molecular tuning strategy.<sup>6</sup> We therefore introduced an *N*-*tolyl*  
116 *substituted tetrahydro-bipyridine* (labeled Py) interlayer between Cu and SSC by an electro-  
117 dimerization method.<sup>6</sup> This metal:molecular film:ionomer combination (labeled Cu:Py:SSC),  
118 in which SSC improves the CO diffusion at the outer layer and Py provides more atop-bound  
119 CO\* on Cu surface (Figure 3A), enabled the highest C<sub>2</sub>H<sub>4</sub> FE of 65 ± 1% at a 2.5 V full-cell  
120 potential and provided a  $j_{\text{C}_2\text{H}_4}$  of 130 mA cm<sup>-2</sup> at 2.6 V (Figure 3B). Detailed CORR-to-C<sub>2</sub>H<sub>4</sub>  
121 performance of the Cu:Py:SSC, Cu:SSC, and bare Cu are summarized in Tables S3-S5. To  
122 gain insight into the enhanced CO-to-C<sub>2</sub>H<sub>4</sub> selectivity and productivity, we investigated the  
123 catalysts using scanning and transmission electron microscopy (SEM and TEM, respectively).  
124 We observed a dendritic Cu fully covered by the Py molecule and SSC ionomer (Figure 3C  
125 and Figure S10). The Cu catalyst has high crystallinity, confirmed by the grazing-incidence  
126 wide-angle X-ray scattering (GIWAXS) (Figure S11). We conclude that there was full  
127 coverage of Py and SSC on the Cu surface.

128 We then conducted *operando* Raman spectroscopic studies on the catalytic interface.<sup>22-25</sup>  
129 We observed a stabilized atop-bound CO\*,<sup>6</sup> known to favor the key CO-CO dimerization  
130 step,<sup>26-28</sup> evidenced by the transformation of CO\* adsorption configurations (Figure S12): the  
131 fraction of the area of atop-bound CO\* at the wave number of ~2080 cm<sup>-1</sup><sup>29</sup> increased to 33%  
132 when Py molecule was electrodeposited onto the Cu surface. By contrast, bridge-bound CO\*  
133 at 1980-2020 cm<sup>-1</sup><sup>29-31</sup> dominated the adsorption configurations on the bare Cu.

134 We then sought to optimize the full-cell EE by increasing the alkalinity of the anolyte  
135 (Figure 3D and Tables S6-S8). With increasing KOH concentration, the C<sub>2</sub>H<sub>4</sub> FE peak  
136 increased to ~65% (Figure 3D), an example of alkalinity favoring C<sub>2+</sub> production.<sup>5,32,33</sup> The  
137 ionic conductivity was also improved by high alkalinity, and the  $j_{\text{C}_2\text{H}_4}$  at each C<sub>2</sub>H<sub>4</sub> FE peak

138 increased from  $\sim 47$  to  $\sim 100$  mA cm<sup>-2</sup>, and the full-cell potential reduced from 2.8 to 2.5 V in  
139 the range of 0.1 to 3 M KOH (Figure 3D, Figure S13, and Tables S5-S7). However, 5 M KOH  
140 lowered the  $j_{\text{C}_2\text{H}_4}$  to 81 mA cm<sup>-2</sup> at all applied potentials (Figure S14 and Table S8), which we  
141 attribute to a low CO concentration at the catalyst layer under this condition (Figure S15).  
142 Considering C<sub>2</sub>H<sub>4</sub> FE,  $j_{\text{C}_2\text{H}_4}$ , and full-cell potential, the 3 M KOH is the best analyte for CO-  
143 to-C<sub>2</sub>H<sub>4</sub> conversion in this system.

144 Further comparisons in 3 M KOH revealed that the Cu:Py:SSC combination outperformed  
145 the Cu:SSC and bare Cu in terms of both  $j_{\text{C}_2\text{H}_4}$  and C<sub>2</sub>H<sub>4</sub> full-cell EE (Figure 3E). Importantly,  
146 we achieve – when compared to bare Cu – a 5x increase in the peak  $j_{\text{C}_2\text{H}_4}$  (from  $26 \pm 2$  to  $129 \pm 1$   
147 mA cm<sup>-2</sup>) and a 1.4x increase in the peak full-cell EE (from  $21 \pm 2$  to  $29 \pm 1\%$ ) using the  
148 Cu:Py:SSC combination (Tables S3 and S5). We observed typical CORR gas and liquid  
149 products in the current density range of 25 to 250 mA cm<sup>-2</sup>, with the peak C<sub>2+</sub> FE of  $\sim 85\%$  at  
150 160 mA cm<sup>-2</sup> (Table S9 and Figure S16). A stable 28% C<sub>2</sub>H<sub>4</sub> full-cell EE for the Cu:Py:SSC  
151 system was achieved in the current density range of 80 to 170 mA cm<sup>-2</sup>, whereas the Cu:SSC  
152 and bare Cu systems were limited to EEs of  $< 20\%$  in this current density range (Figure 3E).  
153 Further optimization of the CO coverage on the Cu:Py:SSC catalyst – through co-feeding CO  
154 with N<sub>2</sub> – improved the C<sub>2</sub>H<sub>4</sub> full cell EE to  $30 \pm 1\%$  at a constant current density of 100 mA  
155 cm<sup>-2</sup> (Table S10).

156 We investigated the C<sub>2</sub>H<sub>4</sub> production rate ( $R_{\text{C}_2\text{H}_4}$ ) and its concentration in the product  
157 stream. The Cu:Py:SSC combination produced C<sub>2</sub>H<sub>4</sub> at almost 0.68 mmol cm<sup>-2</sup> h<sup>-1</sup> and 1.5 and  
158 6 times faster than the Cu:SSC and bare Cu, respectively (Figure S17). Using an inlet CO flow  
159 rate of 4 sccm, we obtained a  $\sim 36\%$  C<sub>2</sub>H<sub>4</sub> concentration in gas products (Figure 3F and Table  
160 S11). This translated to a  $\sim 26\%$  CO-to-C<sub>2</sub>H<sub>4</sub> single-pass conversion and is  $\sim 3$  times higher than  
161 that of bare Cu.



162 We confirmed the stability of the MEA with the Cu:Py:SSC catalyst using 3 M KOH at  
163 150 mA cm<sup>-2</sup>. The system maintained a constant C<sub>2</sub>H<sub>4</sub> FE of 61 ± 2% and a full-cell potential  
164 of 2.73 ± 0.02 V for 110 hours with no performance degradation (Figure 3G). We analyzed the  
165 cathode electrode after 110-hour continuous electrolysis, using electron microscopy, X-ray  
166 photon spectroscopy, and soft X-ray adsorption spectra (sXAS) at the N K-edge. The Cu  
167 morphology and Py:SSC coating as well as associated features were retained (Figures S18, S19,  
168 and S20). The MEA equipped with the Cu:Py:SSC catalyst – when taking the carbonate  
169 formation penalty into account – outperformed literature benchmarks<sup>6,8,11,34-36</sup> including both  
170 CO<sub>2</sub>RR and CORR, in C<sub>2</sub>H<sub>4</sub> FE,  $j_{C_2H_4}$ , C<sub>2</sub>H<sub>4</sub> full-cell EE and operation duration (Table S12).

### 171 **Cascade CO<sub>2</sub>-to-C<sub>2</sub>H<sub>4</sub> electroreduction in the integrated system**

172 We built an integrated system for carbonate-free CO<sub>2</sub>-to-C<sub>2</sub>H<sub>4</sub> electroproduction (Figure  
173 1C) by combining the high-performance CO-to-C<sub>2</sub>H<sub>4</sub> MEA with the CO<sub>2</sub>-to-CO SOEC. The  
174 SOEC was operated at 800°C and a current density of 550 mA cm<sup>-2</sup>, yielding a ~95% CO FE,  
175 ~86% CO full-cell EE (for electricity only), and ~48% single-pass utilization (Figure S21). The  
176 inlet CO<sub>2</sub> flow rate was set at 10 sccm to ensure the optimal 815:15 (mA cm<sup>-2</sup> vs. sccm) ratio  
177 of current density: CO<sub>2</sub> flow rate and an outlet CO production of ~4.5 sccm for a high CO-to-  
178 C<sub>2</sub>H<sub>4</sub> single-pass conversion utilization. The products of the SOEC were purified using CO<sub>2</sub>  
179 capture solution containing 30% ethanolamine before feeding into the CO-to-C<sub>2</sub>H<sub>4</sub> MEA. The  
180 temperature of the purified gas supplied to the MEA electrolyser was measured to be 25 °C.  
181 The system had a peak CO<sub>2</sub>-to-C<sub>2</sub>H<sub>4</sub> EE (for electricity only) of 20% (Figure 4A) and a  
182 maximum single-pass conversion of ~11% for CO<sub>2</sub>-to-C<sub>2</sub>H<sub>4</sub> with no loss of CO<sub>2</sub> to carbonate  
183 formation in electrolytes (Figure 4B). The combined system produced C<sub>2</sub>H<sub>4</sub> at a peak rate of  
184 1.3 mmol h<sup>-1</sup> at 120 mA cm<sup>-2</sup> (Figure 4C), along with a C<sub>2+</sub> FE of ~76% (Table S13). The  
185 system maintained the peak single-pass conversion and productivity in CO<sub>2</sub>-to-C<sub>2</sub>H<sub>4</sub> at 120 mA

186  $\text{cm}^{-2}$  for 40 hours of uninterrupted operation (Figure 4D). The full cascade system achieved  
187 carbonate-free electroproduction of  $\text{C}_2\text{H}_4$  with an energy intensity of  $138 \text{ GJ (tonne C}_2\text{H}_4)^{-1}$ , a  
188 major savings relative to the direct route ( $\sim 267 \text{ GJ (tonne C}_2\text{H}_4)^{-1}$ ) (Table S20).

189 Having established the system performance in side-by-side comparison with previous on-  
190 step  $\text{CO}_2\text{R}$  processes, we take the MEA in the cascade system a step further. We replaced the  
191 oxygen evolution reaction (OER) with the glucose electrooxidation reaction (GOR) for which  
192 the thermodynamic potential is  $\sim 1 \text{ V}$  less than that of OER.<sup>37</sup> We detected gluconate,  
193 glucuronate, glucarate, and formate – all products with values higher than that of glucose – as  
194 the major GOR products in the current density range of  $40$  to  $200 \text{ mA cm}^{-2}$  (Table S14 and  
195 Figure S22). We found that coupling the CORR and GOR in alkaline media reduces the  
196 potential requirement approximately  $1 \text{ V}$  at industrially relevant current densities (Figures 4E  
197 and S23 and Tables S15-18). At a current density of  $120 \text{ mA cm}^{-2}$ , we obtained a  $\text{C}_2\text{H}_4$  FE of  
198  $\sim 55\%$  and a  $\text{C}_{2+}$  FE of  $\sim 90\%$  at an MEA full-cell potential of  $1.27 \text{ V}$  (Figure 4E and Tables  
199 S17 and S19). This voltage reduction enables a total energy requirement of  $\sim 89 \text{ GJ (tonne}$   
200  $\text{C}_2\text{H}_4)^{-1}$ , which represents a  $35\%$  reduction in the energy consumption compared to the MEA  
201 cell using OER anode at the same current density ( $\sim 138 \text{ GJ (tonne C}_2\text{H}_4)^{-1}$ ) (Table S20). All  
202 earlier comparisons involve OER only, both in the cascade system and all reference cases. This  
203 additional GOR result highlights the potential to reduce the energy intensity of  $\text{C}_2\text{H}_4$  production  
204 further. Herein, we also note that although the anodic products – gluconate, glucuronate,  
205 glucarate, and formate – are more valuable than the glucose input, making a full economic case  
206 for the anode side upgrading would require detailed assessment of multiple separations, which  
207 is beyond the scope of this work.

208 Despite the gains demonstrated here, profitable  $\text{C}_2\text{H}_4$  electroreduction with cascade  $\text{CO}_2\text{RR}$   
209 will require further improvements in performance metrics, including selectivity, current density,

210 single pass utilization, energy efficiency – in both the first step (CO<sub>2</sub>-to-CO in SOEC) and  
211 second step (CO-to-C<sub>2</sub>H<sub>4</sub> in MEA) (Note S3 and Table S20). Further reductions in the capital  
212 and operational costs of both systems will also bring the C<sub>2</sub>H<sub>4</sub> electroproduction closer to  
213 viability (Note S3 and Table S20).

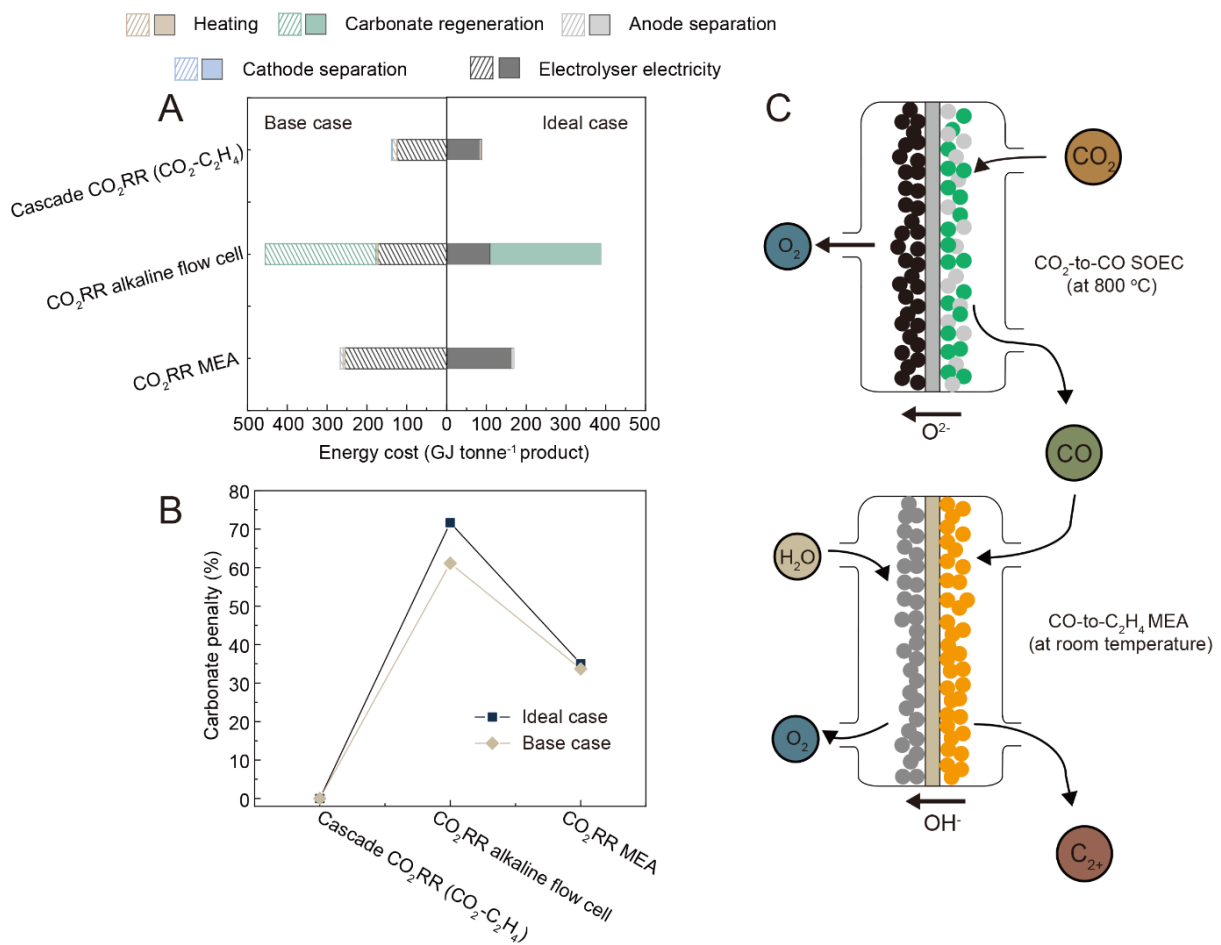
## 214 **CONCLUSIONS**

215 We developed a cascade approach to CO<sub>2</sub>-to-C<sub>2</sub>H<sub>4</sub> conversion that avoids carbonate  
216 formation and associated energy penalties, combining an SOEC with a high performance  
217 CORR MEA system designed here. We designed a layered catalyst structure composed of a  
218 metallic Cu, N-tolyl-tetrahydro-bipyridine, and SSC ionomer to achieve high-rate and efficient  
219 CO-to-C<sub>2</sub>H<sub>4</sub> conversion in a MEA electrolyser. The combined functions of each layer raised  
220 the device C<sub>2</sub>H<sub>4</sub> FE to 65%, at a full-cell C<sub>2</sub>H<sub>4</sub> EE of 28% across a broad range of current  
221 densities, versus the <50% FEs of the bare and single-layer catalyst structures. To drive an end-  
222 to-end CO<sub>2</sub> conversion process without the loss of CO<sub>2</sub> to carbonate, we paired our MEA  
223 electrolyser with a SOEC for CO<sub>2</sub>-to-CO conversion. With the CO stream produced from the  
224 SOEC, the MEA system generated C<sub>2</sub>H<sub>4</sub> at a peak rate of 1.3 mmol h<sup>-1</sup> and maintained  
225 continuous operation for 40 hours. The full cascade system required ~138 GJ (tonne C<sub>2</sub>H<sub>4</sub>)<sup>-1</sup>,  
226 achieving significant savings over the directly-comparable one-step CO<sub>2</sub>-to-C<sub>2</sub>H<sub>4</sub> route (~267  
227 GJ (tonne C<sub>2</sub>H<sub>4</sub>)<sup>-1</sup>). Having established the direct comparison with existing systems on the basis  
228 of OER anode reactions in all cases, we devised an approach to reduce the energy consumption  
229 of the MEA further, switching the OER anode to GOR. With this enhancement, the cascade  
230 SOEC-MEA system requires a total energy requirement of ~89 GJ (tonne C<sub>2</sub>H<sub>4</sub>)<sup>-1</sup>. These results  
231 demonstrate the potential to electrocatalytically convert CO<sub>2</sub> to C<sub>2</sub>H<sub>4</sub> without carbonate  
232 production and associated energy penalties. The result is a record-low energy requirement for  
233 the production of the world's most-produced organic compound.

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**FIGURES**

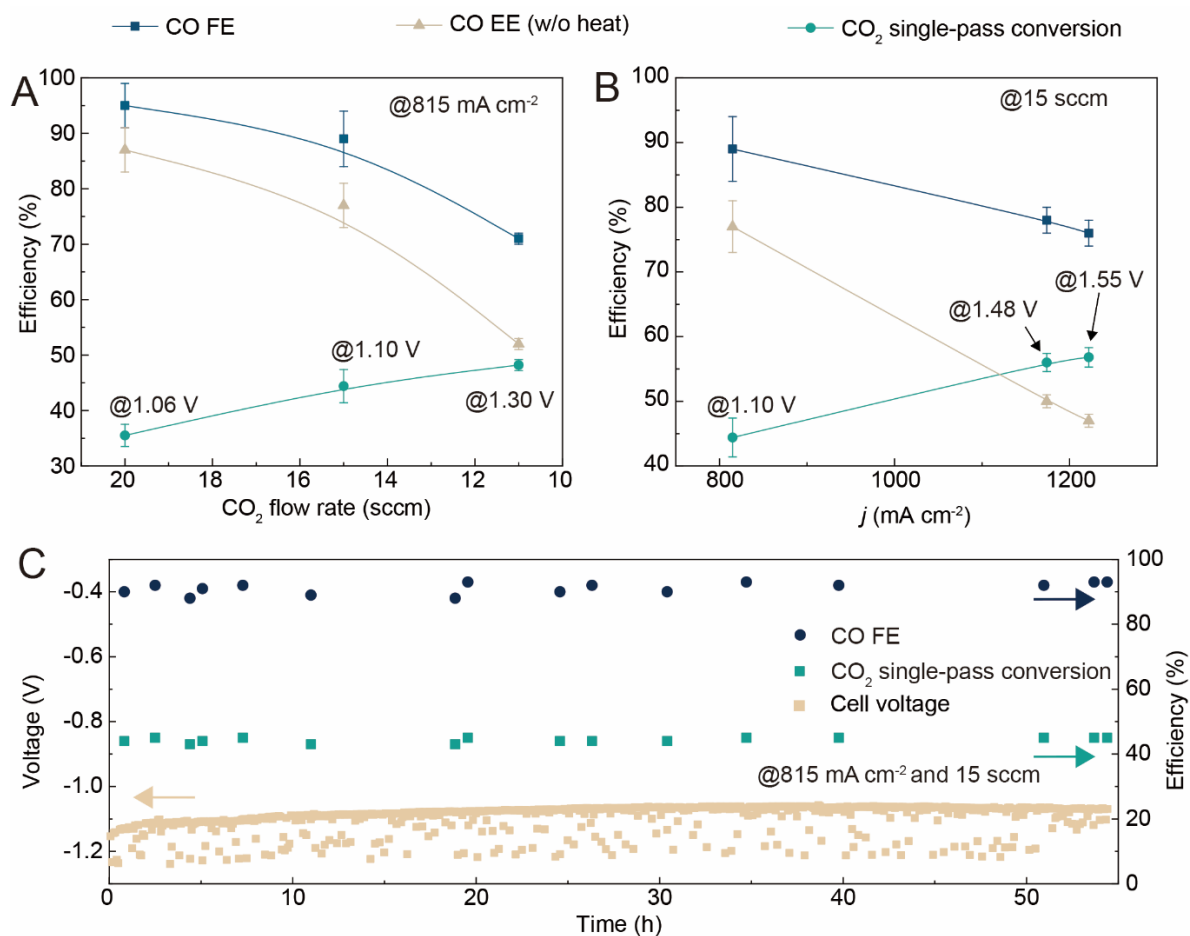


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**Figure 1. Carbonate-formation-free CO<sub>2</sub>-to-C<sub>2</sub>H<sub>4</sub> production through cascade CO<sub>2</sub>RR.**

246 (A) Comparison of energy consumption for C<sub>2</sub>H<sub>4</sub> production in various systems. (B) The  
 247 carbonate penalty (i.e., the fraction of energy consumption due to carbonate formation) in the  
 248 various systems. TEA calculation details are provided in the supplementary information. (C)  
 249 A schematic illustration of renewable CO<sub>2</sub>-synthesized C<sub>2</sub>H<sub>4</sub> in a combined system consisting  
 250 of a CO<sub>2</sub>-to-CO SOEC and a CO-to-C<sub>2</sub>H<sub>4</sub> MEA.

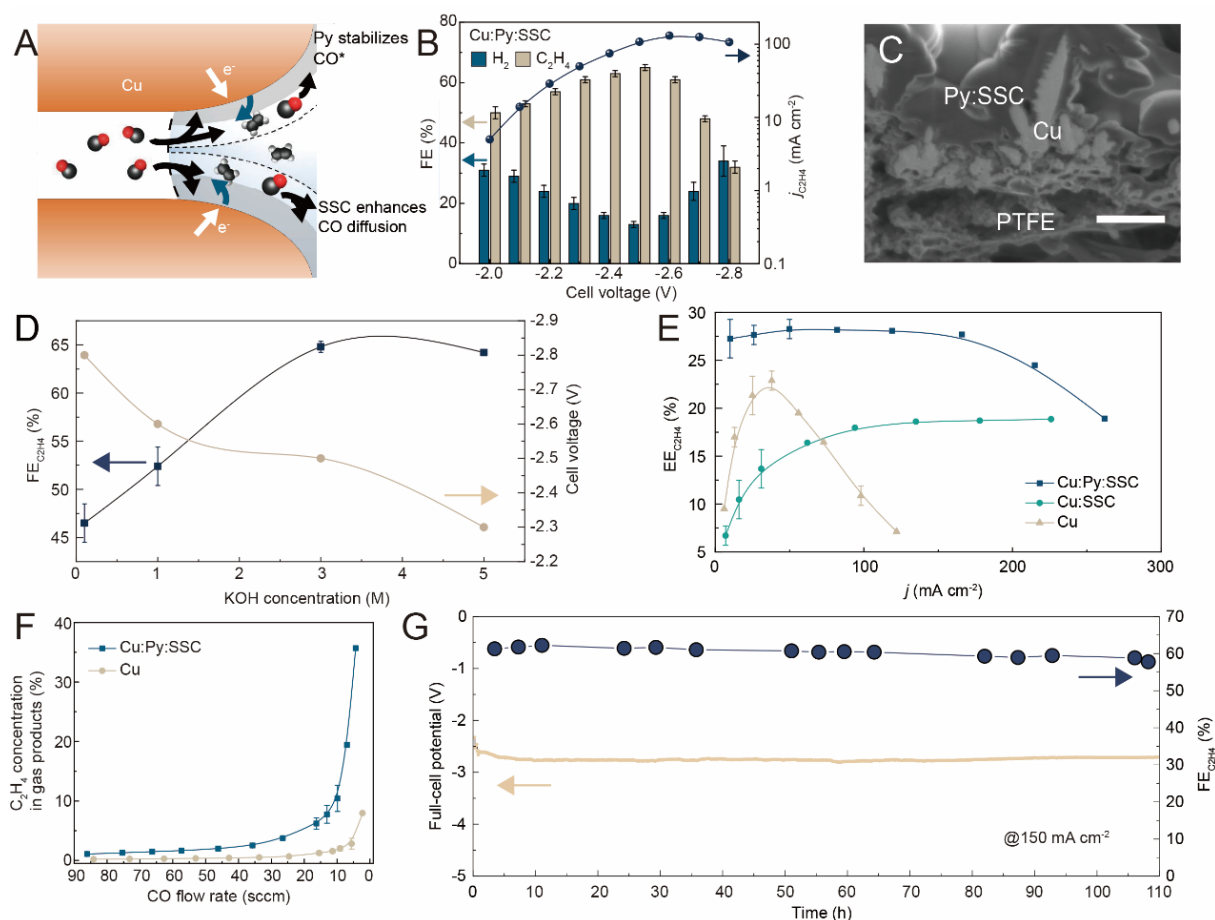
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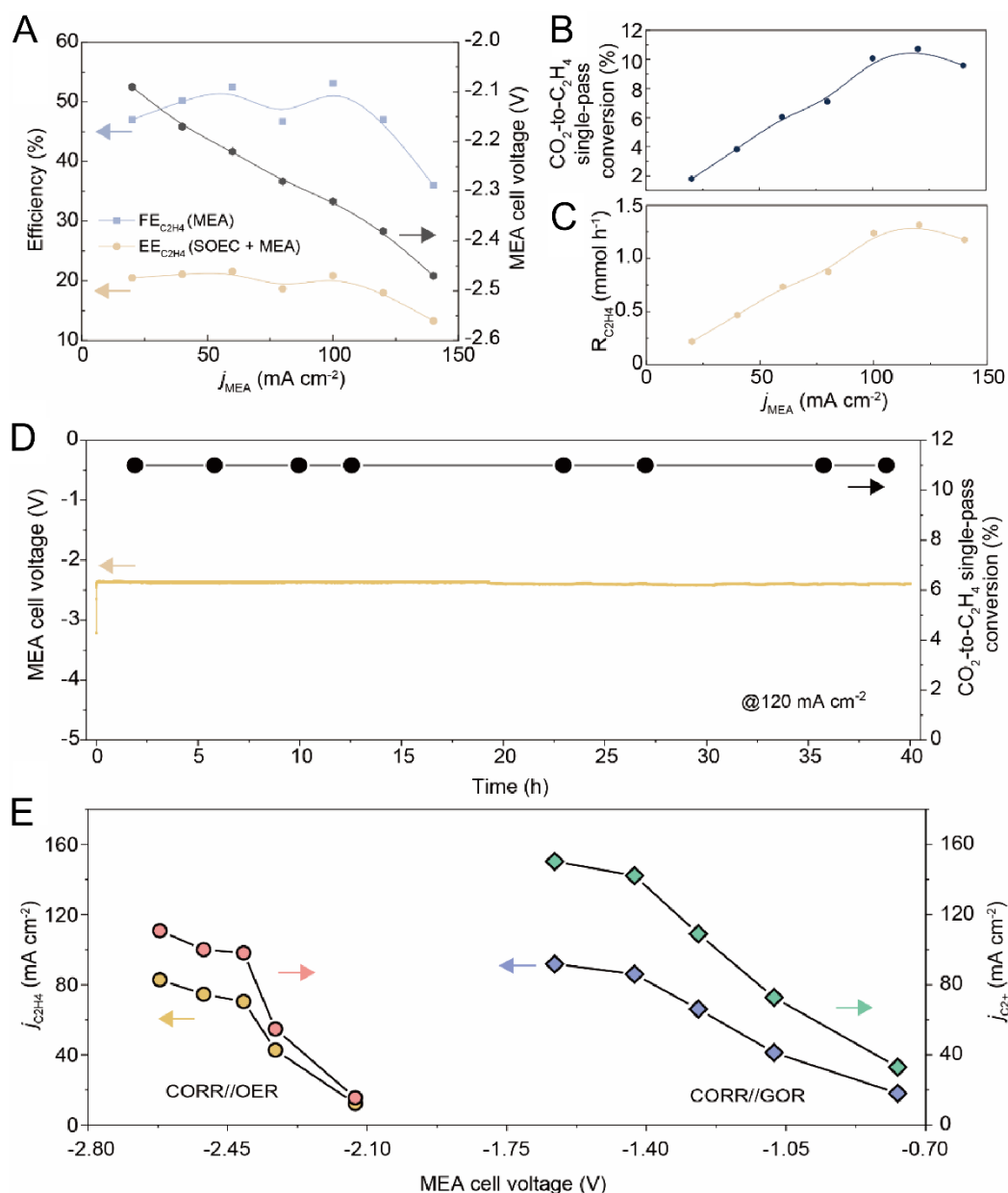
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253 **Figure 2. CO<sub>2</sub>-to-CO conversion in an SOEC.** (A,B) CO<sub>2</sub>-to-CO Faradaic efficiency, single-  
 254 pass conversion, and energy efficiency in a commercial 2.5-cm NiO-YSZ/YSZ/GDC/LSC at  
 255 various CO<sub>2</sub> flow rates and current densities. The increase in the CO<sub>2</sub> single-pass conversion  
 256 by lowering CO<sub>2</sub> flow rates or increasing current density was caused by the CO  
 257 disproportionation reaction, which is also known as the Boudouard reaction. (C) The CO<sub>2</sub>-to-

258 CO Faradaic efficiency, single-pass conversion, and cell voltage profiles during 55-hour test at  
 259 815 mA cm<sup>-2</sup> and a CO<sub>2</sub> flow rate of 15 sccm. The operating temperature is 800 °C. The error  
 260 bars correspond to the standard deviation of three independent measurements.



261  
 262 **Figure 3. CO-to-C<sub>2</sub>H<sub>4</sub> electroreduction in an MEA. (A,B)** Introducing additives to improve  
 263 CO diffusion and stabilize CO\* intermediates leads to enhanced C<sub>2</sub>H<sub>4</sub> selectivity and activity.  
 264 **(C)** Cross-sectional SEM images of the Cu:Py:SSC catalyst. The scale bar is 1 μm. **(D)** The  
 265 C<sub>2</sub>H<sub>4</sub> FE and full-cell voltages in different electrolytes. **(E,F)** Comparisons of the CO-to-C<sub>2</sub>H<sub>4</sub> EE  
 266 and the C<sub>2</sub>H<sub>4</sub> concentration obtained using the Cu:Py:SSC catalyst and controls in MEAs with  
 267 3 M KOH. **(G)** C<sub>2</sub>H<sub>4</sub> FE and full-cell voltage of the MEA equipped with a Cu:Py:SSC cathode  
 268 for 110 hours at 150 mA cm<sup>-2</sup>. The error bars correspond to the standard deviation of three  
 269 independent measurements.



270

271 **Figure 4. C<sub>2</sub>H<sub>4</sub> production performance in the cascade CO<sub>2</sub>RR. (A)** The C<sub>2</sub>H<sub>4</sub> FE and cell  
 272 voltage of the CO-to-C<sub>2</sub>H<sub>4</sub> MEA in the cascade CO<sub>2</sub>RR, and the C<sub>2</sub>H<sub>4</sub> EE of the cascade  
 273 CO<sub>2</sub>RR. **(B,C)** CO<sub>2</sub>-to-C<sub>2</sub>H<sub>4</sub> single-pass conversion and C<sub>2</sub>H<sub>4</sub> production rates of the cascade  
 274 CO<sub>2</sub>RR at different operating current densities for the CO-to-C<sub>2</sub>H<sub>4</sub> MEA. **(D)** Extended CO<sub>2</sub>-  
 275 to-C<sub>2</sub>H<sub>4</sub> single-pass conversion performance of the MEA in the cascade CO<sub>2</sub>RR. **(E)** Effect of  
 276 anodic reaction on the CORR performance metrics of the MEA in the cascade CO<sub>2</sub>RR.

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278 **ACKNOWLEDGMENTS**

279 The authors acknowledge Ontario Centre for the Characterization of Advanced Materials  
280 (OCCAM) for sample preparation and characterization facilities. Funding: This work received  
281 financial support from the Ontario Research Foundation: Research Excellence Program, the  
282 Natural Sciences and Engineering Research Council (NSERC) of Canada, the CIFAR Bio-  
283 Inspired Solar Energy program and TOTAL S.E. and the Joint Centre of Artificial Synthesis,  
284 a DOE Energy Innovation Hub, supported through the Office of Science of the US Department  
285 of Energy under award no. DE-SC0004993. D.S. acknowledges the NSERC E.W.R Steacie  
286 Memorial Fellowship. A.T. acknowledges Marie Skłodowska-Curie Fellowship H2020-  
287 MSCA-IF-2017 (793471). The authors thank Dr. Y.-F. Liao for the GIWAXS measurements  
288 at Spring-8 BL-12B2 beamline of NSRRC. The authors also thank Dr. T. Regier for their  
289 assistance at the SGM beamline of CLS.

290 **AUTHOR CONTRIBUTIONS**

291 D.S. and E.H.S. supervised the project. A.O. carried out all the electrochemical experiments  
292 with advice from Y.W. and F.L.. A.T., A.R.H., J.C.P., and T.A. designed and synthesized the  
293 N-tolylpyridinium molecule and contributed to the manuscript editing. A.O. and F.L. carried  
294 out Raman spectroscopies. Y.W. performed the SEM and TEM analysis. A.O. performed the  
295 nuclear magnetic resonance spectroscopies. A.O. and Y.W. co-wrote the manuscript. J.S.  
296 performed the TEA modelling. T.B. conducted the CO diffusion modelling. M.L., Y.L. and  
297 H.Y. contributed to the discussions and manuscript editing. All authors discussed the results  
298 and assisted during manuscript preparation.

299 **DECLARATION OF INTERESTS**

300 The authors declare no competing interests.

301 **DATA AVAILABILITY**



302 The data supports the plots within this paper and other findings of this study are available from  
303 the corresponding authors upon reasonable request.

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