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Negative nonlinear damping of a multilayer graphene mechanical resonator

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We experimentally investigate the nonlinear response of a multilayer graphene resonator using a superconducting microwave cavity to detect its motion. The radiation pressure force is used to drive the mechanical resonator in an optomechanically induced transparency configuration. By varying the amplitudes of drive and probe tones, the mechanical resonator can be brought into a nonlinear limit. Using the calibration of the optomechanical coupling, we quantify the mechanical Duffing nonlinearity. By increasing the drive force, we observe a decrease in the mechanical dissipation rate at large amplitudes, suggesting a negative nonlinear damping mechanism in the graphene resonator. Increasing the optomechanical backaction further, we observe instabilities in the mechanical response.

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The unique properties of graphene such as atomic thickness, low mass density, and high modulus of rigidity make it very attractive material for nanoscale electromechanical systems (NEMS) for several technological applications. After the first demonstration of a few layers thick graphene NEMS [1], there have been extensive studies on graphene nanoelectromechanical systems ranging from electromechanical resonators [2,3], oscillators [4], and optomechanical systems aiming to probe the quantum regime of graphene motion [5–8]. In this pursuit, large mechanical quality factors in graphene-based NEMS have been demonstrated as well [5,9]. Due to its atomic thickness, graphene-based NEMS also exhibit rich nonlinearity such as onset of Duffing nonlinearity and nonlinear damping at relatively small mechanical amplitudes [9–11]. These properties further make graphene an attractive candidate for developing optomechanical systems to reach the quantum regime of graphene motion [12], to store microwave photons [13], and could possibly be useful to understand dissipation in graphene NEMS for improved device performance [14].

The coupling between mechanical resonator and optical/superconducting microwave cavities has enabled the detection of mechanical motion with excellent sensitivities [15–17], offering an attractive platform to characterize the nonlinear response of mechanical resonators. In this paper, we study nonlinear dynamics of a multilayer graphene resonator by means of coupling it to a superconducting microwave cavity. The graphene resonator is driven by injecting two microwave tones in the cavity, which are detuned by the mechanical resonant frequency leading to an oscillating radiation pressure force which drives the mechanical resonator. By changing the amplitude of these tones, we can independently control the driving force and dissipation due to the optomechanical backaction forces. We drive the mechanical resonator into the Duffing regime and characterize the nonlinearity. With increase in the driving force, we observe a reduction in linear dissipation rate, large hysteresis with sweep direction, and an instability in the mechanical amplitude.

Our device consists of a multilayer graphene resonator coupled to a superconducting microwave cavity as studied previously [5,18], fabricated using the mechanical exfoliation technique. Figure 1(a) shows a scanning electron microscope image of a multilayer graphene resonator coupled to a superconducting microwave cavity. The multilayer graphene mechanical resonator is 10 nm thick and is suspended above a gate electrode of the microwave feedline by approximately 150 nm. Additional information about the device characterization is provided in the Supplemental Material [18]. The superconducting cavity is in a quarter wavelength coplanar waveguide geometry fabricated with an alloy of molybdenum and rhenium ($T_c \approx 9$ K) on an intrinsic silicon substrate [19]. The measurements are performed in a dilution refrigerator under vacuum at 14 mK. The superconducting cavity has a resonance frequency of $\omega_c = 2\pi \times 5.90054$ GHz, with an internal dissipation rate $\kappa_i = 2\pi \times 54$ kHz and coupled to a feedline with an external coupling rate $\kappa_e = 2\pi \times 188$ kHz (coupling fraction $\eta = \frac{\kappa_e}{\kappa (= \kappa_e + \kappa_i)} = 0.78$). The graphene resonator forms a mechanically compliant capacitor to the microwave feedline as shown schematically in Fig. 1(b). The motion of the graphene resonator modulates the capacitance and hence the cavity frequency. The graphene resonator has a resonance frequency of $\omega_m = 2\pi \times 36.233$ MHz. Using thermal noise, we calibrate the optomechanical coupling, defined as $g_0 = \frac{d\omega_c}{dx} x_{zpf}$, where x_{zpf} are the quantum zero-point fluctuations of the mechanical resonator, to be $2\pi \times 0.83$ Hz [5], which also provides an absolute calibration of displacement amplitudes.

In order to probe the mechanical response, we take advantage of the optomechanical coupling and sideband-resolved limit ($\omega_m \gg \kappa$) in an optomechanically induced transparency (OMIT) setup. In an OMIT setup, two microwave fields are injected inside the cavity. A strong drive field p_{drive} at lower mechanical sideband frequency $\omega_d = \omega_c - \omega_m$ and a weak probe field p_{probe} measure the cavity response by sweeping the probe tone in the vicinity of ω_c . When the detuning between drive and probe fields $\Omega = \omega_p - \omega_d$ matches ω_m , the mechanical resonator experiences coherent oscillating radiation pressure force with an amplitude given by $(\frac{4\eta g_0 \sqrt{n_p n_d}}{\omega_m}) m \omega_m^2 x_{zpf}$, where n_d (n_p) is the number of drive

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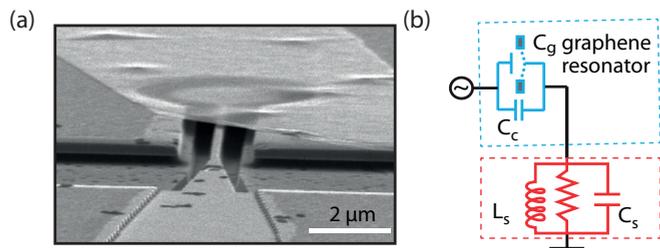


FIG. 1. (a) A scanning electron micrograph of a multilayer graphene (10 nm thick) drum-shaped resonator coupled to a superconducting microwave cavity (not shown here). Graphene resonator is suspended 150 nm above the bottom gate electrode (adapted from Ref. [5]). (b) Schematic diagram of the device: graphene resonator couples external microwave radiation to the cavity by forming a coupling capacitor.

(probe) photons and m is the mass of the resonator. The resulting oscillating response of the mechanical resonator to the radiation pressure force up-scatters the drive field exactly at ω_p leading to an interference with the original probe field measuring the cavity response. This phenomenon is called optomechanically induced transparency (OMIT) [20,21] as described schematically in Fig. 2(a). It is worth pointing out that unlike heterodyne mixing schemes with low-frequency RF drive, the radiation pressure force drive eliminates the need to apply a dc gate voltage. Furthermore, while the strength of the probe tone allows us to control the driving force on the mechanical resonator, independently the drive tone can be used to tune the dissipation in the mechanical resonator using the optomechanically backaction.

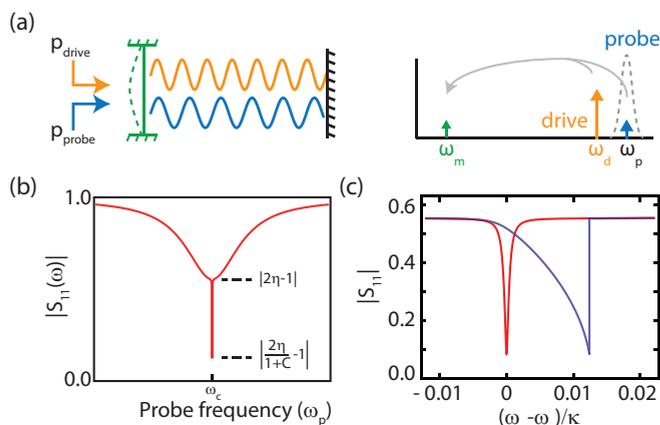


FIG. 2. (a) Schematic showing the idea of radiation pressure driving. Due to the optomechanical coupling, driving the cavity with a strong tone near $\omega_d = \omega_c - \omega_m$ and a weak probe tone ω_p near ω_c exerts a radiation pressure force on the mechanical resonator at ω_m . The strength of radiation pressure force is controlled by the product of probe tone and the drive tone amplitudes. (b) Illustration of the cavity reflection coefficient in the presence of a strong sideband drive. The optomechanical interaction produces an absorption feature in the cavity response. (c) A zoomed-in view of the theoretically expected OMIT feature of a mechanical resonator that includes a Duffing nonlinearity in the linear and nonlinear regimes.

For an overcoupled single-port cavity, the interference between the probe field and upconverted field (drive being at lower motional sideband) leads to an absorption feature at low driving powers as shown schematically in Fig. 2(b). In the linear response limit, the resulting reflection coefficient of the cavity can be written as $S_{11}(\omega) = 1 - \eta\kappa \frac{\chi_c}{1+g^2\chi_m\chi_c}$, where $\chi_m(\omega) = \frac{1}{-i(\Omega-\omega_m)+\gamma_m/2}$ is the susceptibility of the mechanical resonator, $\chi_c = \frac{1}{-i(\Omega-\omega_m)+\kappa/2}$ is the susceptibility of the cavity, γ_m is the mechanical dissipation rate, $g = g_0\sqrt{n_d}$ is the many-photon optomechanical coupling strength, and n_d is the number of the drive photons. In the limit $\kappa \gg 2g \gg \gamma_m$, the measurement of the optomechanically induced absorption (OMIA) allows to directly probe the responsivity of the mechanical resonator giving its amplitude and dissipation rate, thus making it a sensitive technique.

For a red-sideband drive $\omega_d = \omega_c - \omega_m$, the minimum value of the reflection coefficient is given by much simplified expression $|\frac{2\eta}{1+C} - 1|$, where optomechanical cooperativity C is defined as $C = \frac{4g_0^2 n_d}{\gamma_m \kappa}$. In the limit of no optomechanical coupling ($C = 0$), we recover the $|2\eta - 1|$ expression for the minimum for a single-port reflection cavity, which sets the base line of OMIA feature. The linewidth of absorption feature is given by $(1+C)\gamma_m$, where the additional term $C\gamma_m$ originates from the backaction effects of drive photons and can be tuned by n_d . Amplitude of the mechanical resonator can also be cast into a convenient form, $x = x_{zpf}(\frac{C}{1+C})(\frac{\kappa_e}{g})\sqrt{n_p}$. It is instructive to see that for low cooperativity ($C < 1$), the mechanical amplitude can be tuned by both the probe and drive tone as $x \propto \sqrt{n_d n_p}$. On the other hand, in the limit $C > 1$, the mechanical amplitude is proportional to $\sqrt{\frac{n_p}{n_d}}$, suggesting that an increase in drive field leads to optomechanical damping and hence a reduction in the mechanical amplitude. Although the depth of the OMIT dip in the reflection coefficient does not depend on the probe power, the mechanical force of the resonator does: increasing the probe power for a fixed drive power will exert a larger oscillating force on the resonator, and can be used to drive it into the nonlinear regime, as illustrated in Fig. 2(c).

In Fig. 3, we probe the OMIA response in detail by varying the number of intracavity probe photons, hence the driving force, while keeping the number of drive photons fixed at $n_d = 2.5 \times 10^7$ ($C \sim 0.40$) and 1.0×10^8 ($C \sim 1.24$). At low number of probe photons, the OMIA feature is determined by the linear response of the mechanical resonator. As n_p is increased further, the nonlinearity in the OMIA response becomes evident with a stiffening of the mechanical resonator (positive shift in the resonance frequency) and the shark-fin-like Duffing response accompanied by hysteresis with respect to frequency sweep direction.

In addition to the clear Duffing response, with the exception of the bottom two curves, it can also be seen that the OMIA dip on the nonlinear regime becomes deeper. Qualitatively, the observation of a deeper OMIA dip when n_p is increased can be understood from a reduction of the mechanical damping rate as the resonator is driven to larger amplitudes. Such a decreased mechanical damping rate would give a larger cooperativity and thus a deeper OMIA dip. In the last two curves, the cooperativity is continuing to increase, but the

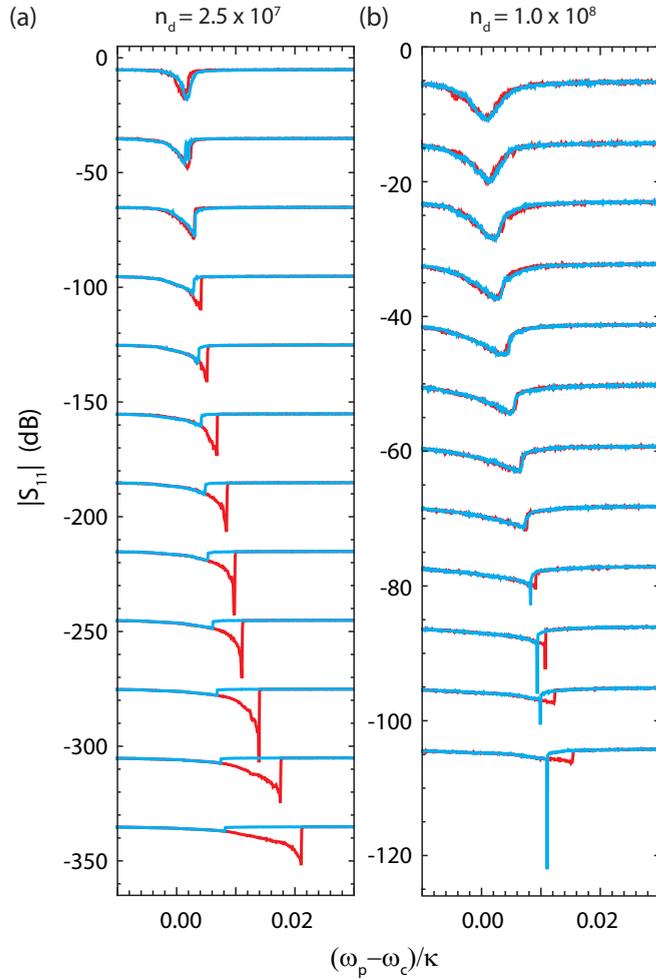


FIG. 3. Forward (red) and reverse (cyan) frequency sweep measurement of OMIA feature of the multilayer graphene drum showing mechanical response at various probe and drive powers. The probe photons are swept from $n_p = 2.5 \times 10^5$ to 3.14×10^6 in 1 dB steps (top to bottom). Number of drive photons n_d is fixed at 2.5×10^7 ($C \sim 0.40$) for panel (a) and 1.0×10^8 ($C \sim 1.24$) photons for panel (b). The evolution of nonlinear response accompanied by the hysteresis can be clearly seen as probe power is increased (top to bottom). Panel (b) shows instability points as sharp dips appearing at large probe power. For clarity, measurements in (a) and (b) are plotted with offsets of -30 dB and -9 dB, respectively.

OMIA dip becomes less deep as the cavity has now crossed over to an effective undercoupled regime (see supplementary information of Ref. [5] for more details). In addition to the deeper OMIA dip that is suggestive of a decreased mechanical damping at higher drive forces, Fig. 3 also shows additional features. Comparing panels (a) and (b), smaller and larger n_d , respectively, the mechanical linewidth in panel (b) is significantly larger. This is a consequence of increased optomechanical damping, which also explains the absence of hysteresis and shows only a transition to a Duffing response at higher powers [22]. Finally, in panel (b), at the highest drive forces, we also observe an instability in the response in the form of a spike in reverse frequency sweep.

To gain quantitative insight into these observations, we perform numerical fits on the data shown in Fig. 3. The

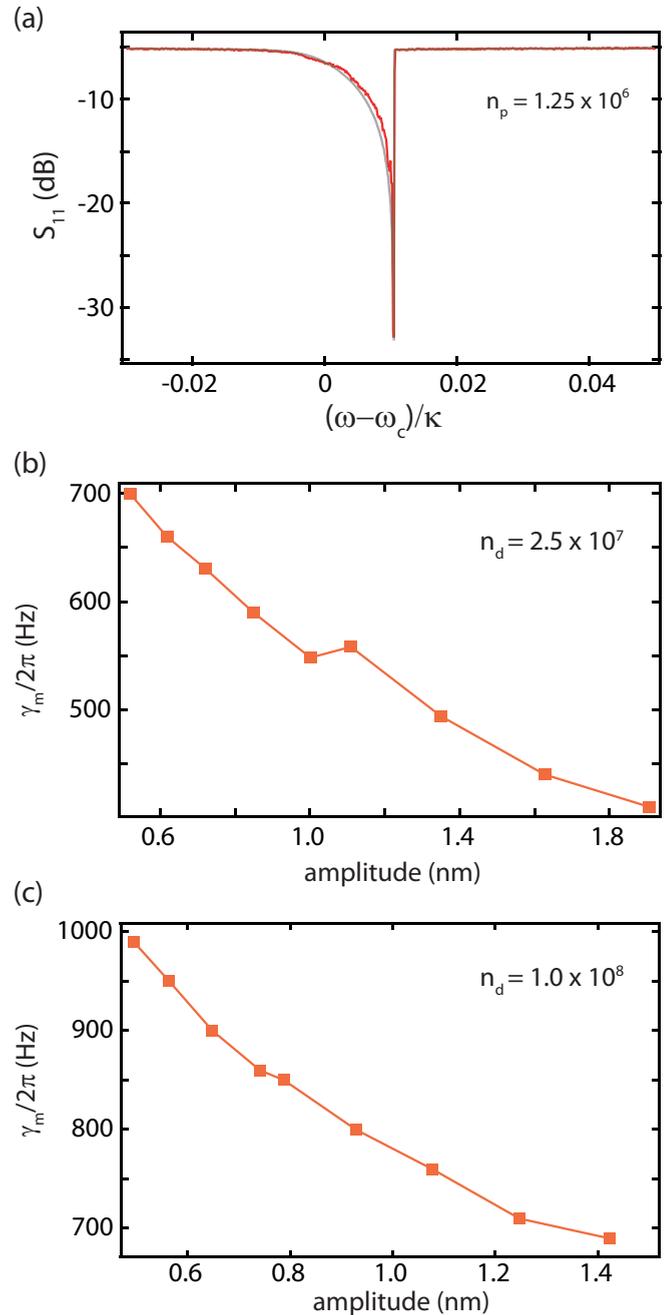


FIG. 4. (a) Measurement of S_{11} showing strong nonlinear response (red curve) together with numerically fitted curve (gray) for $n_d = 2.5 \times 10^7$. (b), (c) Extracted linear dissipation rate γ_m plotted against mechanical amplitude for $n_d = 2.5 \times 10^7$ and for 1.0×10^8 , respectively.

nonlinear response can be primarily captured by including a Duffing term αx^3 in the restoring force of the mechanical resonator [23]. Following Ref. [23], we perform numerical fits to extract the linear mechanical dissipation rate (γ_m), mechanical amplitude (x_0), and the Duffing parameter (α) for any given probe and drive power. The gray curve in Fig. 4(a) is the numerical fitted curve overlaid on top of the experimentally measured data allowing us to extract the Duffing parameter to be $\alpha = 2.3 \times 10^{15} \text{ kg m}^{-2} \text{ s}^{-2}$. Using the analytical expression

for the onset of the Duffing bifurcation point $\omega_{up} = \omega_m + \frac{3}{8} \frac{\alpha}{m_{eff} \omega_m} (x_{up}^2)$, we get $\alpha = 2.5 \times 10^{15} \text{ kg m}^{-2} \text{ s}^{-2}$, which is close to the result we get by performing numerical fits. It should be noted that in the expression of the Duffing parameter for a given driving force, the mechanical quality factor enters through the amplitude of the resonator at the bifurcation point. Figures 4(b) and 4(c) plot the linear damping rate with the amplitude of the resonator extracted by performing numerical fits on the data sets shown in Fig. 3. At low amplitude, we observe mechanical damping rates γ_m of $2\pi \times 700 \text{ Hz}$ ($Q_m = 51\,760$) for $n_d = 2.5 \times 10^7$, while for higher amplitude, the damping rate drops to $2\pi \times 410 \text{ Hz}$ ($Q_m = 88\,373$). Similar observations are made for a second thinner device. The data from the second device are shown in the Supplemental Material [18]. At large number of probe photons, the nonlinear dynamics of the OMIA becomes far more complex. Apart from the nonlinear Duffing response accompanied by the hysteresis, we observe instabilities (single-pixel jumps in absorption) in the reverse frequency sweep shown in Fig. 3(b). While instabilities such as self-oscillation can arise with blue-sideband driving, they are normally not expected for the red-sideband driving performed here, and are also not found in the model we use for fitting [23]. Qualitatively, the instabilities seem to coincide with the switching out of the low-amplitude state. Aside from these instabilities, however, the model does capture well the response for these traces.

The decrease in observed damping rate at higher amplitudes suggests the presence of nonlinear damping terms with negative coefficients (such as $\rho|x|\dot{x}$, $\mu x^2 \dot{x}$, $\lambda \frac{\dot{x}}{1+|x|}$) in the equation of motion of the mechanical resonator [23]. It should be noted that the total damping however remains positive. The fact that the extracted effective driving linear damping shown in Fig. 3 does not follow a quadratic dependence on the driving amplitude as expected for a term proportional to $\mu x^2 \dot{x}$ implies that a nonlinear damping of the form more similar to $\rho|x|\dot{x}$ applies in this range of driving amplitudes. As this negative nonlinear damping occurs also at low cooperativities, and as it is not seen in the theoretical calculations treating the optomechanical nonlinear response, we do not believe that it is an optomechanical effect, but instead intrinsic to the mechanical resonator. The amplitude-dependent negative damping could further give rise to the observed instabilities seen in Fig. 3(b). There have been also observations of nonlinear damping in nanomechanical resonators [24] and carbon-based resonators [9]. One possible source of negative

nonlinear damping is the saturation of two-level systems coupled to the mechanical resonator [25,26]. At low drive powers, these two-level systems can absorb energy from the mechanical resonator, increasing the mechanical damping rate. At higher powers, the two-level systems (TLSs) become saturated, and the damping rate goes down. Such a process was suggested as an explanation of power-dependent attenuation losses in glasses [27–29], and also was used to describe power-dependent dielectric losses in superconducting electrical resonators [30]. For such a saturation result in nonlinear damping effects, the level spacing of the TLSs should be larger than the bath temperature. In order for TLSs to describe the negative nonlinear damping observed here, the coupling between the TLSs and the mechanical resonator would have to be nonresonant, mediated by strong higher order processes.

We also note that resonators driven in the bifurcated regime can be very sensitive to environment noise that can induce premature switching from the high- to the low-amplitude branch [31], something not captured by our theoretical model. We note, however, that in our measurements, such switching would make the OMIA dips appear less shallow, and lead to an underestimation of the coefficient of the negative nonlinear damping rate, and therefore our measurements represent a lower bound on the magnitude of the negative nonlinear damping.

In conclusion, we examined the nonlinear dynamics of a graphene resonator coupled to a superconducting microwave cavity. In the linear response limit, optomechanically induced transparency measurements easily allow us to extract the linear damping rate and peak amplitude. At moderate driving force when the response becomes nonlinear, we perform numerical fits by including a Duffing term in the mechanical restoring force and find $\alpha \approx 2.3 \times 10^{15} \text{ kg m}^{-2} \text{ s}^{-2}$. Increasing the driving force further, the OMIA response becomes complex and it is no longer captured by the Duffing term. At these large amplitudes, the nonlinearities start becoming relevant and make the mechanical damping rate appear low at larger amplitudes, where we observe the phenomenon of negative nonlinear damping in a mechanical resonator.

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