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Article

Intersection Sight Distance Characteristics of Turbo Roundabouts

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Abstract: A turbo roundabout uses spiral circulatory roads for effectively counteracting the problems faced in modern multilane roundabouts. First developed in 1996, the turbo roundabout has an advantage over the conventional roundabout regarding capacity and safety. Turbo roundabouts are still in the developing phase in North America, but even in the European subcontinent where they exist in large numbers, reliable analytical studies on the critical parameters of roundabout visibility are lacking. Visibility (sight distance) helps to shape the geometry of the intersection and aids in safety. This paper presents the mathematical characteristics of the intersection geometry and intersection sight distance (ISD) of the turbo roundabout. Mathematical formulas are presented for the sight distance from the approaching vehicle to the conflicting-entering and circulating vehicles. The maximum lateral clearances to the conflicting vehicles are derived using mathematical optimization. The developed analytical method is verified graphically using AutoCAD. To assist in practical applications, design aids for the maximum lateral clearance are presented. The presented method and design aids should aid in promoting safety at turbo roundabouts.



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Keywords: turbo roundabout; intersection sight distance; road safety; lateral clearance

1. Introduction

Transportation organizations have been struggling to cope with traffic congestion and delay resulting from conventional signalized and un-signalized intersections. Public resistance initially hindered switching over to these safer options in North America, but it has rapidly progressed in replacing the signalized intersections with small diameter- roundabouts in the last two decades [1]. Roundabouts became popular due to their highly safe traffic operations compared to signalized intersections. They brought advantage in safety, delay, emissions, and fuel savings. In understanding the impacts of roundabouts, numerous research studies have been conducted over time, including performance comparison of turbo and conventional roundabouts [2], single-lane roundabouts [3], safety standards for turbo roundabouts [4], safety at roundabouts with traffic signals [5], turbo roundabouts in comparison to two-lane roundabouts [6], urban scenarios [7], and formulating design principles for turbo roundabouts [8,9].

From the previous studies [10,11], most roundabouts manage traffic operations entirely well on single lanes. However, degradation in safety and capacity standards are reported [12,13] when single-lane roundabouts are converted into multi-lane roundabouts to cater to the increased traffic congestion. The most significant problem with a multilane roundabout is that it has 16 conflict points that ultimately decrease traffic safety. Moreover, the vehicle sideswipe collisions increase at multilane roundabouts compared to single lane roundabouts due to an increase in the curvature of the vehicle path, hence making them more prone to property damage only collisions [14]. In addition, there is a maneuvering

problem for drivers who want to exit from the left-hand access lane as they need to change lanes over a very short distance at the roundabout and the situation becomes worse if the roundabout has two exit lanes. Another principal maneuvering problem is that the drivers behind the vehicle near the exit have no idea whether the driver ahead will take an exit or will continue through the roundabout. In addition, there is a problem of inner lane usage that negatively affects roundabout capacity [15]. Other driving behaviour challenges faced at multilane roundabouts are that drivers fail to maintain lane positions in multilane roundabouts and often take exits from the incorrect lane [16].

To address the problems of multi-lane roundabouts, designers have devised many solutions such as flower roundabouts [17], compact-semi-two-lane roundabouts [18], target roundabouts [19], and turbo roundabouts [20]. The best solution for the multi-lane intersection was found with the provision of turbo roundabouts. In turbo roundabouts, a reduction of 40% to 50% was observed for potential accidents, where injuries were decreased by 20% to 30% [21]. In addition, the best type of turbo roundabout is the one with raised traffic lane dividers that further reduce collision rate [15]. In turbo roundabouts, traffic streams flow separately even before the entry into the roundabout, where they occupy separate lanes throughout the roundabout. In addition, traffic flows run separately at the exit from the roundabout [22].

To the authors' knowledge, analytical modelling of sight distance of turbo roundabouts has not been addressed in the literature. This paper presents the mathematical characteristics of turbo roundabouts and analytical models of the intersection sight distance (ISD) that assist as handy tools during the design compared to the traditional graphical approach. General analytical models for lateral clearance at multi-lane turbo knee roundabouts to the circulatory and entering vehicles are developed. The models are developed for two cases. The first case (Case 1) corresponds to an approaching vehicle at 15 m from the yield line and the second case (Case 2) corresponds to an approaching vehicle at the yield line. The developed method is validated graphically using AutoCAD and its application is illustrated using a numerical example.

2. Geometric Characteristics

2.1. Design of Circulatory Roadway

Turbo Roundabout is a spiral circulatory roadway in which the radius increases after every interval [6]. The interval is defined by the translation axis which is at angle θ_t from the y -axis, as shown in Figure 1. The study by Murphy [23] suggests that the angle of translation axis should depend on the swept path of the vehicle and should be applied iteratively. The geometry of a knee-type roundabout with an initial radius R_1 and a primary translation axis is shown in Figure 2. Note that a knee type roundabout is a regular roundabout, except that it includes a bypass lane. The advantage of the bypass lane is that it offers more capacity in turbo roundabouts since capacity is generally less in turbo roundabouts compared to conventional multilane roundabouts [24]. The procedure of the transition from the turbo-block to turbo roundabout consists of adding a truck-apron and approach legs. By constructing the width of the apron according to the Dutch guidelines, a shift is observed between the inner and outer truck aprons [25,26]. This shift is applied by a constant m . The width of a circulatory roadway is denoted by W_c . In all the given templates of the turbo block including knee-type turbo roundabouts, the value inner radius R_1 is defined based on the area of the intersection. The width of circulatory roadway W_c depends on the swept path of the vehicle. Using R_1 , W_c , and m , the radius for other consecutive circles can be formulated. Since $2R_2 - 2R_1 = W_c + m$, the radius of other circles is given by

$$R_2 = \frac{W_c + m + 2R_1}{2} \quad (1)$$

where R_2 denotes the radius of the second consecutive semi-circle with centre n (m), R_1 denotes the turbo roundabout initial radius with centre O_1 (m), W_c denotes the circulatory

roadway width (m), and m denotes the shift between inner and outer apron (m), as shown in Figure 2.

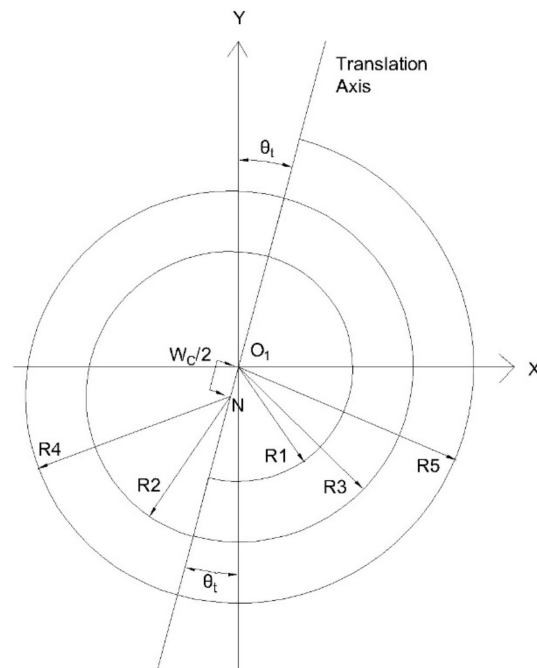


Figure 1. Design of the circulatory roadway.

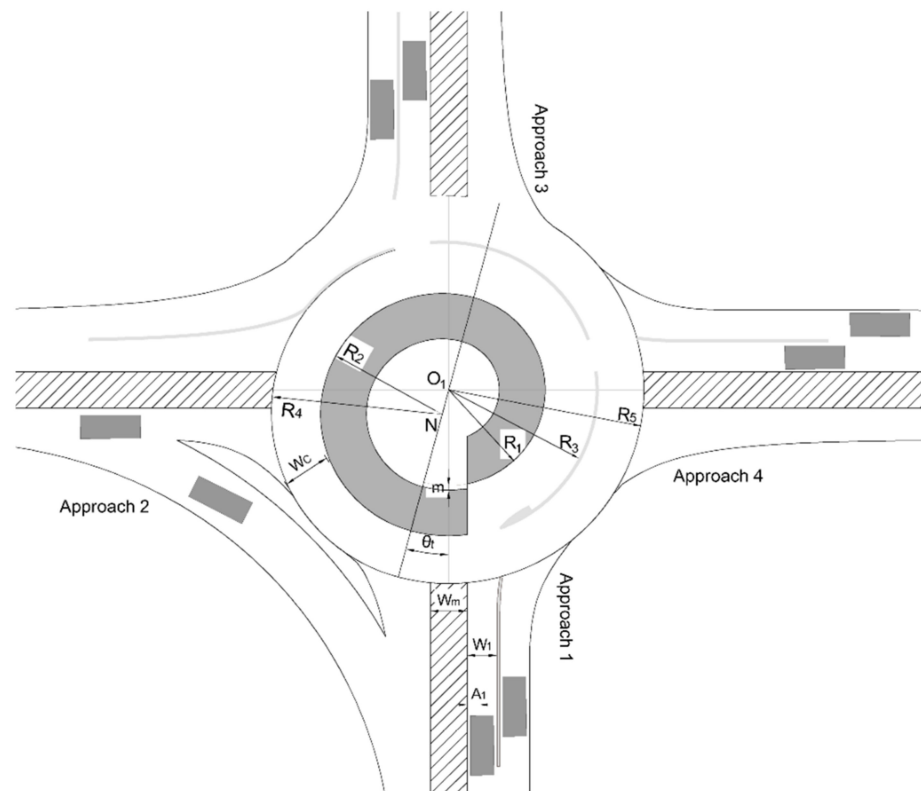


Figure 2. Geometry of the modified turbo roundabout.

Similarly, the radius of the next semicircle is determined by replacing R_2 with R_3 and R_1 with R_2 . This process continues to find the next radius and so on. In general, Equation (1) can be generalized as

$$R_{n+1} = \frac{W_c + m + 2R_n}{2} \tag{2}$$

where R_n denotes the radius of the semicircle of turbo roundabout with centre O_1 and R_{n+1} denotes the radius of next consecutive semi-circle of turbo roundabout with centre N . From Figures 1 and 2, the coordinates of the new center N are given by

$$x_N = (O_1N) \sin \theta_t = \frac{W_c}{2} \sin \theta_t \tag{3}$$

$$y_N = (O_1N) \cos \theta_t = \frac{W_c}{2} \cos \theta_t \tag{4}$$

On closely observing the turbo block and turbo roundabout, note that it has many different semi-circles but only two centres O_1 and N , where O_1 is the centre of all the semi-circles on the right-hand side of the translation axis and N is the centre of all the semi-circles on the left-hand side of the translation axis (Figure 1). The difference between the two centres is approximately equal to half the circulatory roadway width ($W_c/2$). After laying out the turbo block using Equation (2), the turbo roundabout is carved out by constructing the roundabout legs at the intersection points of the horizontal and vertical axes of the turbo block or at an exactly 90-degree angle along the roundabout, as suggested by Fortuijn [8] and Fortuijn and Hendrik [9].

There are a total of four approaches at the Turbo roundabout with a bypass lane at Approach 2. The width of the circulatory roadway is W_c and the width of the approach road is W_1 . In addition, there is a median of width W_m separating the flow of the traffic. The two-lane knee type turbo multilane turbo roundabout consists of a total of five semicircles, the radius and centre of which goes on changing with each rotation at the translation axis.

2.2. Intersection Sight Distance

Intersection sight distance is the distance which a driver, having no right of way, needs to see and then safely react to the conflicting vehicle. Intersection collisions are mainly caused by inadequate sight distance at intersections. For ISD, a clear view of traffic is provided for the approaching vehicle at the intersection to enable the driver to perceive and react to the acceptable gap. The required sight distance at roundabouts is achieved using a sight triangle. The sight triangle is provided and checked at the entry point of each leg of the intersection.

Intersection sight distance should be measured using a driver height and an object height of 1.080 m, as stated by the American Association of State Highway and Transportation Officials [27]. In addition, ISD should be calculated for a particular critical time. The critical time is defined as the minimum time interval in the vehicle stream that a minor street driver is ready to accept for crossing or entering the major stream conflict zone [28].

In traditional and turbo roundabouts, the vehicle entering the roundabout at any of the approaches must yield for the vehicles in the circulating stream, which makes the entering leg as a minor street and the circulating stream as a major stream conflict zone. For roundabouts, the sight distance triangle is checked for the conflicting-circulating and entering vehicles. The sight distance of the approaching vehicle is checked at two different positions for each of the above-mentioned cases. The first position is when the approaching vehicle is 15 m from the yield line and the second position is when the approaching vehicle is at the yield line [29]. The distance travelled during the critical time is given by

$$D_1 = 0.278 t_c V_c \tag{5}$$

$$D_2 = 0.278 t_c V_e \tag{6}$$

where D_1 denotes the sight distance of the sight triangle corresponding to the conflicting-circulating vehicle (m), t_c denotes the critical time (s), V_c denotes the speed of the conflicting-circulating vehicle (km/h), D_2 denotes the sight distance of the sight triangle corresponding to the conflicting-entering vehicle (m), and V_e denotes the speed of the conflicting-entering vehicle (km/h).

As per NCHRP [16] and AASTHO [27], the critical time for multilane roundabouts should be taken as 5 s. A study by Guerrieri et al. [30] suggested a critical time for turbo roundabouts between 4.03 s and 5.48 s. This range was determined using traffic sample data at a real turbo roundabout and was found to be consistent with previous studies. In this paper, a value of 5 s for critical time was used, which is the recommended value by both AASTHO [27] and NCHRP [16]. The sight triangle consists of the sightline from the approaching vehicle to the conflicting vehicle, the line from the approaching vehicle to the conflict point, and the line on the vehicle path from the conflict point to the conflicting vehicle.

In the case of multiple lanes, each lane has an approaching vehicle and two sightlines to the conflicting-circulating and entering vehicles are considered. Out of these two sightlines, the sightline that requires more area is selected for design purposes. The sightline from the approaching vehicle to the conflicting vehicle is needed for calculating the lateral clearance. According to the *Roundabout Information Guide* [16], it is recommended not to provide more than the required lateral clearance. The reason is that excessive intersection sight distance can lead to higher vehicle speeds and thus affects roundabout safety. This can be achieved through landscaping tools such as planting trees along the sightline.

3. Assumptions and Procedures

Analytical models for the conflicting-entering and circulating vehicles are developed and will be graphically verified. The following assumptions were made in developing the models:

1. The centre of the turbo roundabout arcs on the right side is O_1 (Figure 2).
2. The approach legs are intersecting the turbo roundabout exactly at a 90-degree angle.
3. The critical time t_c for ISD is 5 s.
4. The distance from the front end of the vehicle and the driver's eye is assumed to be 2.43 m.

The procedure for developing ISD models for the turbo roundabout involves the following steps (see Figure 3):

1. Choose the type of turbo roundabout and determine its initial parameters.
2. A swept path and speed analyses of the design vehicle are carried out. If the analyses do not satisfy the swept path or speed requirements, redesign the parameters.
3. Once the initial radius and translation axis have been defined, develop the radii of other consecutive semi-circles.
4. To analyse ISD, determine the coordinates of the centre of the arcs on the left and right sides of the translation axis. The coordinates of right side semicircles are assumed to be at the origin.
5. Determine the coordinates of the approaching vehicle when it is at 15 m from the yield line (Case 1) and when it is at the yield line (Case 2).
6. Determine the coordinates of the conflict point. These coordinates are important because they are needed to determine the coordinates of the conflicting-circulating and conflicting-entering vehicles.
7. Determine the coordinates of the conflicting-circulating and conflicting-entering vehicles by calculating the distance travelled by the vehicle during the critical time from the conflict point following the vehicle movement trajectory.
8. Determine the equation of the sightline using the coordinates of the approaching vehicle and those of the conflicting-circulating or the conflicting-entering vehicle. Then, develop an equation for the lateral clearance.

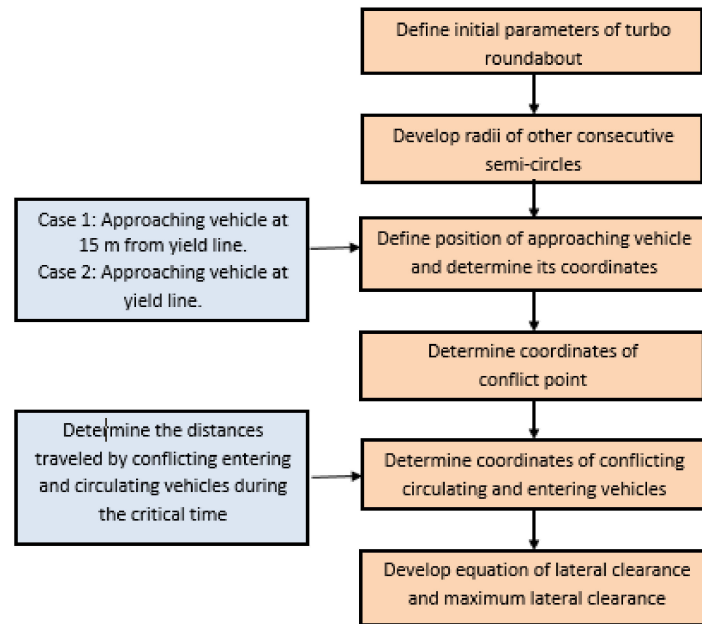


Figure 3. Procedure of ISD analysis of turbo roundabout.

4. Sight Distance Model: Conflicting-Circulating Vehicle

Following the procedures of Easa [31], the sight distance for the approach is determined at 15 m from the yield line (L_{min}). As shown in Figure 4 for the approaching vehicle, the driver eye from the yield line is Point a . From this point, the vehicle will move toward the center of the entry lane W_1 so that it can comfortably take turn either to the inner or the outer circulatory lane of width W_C . This center of the lane is Point e . There is a median separating the entry and exit lanes, and the center of the median intersects with R_5 Point z . The width of the median is W_m . Interestingly; the nature of the turbo roundabout is such that the y -axis exactly passes through the center off the median. For the circulating vehicle, the distance from the driver’s eye to the outer edge of the circulatory roadway is denoted as A_2 and for the approaching vehicle, the distance from the driver’s eye to the outer edge of the median is denoted as A_1 , as shown in Figure 4.

4.1. Coordinates of Conflict Point

Consider first Case 1, where the approaching vehicle is located 15 m before the yield line. To determine the coordinates of the conflict point and the approaching vehicle, the coordinates of Point e (x_e, y_e) are first determined as

$$x_e = \left(\frac{W_m}{2} + \frac{W_1}{2} \right) \tag{7}$$

$$y_e = \sqrt{R_5^2 + \left(\frac{W_m}{2} + \frac{W_1}{2} \right)^2} = \left(R_5^2 \left(\frac{W_m}{2} + \frac{W_1}{2} \right)^2 \right)^{0.5} \tag{8}$$

where R_5 denotes the radius of the outer semi-circle of the roundabout with O_1 as a center, W_m denotes the width of median, and W_1 denotes the width of the entry lane. The coordinates of the approaching vehicle are given by

$$x_a = \frac{W_m}{2} + W_1 - A_1 \tag{9}$$

$$y_a = R_5 + L_{min} \tag{10}$$

where A_1 denotes the distance between the driver eye and outer edge of the median and L_{min} denotes the distance from the yield line (15 m).

To find coordinates of Point c ; let us denote coordinates of Point c be (x_c, y_c) . As Point c lies on the extension of the line ae and both ae and ac have the same slopes, the equation of line ac in terms of x_c and y_c is given by

$$x_c = \frac{x_a + (y_c - y_a)}{p_{ac}} \tag{11}$$

where

$$P_{ac} = P_{ae} = \frac{y_e - y_a}{x_e - x_a} \tag{12}$$

In addition, since the coordinates (x_c, y_c) satisfy the equation of a circle of radius $(R_5 - A_2)$ with the centre $O_1 (0, 0)$, the equation of this circle is given by

$$x_c^2 + y_c^2 = (R_5 - A_2)^2 \tag{13}$$

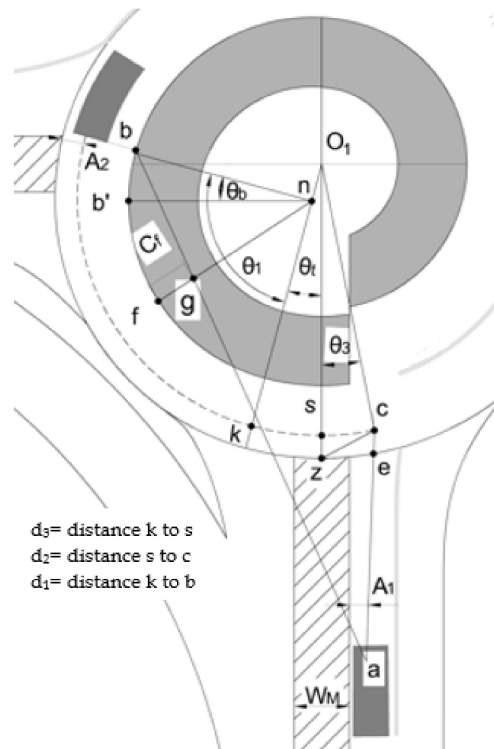


Figure 4. Geometry of ISD for the approaching and conflicting-circulating vehicles.

Since the conflict Point c lies on both the circle and the straight-line ac , x_c and y_c can be determined by solving for their point of intersection as follows. Substituting for x_c from Equation (11) into Equation (13), then

$$x_a^2 + \frac{(y_c - y_a)^2}{P_{ac}^2} + \frac{2x_a(y_c - y_a)}{P_{ac}} + y_c^2 = (R_5 - A_2)^2 \tag{14}$$

Converting Equation (14) into a quadratic form in terms of y_c , then

$$y_c^2 \left[\frac{1}{P_{ac}^2} + 1 \right] + y_c \left[\frac{-2y_a}{P_{ac}^2} + \frac{2x_a}{P_{ac}} \right] + \left[\frac{y_a^2}{P_{ac}^2} - \frac{2x_a y_a}{P_{ac}} - (R_5 - A_2)^2 \right] = 0 \tag{15}$$

This is a quadratic equation in y_c , which is written as

$$\beta y_c^2 + \gamma y_c + \lambda = 0 \tag{16}$$

where

$$\beta = \left[\frac{1}{P_{ac^2}} + 1 \right] \tag{17}$$

$$\gamma = \left[\frac{-2y_a}{P_{ac^2}} + \frac{2x_a}{P_{ac}} \right] \tag{18}$$

$$\lambda = \left[\frac{y_a^2}{P_{ac^2}} - \frac{2x_a y_a}{P_{ac}} - (R_5 - A_2)^2 \right] \tag{19}$$

Solving Equation (16) gives

$$y_c = \frac{-\gamma \pm \sqrt{\gamma^2 - 4\beta\lambda}}{2\beta} \tag{20}$$

The solution for y_c gives two values, and only the feasible value is used for further analysis. Substituting for y_c from Equation (20) into Equation (13), the x_c is then given by

$$x_c = \left\{ (R_5 - A_2)^2 - y_c^2 \right\}^{0.5} \tag{21}$$

4.2. Coordinates of the Circulating Vehicle

To determine the coordinates of the circulating vehicle, the position of the circulating vehicle is first determined using Equation (3). Using this equation, the total distance (SSD travelled by the vehicle in t_c) is obtained. The total SSD can be divided into three parts (d_1, d_2, d_3) as depicted in Figure 4, where d_3 is the distance travelled by the vehicle between Points s and c , d_2 is the distance travelled by the vehicle between Points k and s , and d_1 is the distance covered by the vehicle between Point k and the front end of the conflicting-circulating vehicle. The total distance $D_1 = d_1 + d_2 + d_3$. Since D_1, d_2 , and d_3 are known, then d_1 is given by

$$d_1 = D_1 - (d_2 + d_3) \tag{22}$$

$$d_1 = (R_5 - A_2) \{ \theta_3 - \theta_t \} \tag{23}$$

To determine θ_3 , from the triangle O_1cz

$$\text{Cos}\theta_3 = \frac{(R_5 - A_2)^2 + R_5^2 - (zc)^2}{2(R_5 - A_2)R_5} \tag{24}$$

where $zc = \sqrt{(x_z - x_c)^2 + (y_z - y_c)^2}$. Determine the coordinates of Point b , θ_b given by

$$\theta_b = \theta_1 - (90 - \theta_t) \tag{25}$$

Thus, the coordinates of Point b are given by

$$x_b = R_2 \text{cos}\theta_b + \frac{W_c}{2} \text{sin}\theta_t \tag{26}$$

$$y_b = -R_2 \text{sin}\theta_b + \frac{W_c}{2} \text{cos}\theta_t \tag{27}$$

For Case 2 (approaching vehicle at yield line), only the coordinates of the approaching vehicle change. The equations of the coordinates of the conflict point and those of the circulating vehicle do not change as they are independent of the coordinate value of the approaching vehicle. The only parameter that will vary is the lateral clearance. As the vehicle approaches the yield line, there is a certain distance between the front end of the

vehicle and the driver’s eye, d_e , which is assumed to be equal to 2.43 m [31]. In addition, the vehicle is assumed to be at the centre of the inner lane when at the yield line, so Point a overlaps with Point e when the vehicle is at the yield line. Thus, the coordinates of the approaching vehicle (x_a, y_a) are given by

$$x_a = \left(\frac{W_m}{2} + \frac{W_1}{2} \right) \tag{28}$$

$$y_a = (R_5 + d_e) \tag{29}$$

4.3. Lateral Clearance Formulation

4.3.1. General Lateral Clearance

The lateral clearance is the clear distance required to be maintained between the line of sight and the outer circular edge of the truck-apron to provide a mutual unobstructed view of the approaching vehicle and the conflicting vehicle.

The formulation of the lateral clearance depends on the coordinates of the approaching and conflicting-circulating vehicles both of which are determined using Equations (9), (10), (26), and (27). In Figure 4, considering an arbitrary Point f on the edge of the truck apron (x_f, y_f) , Point g is determined where line ab intersects nf . Now that the points are set, the lateral clearance (C_f) is equal to the distance gf , which is given by

$$gf = C_f = R_2 - \sqrt{(x_g - x_N)^2 + (y_g - y_N)^2} \tag{30}$$

where

$$x_g = \frac{y_a - y_N - x_a P_{ab} + x_N P_{Nf}}{P_{Nf} - P_{ab}} \tag{31}$$

$$y_g = \frac{y_a P_{Nf} - y_N P_{ab} - (x_a - x_N) P_{ab} P_{Nf}}{P_{Nf} - P_{ab}} \tag{32}$$

4.3.2. Maximum Lateral Clearance

Note that Point f is variable, and the coordinates of Point g depend on the coordinates of Point f . To determine the maximum clearance $C_{f(Max)}$, Point f is considered as a variable and the maximum lateral clearance is obtained using mathematical optimization with the Microsoft Excel add-in tool Solver software. The optimization model for determining the maximum lateral clearance is given by

$$\text{Maximize } Z = C_f \tag{33}$$

Subject to $d_L < d_f < d_U$, where d_f denotes the distance of Point f on the edge of the truck apron (decision variable), d_L and d_U denote the arbitrary lower and upper limits of the decision variable d_f , which covers the possible range of the lateral clearance.

5. Sight Distance Model: Conflicting-Entering Vehicle

5.1. Coordinates of Entering Vehicle

Consider first Case 1, where the approaching vehicle is located 15 m before the yield line. Point a denotes the driver’s eye in the approaching vehicle. b_2 is the point which lies at such a distance as travelled by the entering vehicle during the critical time t_c from the conflict Point c . C_{f2} is the lateral clearance distance required for ISD for the conflicting-entering vehicle. z_1 is the point (not shown in the figure) which is the center of the bypass lane with radius R_{bypass} . The total sight distance D_2 from the conflict Point c to b_2 is given by

$$D_2 = d_2 + d_3 + d_4 + d_5 + d_6 \tag{34}$$

where d_6 denotes the distance covered by vehicle from b_2 to q , d_5 denotes the distance covered by vehicle from q to p' , d_4 denotes the distance covered by vehicle from p' to k , d_3 denotes the distance covered by vehicle from s to c , and d_2 denotes the distance covered by vehicle from k to s , as shown in Figure 5. Therefore, the distances d_2, d_3, d_4 are determined as

$$d_2 = \theta_T (R_5 - A_2) \tag{35}$$

$$d_4 = \theta_4 (R_4 - A_2) \tag{36}$$

$$d_3 = \theta_3 (R_5 - A_2) \tag{37}$$

where $\theta_4 = 45^\circ - \theta_t$ and θ_3 is given by Equation (24). To determine d_5 , the coordinates of p and q are needed. The coordinates of p are given by

$$x_p = \frac{w_c}{2} \sin \theta_t + \frac{1}{\sqrt{2}} (R_4 - A_2) \tag{38}$$

$$y_p = \frac{w_c}{2} \cos \theta_t + \frac{1}{\sqrt{2}} (R_4 - A_2) \tag{39}$$

The coordinates of q are given by

$$x_q = x_n + R_6 = \frac{w_c}{2} \sin \theta_t + R_6 \tag{40}$$

$$y_q = \frac{w_m}{2} + w_1 - A_1 \tag{41}$$

Using Equations (38)–(41), the distance between Points p and q is obtained as

$$l_{pq} = \sqrt{(x_p - x_q)^2 + (y_p - y_q)^2} \tag{42}$$

The coordinates of z_1 are

$$x_{z_1} = y_{z_1} = \left(R_{bypass} + w_e + \frac{w_M}{2} \right) \tag{43}$$

Similarly using Equations (38)–(41) and (43), the distance between Points p and z_1 and between Points q and z_1 is given by

$$l_{qz_1} = \sqrt{(x_q - x_{z_1})^2 + (y_q - y_{z_1})^2} \tag{44}$$

From the three distances l_{pq}, l_{pz_1} , and l_{qz_1} of triangle pqz_1 , the angle θ_5 is determined as

$$\theta_5 = \cos^{-1} \left[\frac{l_{pz_1}^2 + l_{qz_1}^2 - l_{pq}^2}{2l_{pz_1}l_{qz_1}} \right] \tag{45}$$

The entering vehicle travels along the straight portion b_2q and then accelerates at the curve qp with center z_1 . However, before the vehicle reaches p , it reverses the curvature and tends to move along a curve around the center n . Thus, instead of touching p , it crosses Point p' and thus the trajectory of the vehicle will be along $b_2-q-p'-k-s-c$, as shown in Figure 5. Locating the exact position of Point p' mathematically is quite cumbersome. Therefore, for practical purposes and to maintain simplicity, p' is assumed to coincide with p . Thus, $l_{qp} \simeq l_{qp'}$ and $l_{pz_1} \simeq l_{p'z_1}$. Then, the curved distance along qp' (Figure 5) is given by

$$d_5 = \theta_5 l_{p'z_1} \tag{46}$$

As the distance pp' is negligibly small, θ_5 can also be simply but less precisely determined by considering $l_{qp} \simeq l_{qp'}$ as a circular arc of radius z_1p and drawing the right bisector of the chord qp :

$$\theta_5 = 2\sin^{-1} \frac{pq/2}{z_1p} \tag{47}$$

$$D_2 = d_{cir} + d + d_{entry} \tag{48}$$

We have already found d_2, d_3, d_4 and d_5 . Now, we must find d_6 . As per Easa et al. [32], d_{cir} denotes the distance along circulatory path, d denotes the distance during deceleration, and d_{entry} denotes the distance along entry curve. Based on Figure 5,

$$D_2 = (d_2 + d_3 + d_4) + d_5 + d_6 \tag{49}$$

$$d_{entry} = d_6 = \theta_4 (R_4 - A_2) + \theta_T(R_5 - A_2) + \theta_3 (R_5 - A_2) + \theta_5 l_{qz_1} - D_2 \tag{50}$$

As per Easa et al. [32], depending on the position of the entry vehicle, there are three cases for which D_2 can be determined. The first case is when the end of the sight distance leg lies on the circulatory part of the entry path (vehicle b_2 lies between Point p' and c), where the distance D_2 is given by

$$D_2 = t_c v_{cir} \tag{51}$$

The second case is when the end of the sight distance leg lies on the deceleration part (vehicle b_2 lies between Points q and p'), where the distance D_2 is given by

$$D_2 = d_{cir} + \frac{v_c t' + t' \sqrt{v_{cir}^2 + (v_e'^2 - v_{cir}^2)}}{2} \tag{52}$$

Both of these cases are not relevant to this study because when vehicle b_2 lies between Points q and c , the lateral clearance is always negative. This means that, in Figure 5, the distance z_1f_2 is always greater than the radius of the bypass lane, hence there is no requirement for providing any lateral clearance. The third case is when vehicle b_2 lies on the end of the sightline.

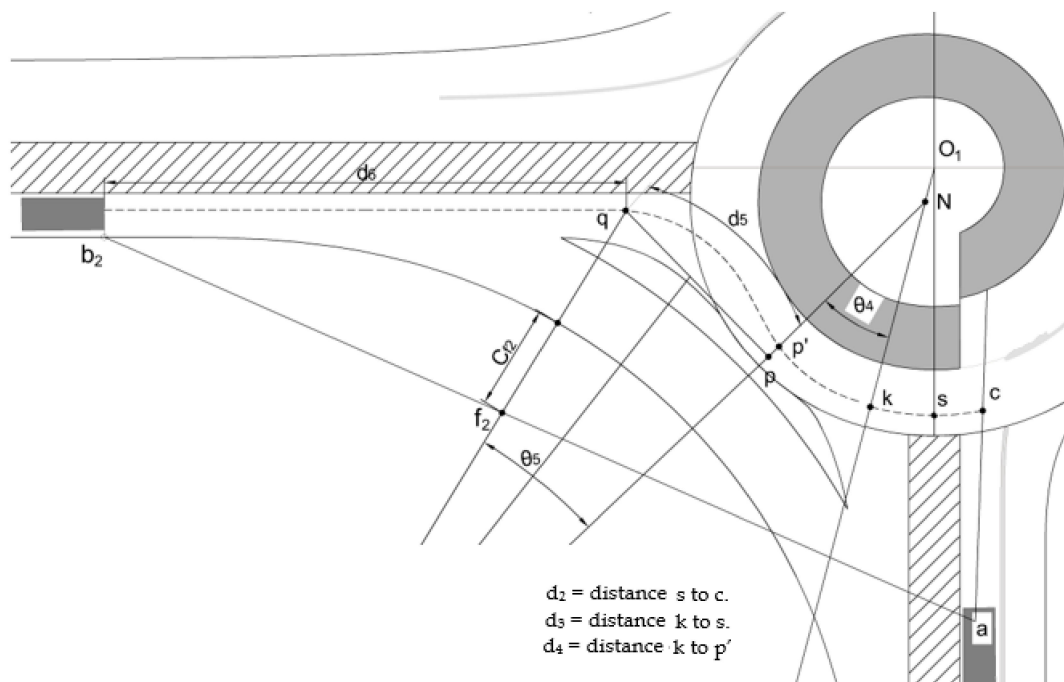


Figure 5. Geometry of ISD of the approaching and conflicting-entering vehicles.

The entry part before deceleration (between Points b_2 and q) requires calculating the lateral clearance. The distance D_2 for the third case is given by

$$D_2 = -\frac{(v_e - v_{cir})^2}{2a} + v_e t_c + d_{cir} \left(1 - \frac{v_e}{v_{cir}}\right) \tag{53}$$

After finding D_2 for the third case, the distance d_6 is obtained from Equation (50). Hence, the coordinates of b_2 are given by

$$x_{b_2} = (d_6 + R_6 + x_N) \tag{54}$$

$$y_{b_2} = \left(\frac{W_m}{2} + w_e\right) \tag{55}$$

When the approaching vehicle is at the yield line, only the coordinates of this vehicle change. The equations for the coordinates of conflict point and the conflicting-circulating vehicle do not change. In addition, as the vehicle approaches the yield line, there will be a certain distance from the front end of the vehicle and the driver's eye, d_e . As previously stated, this distance is assumed to be 2.43 m. Then, the coordinates of the approaching vehicle are given by

$$x_a = \left(\frac{W_m}{2} + \frac{W_1}{2}\right) \tag{56}$$

$$y_a = (R_5 + d_e) \tag{57}$$

5.2. Lateral Clearance Formulation

The equation of lines ab_2 and qz_1 can be derived as

$$y_{f_2} = y_a + \left(\frac{y_{b_2} - y_a}{x_{b_2} - x_a}\right) (x_{f_2} - x_a) \tag{58}$$

$$y_{f_2} = y_q + \left(\frac{y_q - y_{z_1}}{x_q - x_{z_1}}\right) (x_{f_2} - x_q) \tag{59}$$

Solving Equations (58) and (59), the coordinates of Point f_2 (x_{f_2}, y_{f_2}) can be determined as

$$x_{f_2} = \frac{y_q - y_a - x_q P_{qz_1} + x_a P_{ab_2}}{P_{ab_2} - P_{qz_1}} \tag{60}$$

$$y_{f_2} = \frac{y_q P_{ab_2} - y_a P_{qz_1} - P_{ab_2} P_{qz_1} (x_q - x_a)}{P_{ab_2} - P_{qz_1}} \tag{61}$$

Now, the lateral clearance C_{f_2} is given by

$$C_{f_2} = R_{bypass} - \sqrt{(x_{f_2} - x_{z_1})^2 + (y_{f_2} - y_{z_1})^2} \tag{62}$$

As shown in Figure 5, the lateral clearance C_{f_2} is measured along the line qz_1 . By defining the lateral clearance at this location, the sightline can be defined by connecting Point a and the outer end of the lateral clearance C_{f_2} . Thus, the required lateral clearance for the entire sightline is completely defined. In addition, C_{f_2} is approximately equal to the maximum lateral clearance and can be implemented along the entire sightline.

6. Model Validation

The proposed analytical ISD models were validated using an application example. The results of the analytical models were compared with those obtained graphically using AutoCAD. Consider a turbo roundabout with initial radius $R_1 = 10.50$ m, $V_{cir} = 30$ km/h, width of circulatory road width $W_1 = 3.19$ m, and width of entry lane $W_c = 5.15$ m. The primary translation axis is at 15 degrees (0.27 radians) with the y -axis. The width of the median $W_m = 4.00$ m and critical time $t_c = 5$ s. Table 1 shows the input data.

Table 1. Input data used for validation.

Parameter	Value
X_0	0
Y_0	0
R_1	10.50 m
W_1	3.19 m
m	0.43 m
W_m	4.00 m
W_C	5.15 m
A_1	2.00 m
A_2	1.78 m
L_{min}	14.95 m
θ_T	0.26 (rad)
t_C	5 s
V_C	30 km/h
V_e	60 km/h

The input data for model validation and application are shown in Table 1. Using the given value of the initial radius $R_1 = 10.5$ m, the width of circulatory road $W_c = 5.15$ m, and the shift $m = 0.43$, Equation (2) was used to calculate the subsequent radii as $R_2 = 13.3$ m, $R_3 = 16.1$ m, $R_4 = 18.9$ m, $R_5 = 21.7$ m, and $R_6 = 24.5$ m. For validating the analytical model, the input values were plotted on AutoCAD. The comparison of the analytical and graphical results are shown in Table 2. The analytical results of the application example are obtained using the derived equations, and the results are shown in Figure 6.

Table 2. Results of application example and comparison with graphical results.

No.	Variable	Symbol	Analytical	Graphical
1	x -Coordinate of approaching vehicle	x_a	3.19	3.19
2	y -Coordinate of approaching vehicle	y_a	-36.60	-36.60
3	x -Coordinate of conflict point	x_C	3.60	3.63
4	y -Coordinate of conflict point	y_C	-19.64	-19.67
5	x -Coordinate of circulating vehicle	x_b	-10.17	-10.23
6	y -Coordinate of circulating vehicle	y_b	5.19	5.3
7	Lateral Clearance at Point f	C_f	6.57	6.53
8	x -Coordinate of entering vehicle	x_{b_2}	-61.83	-61.9
9	y -Coordinate of entering vehicle	y_{b_2}	-5.21	-5.21
10	Lateral Clearance at Point f_2	C_{f_2}	7.54	7.61

It was observed from the above comparison tables that the values calculated using the analytical model closely match those obtained graphically. The small variation observed for a few parameters is due to the complex mathematics involved.

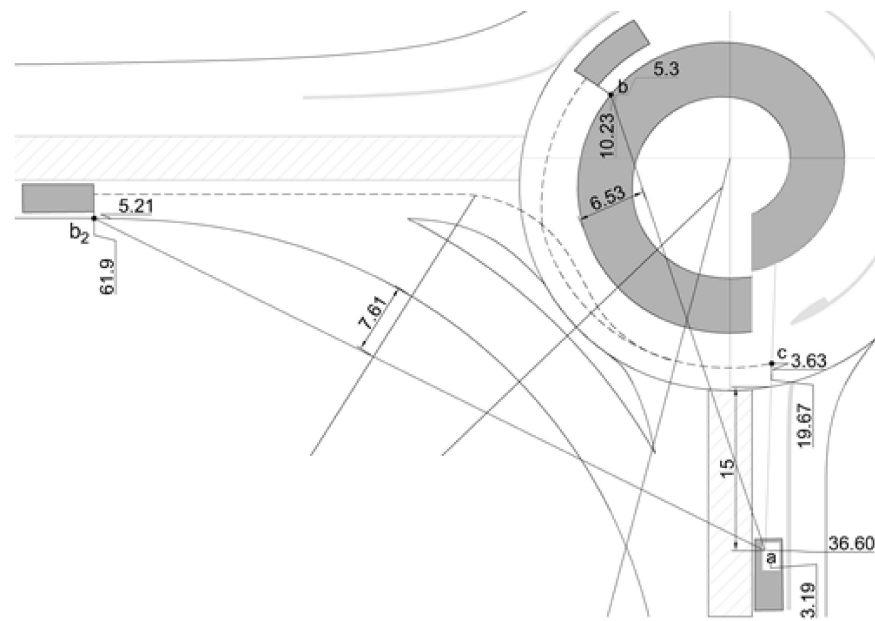


Figure 6. Model validation.

7. Design Aids

Table 3 shows the required maximum lateral clearance to the conflicting-circulating vehicle for different speeds and radii. Table 4 shows the lateral clearance C_{f2} to the conflicting-entering vehicle for different speeds and radii. Note that the values of lateral clearance of Table 4 are applicable only for Approach 1. For Approach 2 (where there is no bypass lane), the required lateral clearance approximately equals those shown in Table 4 plus half the width of the bypass lane roadway (3.19 m). The required lateral clearance for this approach are shown in Table 5. Note that the range of the circulatory speed is 15 km/h to 30 km/h, according to the literature [30]. As noted in Table 3, the maximum lateral clearance increases when the approach vehicle is at yield line. However, for the conflicting-entering vehicle, the results are the opposite as the lateral clearance decreases when the approach vehicle is at the yield line, as shown in Tables 4 and 5. The negative values of the lateral clearance in these tables mean that no lateral clearance is required as the sightline lies entirely in the inside of the bypass roadway. For Approaches 3 and 4, the lateral clearance is approximately the same as those for Approach 2 (Table 5) since there is only a minor difference between the radii and centers of the inscribed semi-circles of the respective approaches.

Table 3. Maximum lateral clearance for conflicting-circulating vehicle (in meters).

V_C (km/h)	Approaching Vehicle at	
	15 m from the Yield Line	Yield Line
(a) $R_1 = 10.50$ m		
15	1.4	1.5
20	1.6	2.6
25	3.6	5.0
30	6.6	7.9
(b) $R_1 = 12.00$ m		
15	1.3	1.4
20	1.6	2.3
25	3.1	4.5
30	5.8	7.2

Table 4. Lateral clearance C_{f2} (m) for conflicting-entering vehicle (Approach 1).

Speed of Circulating Vehicle, V_c (km/h)	Speed of Entry Vehicle, V_e (km/h)					
	40		50		60	
	$R_1 = 10.5$ m	$R_1 = 12$ m	$R_1 = 10.5$ m	$R_1 = 12$ m	$R_1 = 10.5$ m	$R_1 = 12$ m
(a) Approaching Vehicle at the Yield Line						
15	−9.0	−10.42	−7.07	−8.66	−5.64	−7.37
20	−4.4	−4.7	−2.24	−2.42	−0.63	−0.71
25	−2.7	−2.51	−0.42	−0.15	1.19	1.57
30	−1.8	−1.41	0.5	0.97	2.12	2.71
(b) Approaching Vehicle 15 m from the Yield Line						
15	−9.2	−11.3	−6.5	−9.0	−4.5	−7.1
20	−2.7	−3.4	0.7	−0.1	3.2	2.5
25	0.1	−0.3	3.5	3.3	6.1	6.0
30	1.4	1.4	5.0	5.1	7.6	7.8

Table 5. Approximate maximum lateral clearance (m) for conflicting-entering vehicle (Approach 2).

Speed of Circulating Vehicle, V_c (km/h)	Speed of Entry Vehicle, V_e (km/h)					
	40		50		60	
	$R_1 = 10.5$ m	$R_1 = 12$ m	$R_1 = 10.5$ m	$R_1 = 12$ m	$R_1 = 10.5$ m	$R_1 = 12$ m
(a) Approaching Vehicle at the Yield Line						
15	−7.3	−8.8	−5.4	−7.0	−4.0	−5.7
20	−2.8	−3.0	−0.6	−0.8	0.9	0.9
25	−1.0	−0.9	1.2	1.4	2.8	3.1
30	−0.1	0.2	2.2	2.5	3.7	4.3
(b) Approaching Vehicle 15 m from the Yield Line						
15	−7.5	−9.7	−4.8	−7.3	−2.8	−5.5
20	−1.0	−1.7	2.2	1.5	4.7	4.0
25	1.6	1.3	5.0	4.8	7.63	7.5
30	3.0	3.0	6.5	6.6	9.1	9.3

8. Conclusions

Intersection sight distance for knee-type turbo roundabout has been modelled for two key positions of the approaching vehicle. In the study, ISD was analytically formulated by constructing sightlines and sight triangles that help the drivers of the approaching vehicles to see the conflicting vehicles and decide to safely enter the roundabout. The developed analytical model is of a generic nature and can be used for any knee-type turbo roundabout conditions. The model was validated using AutoCAD and its application was illustrated using a numerical example. Based on the present research, a few important insights are provided:

1. The results of the present study show that the required lateral clearance for the conflicting circulating vehicle increases when the approaching vehicle is at the yield line compared when the vehicle is 15 m before the yield line at any speed or radius. The reverse is true for the conflicting-entering vehicle.
2. Intersection sight distance has been established to increase the safety of turbo roundabouts. However, providing greater sight distances than the required ISD values is not recommended as the collision rate may increase. In this regard, landscaping techniques can be used to restrict the sightlines to only ISD requirements.
3. The developed method may be further used in developing safety performance functions or crash modification factors under varying roadway and traffic conditions. A

detailed study on calibrating the developed equations along with its robust validation using field conditions may be considered as one of the ways forward to extend this study. In addition, reliability-based performance analysis of the developed method can be performed to improve efficiency and safety of turbo roundabouts.

4. This paper has focused on modeling ISD for turbo roundabouts. The presented design aids should be helpful for designers to directly determine the lateral clearance requirements, and as such the paper helps bridge the gap between theory and practice. Future research should address several aspects, including the implications of the findings of this paper for research, practice, and society, and the economic viability of turbo roundabouts. In addition, a comparison of the AASHTO and European Union standards is warranted.

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Abbreviations

The following notations are used in this paper:

a	position of approach vehicle
A_1	distance between the driver eye and outer edge of the median
A_2	distance between the driver eye and outer edge of the roundabout
b	position of circulating conflicting vehicle
b_2	position of entering conflicting vehicle
c	conflict point
C_f	lateral clearance for circulating conflicting vehicles
C_{f2}	lateral clearance for entering conflicting vehicles
d	distance during deceleration
d_2	distance covered by vehicle from k to s
d_3	distance covered by vehicle from s to c
d_4	distance covered by vehicle from p' to k
d_5	distance covered by vehicle from q to p'
d_6	distance covered by vehicle from b_2 to q
d_{cir}	distance along circulatory path
d_{entry}	distance along entry curve
D_1	sight distance of the sight triangle of the conflicting-circulating vehicle
D_2	sight distance of the sight triangle of the conflicting-entering vehicle
L_{min}	distance from the yield line (15 m)
m	shift between inner and outer apron
N	centre of all the semi-circles on the left-hand side of the translation axis
O_1	centre of all the semi-circles on the right side of the translation axis
R_1	turbo roundabout initial radius with centre O_1
R_2	radius of the second consecutive semi-circle with centre n
R_5	radius of outer semi-circle of roundabout with center O_1
B_{bypass}	radius of the bypass lane
R_n	radius of the semicircle of turbo roundabout with centre O_1

R_{n+1}	radius of next consecutive semi-circle of turbo roundabout with centre n
t_c	critical time
V_c	speed of the conflicting-circulating vehicle
V_e	speed of the conflicting-entering vehicle
W_m	width of median
W_1	width of the entry lane
W_c	circulatory roadway width
Z_1	centre of the radius of bypass lane
θ_T	angular distance between translation axis and y -axis

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