

# Parameter Scaling Protocol for Upper-limb Musculoskeletal Models

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## **Abstract**

Generic musculoskeletal models are not reliable predicting inter-individual variations in muscle forces. Scaling the model parameters is necessary to represent the muscle characteristics of the subjects and thus to pinpoint the differences in force capacity. Optimal Fiber (OFL) and Tendon Slack Length (TSL) have been identified as the two most influential parameters in muscle force generation. The goal of the current study is adjusting a lower-limb scaling algorithm for OFL and TSL to the Delft Shoulder and Elbow Model (DSEM). Furthermore, we evaluate the effect on the preservation of model consistency and muscle force production. Firstly, we scaled the DSEM geometrically. That drove twenty-two muscles to work out of the physiological range in the F-L curve up to 41% of the shoulder ROM. Moreover, the consistency of the model dropped by 78%. We tested three approaches to scale OFL and TSL. The constrained method delivered the best results reducing these percentages to 8% and 2.9%, respectively. It also increased the muscle force production of the DSEM 1.2%BW compared to the geometrically scaled version. The adaptation of the constrained scaling algorithm to the DSEM provides consistency values in the same range observed in lower-limb models. Therefore, we state that it is necessary to scale OFL and TSL whenever the dimensions of the DSEM are modified to obtain reliable muscle force estimations. We recommend further validation of the procedure developed in this article, for example, against data from instrumented endoprosthesis.

*Keywords:* Musculoskeletal Model, Delft Shoulder and Elbow Model, Optimal Fiber Length, Tendon Slack Length, Scaling, Upper-limb, Muscle-tendon parameters

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## 1. Introduction

Musculoskeletal (MSK) models provide a unique insight into aspects of the internal functioning of the locomotive system, such as net joint moments and muscle forces. Their initial purpose was raising knowledge about the bases of the MSK system. Early studies cover topics such as muscle collaboration to produce torques around joints [1], and estimation of the differences in joint loading during diverse tasks [2, 3]. In recent years, MSK models start to be helpful as well in the clinical field. Modern studies use them to predict the outcomes of tendon transfer surgeries [4] ("what if" simulations) and to explain how neuromuscular pathologies alter motion [5, 6].

Generic models, created from cadaveric data, are suitable for first-time investigations because they analyze the loading changes among tasks, not individuals. However, generic models are not appropriate for contemporary researches. These studies focus on the variations in muscle force capacity among subjects (instead of tasks), and models employing cadaveric data do not account for those differences [7]. In this landscape, MSK models should be capable of reproducing the force capability of the subjects. Hence, the set of parameters that determines the generation of force in MSK models must be scaled accordingly to the anatomical characteristics of the individuals [8, 9, 10, 11].

There are three groups of parameters in MSK models: geometrical, inertial, and muscle. Medical imaging, like MRI and CT-scans, allows measuring geometrical (for instance, segment dimensions and musculotendon lengths) [12], inertial (segmental mass) [13], and some muscle parameters (Physiological Cross-Section Area) [14] in living subjects. No current techniques allow measuring other muscle parameters, such as optimal fiber (OFL) and tendon slack length (TSL), in-vivo and hence, it is troublesome to scale them. However, these last two parameters are the most influential of all of them for muscle force generation. Therefore the adjustment of OFL and TSL is essential for the MSK model to match the force capacity of the subject [15, 16].

Geometrical scaling is the first step to modify the cadaveric parameters of the model. It involves adjusting the dimensions of the segments and the calculation of the joints' center of rotation. The length of the musculotendon units (MTU) is scaled proportionally to preserve the direction of their

38 force vectors. Then, the segment mass is scaled accordingly to the whole  
 39 body mass of the subject [17]. Several studies demonstrate that adjusting  
 40 these parameters improves joint loading estimations [7, 18]. However, others  
 41 shows that this level of scaling is not enough for a MSK model to represent  
 42 the muscle force capacity of a subject [19, 11, 20]. Even though the next  
 43 step seems to be modifying the muscle parameters of the model, it is not a  
 44 common practice, given the reasons in the previous paragraph. The alterna-  
 45 tive is not adjusting OFL and TSL to the new MTUs length, which causes a  
 46 shift in their working area in the Force-Length curve.

47

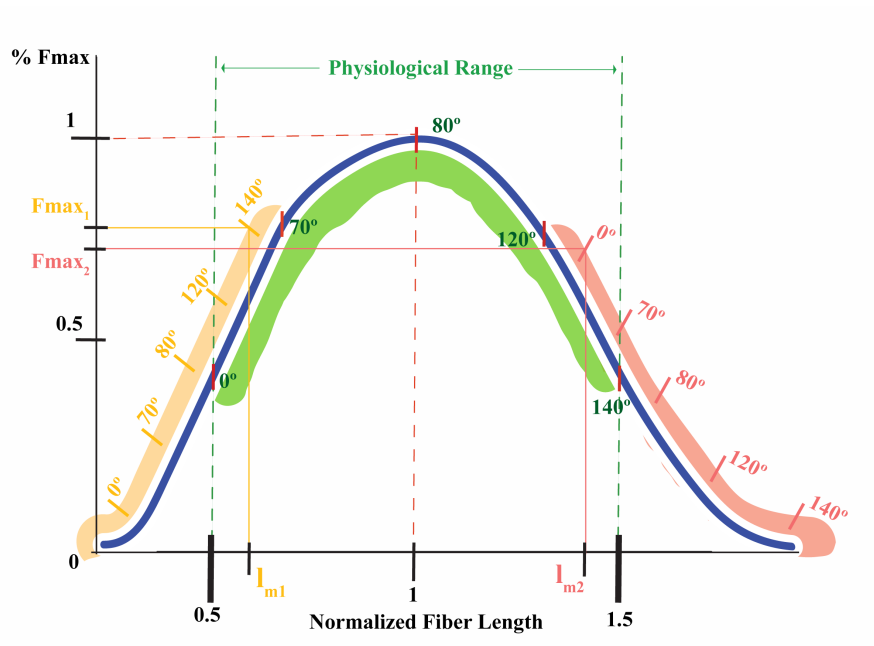


Figure 1: The coloured areas (yellow and red) shows the shift in the working area of an upper-limb muscle caused by modifying its length without accordingly adjusting its muscle parameters. The green area represents the length excursion of the muscle in the reference model (GM).  $F_{max1}$  and  $F_{max2}$  illustrate the decrease in muscle force production (both values are below the  $F_{max} = 1$ ). Furthermore, the behavior of the muscle is altered since  $F_{max1}$  and  $F_{max2}$  do not take place at the optimal fiber length ( $L_{norm}^m = 1$ ) but at  $l_{m,norm1}$  and  $l_{m,norm2}$ . The degrees marked along each of the three zones illustrate the humeral elevation angle. It also shows how the altered muscle behavior affects the force production since for a certain angle (e.g.,  $120^\circ$ ) the force generated in each situation varies. The X-axis indicates the normalized fiber length, which is the ratio between the length of the muscle and its optimal fiber length (Eq. 9).

48 The F-L curve defines the maximum force a muscle can generate depend-  
49 ing on its length. Figure 1 illustrates the F-L relation of a generic upper-limb  
50 muscle (in blue). In a generic model, all the muscles work within the physi-  
51 ological range (in green). However, the shift in the operating area caused by  
52 not adjusting the muscle parameters to the new MTUs length brings them  
53 to work out of the physiological area (red and yellow regions). In that sit-  
54 uation, the force generation of the muscles decreases, and their force peak  
55 happens at a different angle of humeral elevation. Winby describes this event  
56 as a loss of consistency in the scaled model. He establishes that the aim of  
57 any scaling technique should be not altering the F-L working region of the  
58 MTUs of the model [21]. In other words, the goal must be preserving the  
59 consistency of the model. Otherwise, the scaling process provokes a loss in  
60 the force capacity of the muscles due to the shift in its working region which,  
61 ultimately, alters their behavior.

62  
63 The literature on scaling muscle parameters for lower-limb models is quite  
64 extensive. A significant number of articles with different approaches have  
65 been published, which are classified on anthropometric or functional. The  
66 former rely solely on anatomical data [22, 21], while the later also employ  
67 dynamometry [23] or EMG [24, 10, 25]. Further studies have evaluated the  
68 influence of muscle parameters on the MTU moments in gait analyses [26, 16].  
69 Nevertheless, all these experiments (as well as Winby’s research) have only  
70 been conducted with lower-limb models, and literature on the topic for upper-  
71 limb models is very limited [27, 14, 28].

72  
73 In conclusion, scaling the parameters of MSK models is essential to match  
74 the force capacity of a subject. The most common scaling approaches (ge-  
75 ometrical techniques), however, provoke a loss of consistency in the scaled  
76 models. Consequently, these models do not match the force capability of  
77 the subjects. Studies involving lower-limb models have demonstrated that  
78 the loss of consistency is due to not scaling OFL and TSL [15, 16, 26]. Re-  
79 garding upper-limb models however, no study has examined that, despite  
80 some articles having reported that geometrically scaled upper-limb models  
81 also underestimate muscle forces.[19]

82  
83 The aim of this paper is studying the effect of scaling optimal fiber and  
84 tendon slack length on the consistency of geometrically scaled upper-limb  
85 models. We choose to adjust these two parameters following the recom-

86 mendations identified in the literature: maintain the model consistency and  
87 establish a non-linear relation between muscle length and OFL and TSL  
88 [15, 16, 8, 29]. For that purpose, we find the optimization algorithm devel-  
89 oped by Modenese the best option available [22]. The first condition is that  
90 the optimization algorithm scales OFL and TSL at least. Secondly, it should  
91 be not need dynamometer or EMG measurements since these methods are  
92 computationally expensive and require extremely large quantities of data.  
93 As far as we know, the only approach with those characteristics and which is  
94 suitable for upper-limb models is Modenese’s algorithm, although he did not  
95 prove it. Furthermore, his method outperforms the techniques reviewed by  
96 Winby in terms of preserving consistency, and contains a non-linear approach.

97  
98 We hypothesized that adjusting OFL and TSL in geometrically scaled  
99 upper-limb models would enhance their consistency. Furthermore, we ex-  
100 pected that improving the model’s consistency would cause an increase in its  
101 muscle force production.

## 103 2. Materials and Methods

### 104 2.1. *Musculoskeletal Model. The Delft Shoulder and Elbow Model.*

105 The Delft Shoulder and Elbow Model (DSEM) is a finite element model  
106 created by Van der Helm [30]. It depicts the upper-limb with six rigid bodies  
107 and thirty-one muscles, which divided in 139 contractile elements operate  
108 seventeen Degrees of Freedom (DOF). We named this version of the model  
109 the Generic Model (GM) [19].

110  
111 We also employed the geometrically scaled models from Bolsterlee’s in-  
112 vestigation [14]. These are versions of the DSEM whose segments’ length  
113 and mass were adjusted linearly according to the dimensions of five partici-  
114 pants. The length of the contractile elements in these models also changed  
115 proportionally with the new segments’ measures. The position of the gleno-  
116 humeral center of rotation was calculated using instantaneous helical axes  
117 (IHA) [31]. Nevertheless, out of the five scaled subjects, only two of them  
118 completed the Inverse Kinematic (IK) analysis. In the other three, the simu-  
119 lation crashed due to a collision between the scapular and thoracic segments.  
120 Since the scapula, clavicle and thorax were modeled as a closed kinematic

121 chain, not every combination of joint angles is feasible, and that leads to  
 122 collisions among these segments [30]. For the current study, the two models  
 123 that completed the IK analysis were named scaled-generic model 3 (SGM3)  
 124 and scaled-generic model 5 (SGM5). They are also mentioned as geometri-  
 125 cally scaled models.

126

127 ***2.2. Scaling procedure: Modenese’s algorithm for scaling optimal***  
 128 ***fiber and tendon slack length in geometrically scaled models.***

129 The scaling approach developed by Modenese exploited the insight pro-  
 130 vided by Zajac of the dimensionless Hill’s muscle model [32]. We calculated  
 131 the length of the MTUs ( $L^{mt}$ ) using the definition of muscle length by Hill  
 132 (Eq. 1, [33]), which depends on its tendon ( $l_t$ ) and muscle fiber length ( $l_m$ ),  
 133 and its pennation angle ( $\alpha$ ):

$$L_m^{mt} = l_m * \cos \alpha + l_t \quad (1)$$

134

135 Introducing normalized variables ( $l^{m,norm}$  and  $l^{t,norm}$ ), Zajac (Eq. 2, [32])  
 136 showed the dependence between the  $L_m^{mt}$  and its OFL ( $l_o^m$ ) and TSL ( $l_{s,m}^t$ ).  
 137 We employed the following equation (in vector notation) to estimate ( $l_o^m$ )  
 138 and ( $l_{s,m}^t$ ) for the SGMs:

$$L_m^{mt} = (l_{m,norm} * \cos \alpha) * l_o^m + l_{t,norm} * l_{s,m}^t \quad (2)$$

139

140 Based on the principles of the model by Hill, the  $l_{m,norm}$  and  $l_{t,norm}$  re-  
 141 main the same for a specific muscle in any individual. Then, the operating  
 142 behavior of the muscles in a generic model (whose parameters, extracted from  
 143 a cadaver, are physiologically valid) must be preserved when this model is  
 144 geometrically scaled [22, 21]. Consequently, Modenese developed an opti-  
 145 mization algorithm which solved Eq. 2, finding the values for OFL and TSL  
 146 (for the new  $L_m^{mt}$ ) to better preserve  $l_{m,norm}$  and  $l_{t,norm}$  as in the generic  
 147 model (GM).

148

149 Modenese’s algorithm contained three approaches that we modified so  
 150 that they could be applied to every MTU ‘ $m$ ’ in the DSEM. The collection

151 of the  $N$  samples of the variables in Eq. 4, 5, and 6 is addressed in the com-  
 152 ing section (2.3 *Scaling Protocol for the DSEM*).  $N$  is the optimal number of  
 153 sampling points (being 'n' each of those sampling point) that maximized the  
 154 accuracy of the three scaling approaches (Eq. 3, [22]).  $N$  depends logarithmi-  
 155 cally on the Degrees of Freedom (DOF) operated by the muscle (or MTU)  
 156 being analyzed.

$$N = 10^{DOF} \quad (3)$$

157 • **Linear approach:** We employed MATLAB to find a solution to the  
 158 least square problem of calculating  $l_o^m$  and  $l_{s,m}^t$  in Eq. 2. MATLAB  
 159 did so while minimizing the error introduced by the pseudoinverse of a  
 160 matrix (Eq. 4). If any of the new OFL or TSL are negative, they kept  
 161 their original values from the GM.

$$\begin{bmatrix} l_o^{m,subj} \\ l_{s,m}^{t,subj} \end{bmatrix} = \begin{bmatrix} l_{1,norm}^{m,ref} * \cos \alpha_{m,1}^{ref} & l_{m,1,norm}^{t,ref} \\ \vdots & \vdots \\ l_{n,norm}^{m,ref} * \cos \alpha_{m,n}^{ref} & l_{m,n,norm}^{t,ref} \end{bmatrix}^{-1} * \begin{bmatrix} L_{m,1}^{mt,subj} \\ \vdots \\ L_{m,n}^{mt,subj} \end{bmatrix} + e \quad (4)$$

162

163 • **Constrained approach:** In this case, we used MATLAB's function  
 164 'lsqnonneg' to find a solution to the least square problem of calculating  
 165  $l_o^m$  and  $l_{s,m}^t$  in Eq. 2. The algorithm minimizes the error introduced by  
 166 the pseudoinvserse while taking into account the restriction that the  
 167 solution should be greater than zero. The constrained method showed  
 168 a higher residue than the linear one due to the constraint introduced.

169 • **2-step approach:** This time OFL and TSL were calculated separately  
 170 to ensure both were greater than zero.

171 1. We scaled the TSL in the SGMs proportionally ( $l_{s,m}^{t,prop}$ ) to the  
 172 new MTU length ( $L_m^{mt,subj}$ ). This adjustment kept the fraction of  
 173 length represented by the TSL as in the GM (Eq. 5).

$$l_{s,m}^{t,prop} = \frac{l_{s,m}^{t,ref}}{L_m^{mt,ref}} * L_m^{mt,subj} \quad (5)$$

174

175  
176

2. Calculation of the OFL using the linear approach and the proportional TSL ( $l_{s,m}^{t,prop}$ , Eq. 6).

$$l_o^{m,subj} = \begin{bmatrix} l_{1,norm}^{m,ref} * \cos \alpha_{m,1}^{ref} \\ \vdots \\ l_{n,norm}^{m,ref} * \cos \alpha_{m,n}^{ref} \end{bmatrix}^{-1} * \begin{bmatrix} L_{m,1}^{mt,subj} - l_{m,1}^{t,prop} \\ \vdots \\ L_{m,n}^{mt,subj} - l_{m,n}^{t,prop} \end{bmatrix} + e \quad (6)$$

177  
178  
179

3. Recalculation of the final value for TSL using the new value for OFL.

### 180 2.3. *Scaling Protocol for the DSEM.*

181 Preserving the  $l_{m,norm}$ , and  $l_{t,norm}$  of every muscle as in the GM required  
182 mapping these variables in the first place. For that purpose, we needed to  
183 explore the complete length excursion of all the MTUs in the DSEM. The  
184 length of a MTU only changes with the motion of the joints actuated by  
185 that specific MTU. Therefore, a complete mapping of the length's excursion  
186 of the biceps, for instance, implied exploring the whole ROM of the joints  
187 crossed by this muscle.

- 188 1. Identification of joints actuated by a certain MTU: Firstly, we calcu-  
189 lated the muscle path (Eq. 7). We did so by computing the Eculidean  
190 distance from the origin of the MTU to its insertion in the initial step  
191 of the simulation ' $n = 1$ '. The joints actuated by a MTU were those  
192 crossed by its muscle path and  $\theta$  is the joint angle in each step (' $n$ ') of  
193 the simulation:

$$L_{m,n}^{mt}(\theta) = dist(insertion Node_{m,n}(\theta), origin Node_{m,n}(\theta)) \quad (7)$$

194  
195  
196  
197  
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199

We also employed this formula (Eq. 7) to map the length of the MTUs in both, the GM ( $L_{m,n}^{mt,ref}$ ) and the SGMs ( $L_{m,n}^{mt,subj}$ ). For MTUs wrapping around bony contours, we followed the recommendations issued by [30] for '*Curved-Truss*' elements. From these measurements of  $L_m^{mt}$  we derived  $l_m$  and  $l_t$  using Eq. 1.



200 2. Several simulations were run with the GM to explore the ROM of the  
 201 crossed joints. For every sampling point 'n', we calculated  $\alpha_{m,n}^{ref}$  (Eq. 8),  
 202  $l_{m,n,norm}^{ref}$  (Eq. 9), and  $l_{t,n,norm}^{ref}$  (Eq. 10). We needed these parameters  
 203 in order to solve Equation 2. In Eq. 8,  $\alpha_{m,1}^{ref}$  stands for the pennation  
 204 angle in the initial step of the simulation  $n = 1$  :

$$\alpha_{m,n}^{ref} = \arcsin \left( \frac{l_o^{m,ref} * \sin \alpha_{m,0}^{ref}}{l_{m,n}^{ref}} \right) \quad (8)$$

$$l_{m,n,norm}^{ref} = \frac{l_{m,n}^{ref}}{l_o^{m,ref}} \quad (9)$$

$$l_{t,n,norm}^{ref} = \frac{l_{t,n}^{ref}}{l_s^{ref}} \quad (10)$$

205

- 206 • Values of  $l_{m,n,norm}^{ref}$  over 1.5 or under 0.5 were filtered out since  
 207 they are considered to be out of physiological conditions.
- 208 • Values for  $\alpha_{m,n}^{ref}$  over 0.84 rad were filtered out since they are con-  
 209 sidered to be out of physiological conditions.

210 3. We repeated step number 1 of this protocol, this time using the SGMs  
 211 to map the lengths of the scaled MTU ( $L_{m,n}^{mt,subj}$ ) in the same joint con-  
 212 figurations.

213

214 4. Finally, we introduced the  $L_m^{mt,subj}$ ,  $\alpha_m^{ref}$ ,  $l_{m,norm}^{ref}$ , and  $l_{t,norm}^{ref}$  vectors  
 215 into Eq. 2. Then, we applied the three solving techniques to find three  
 216 sets of solutions (OFL and TSL) for every MTU 'm'.

217 The new scaled models whose muscle parameters had been estimated by  
 218 each of the three approaches proposed by Modenese were grouped under the  
 219 names: scaled model 3 (SM3) and scaled model 5 (SM5). For example, the  
 220 'constrained SM3' refers to the SM3 whose muscle parameters have been  
 221 modified using the constrained approach.

222

223 **2.4. Motion Data.**

224 We used Range Of Motion (ROM) trials [2] in order to map the length  
225 excursion of every MTU in the DSEM, apart from other variables, as we  
226 introduced in the protocol introduced in the previous section.

227  
228 Then, we conducted two sets of trials to evaluate the effects on consis-  
229 tency of adjusting OFL and TSL in the DSEM. We selected two movements  
230 from Bolsterlee’s dynamic tests [14]. The two dynamic tests chosen were:  
231 forward shoulder flexion and scaption. We considered the first one to be an  
232 uncomplicated movement since it simply involved the motion of the shoulder  
233 on a single plane. However, the scapular retraction (scaption) included mul-  
234 tiple and simultaneous rotations plus the scapula covering the extremes of  
235 its ROM, which is usually troublesome. Secondly, the force trials selected to  
236 examine the variation in muscle force production included: shoulder forward  
237 flexion (we called it anteflexion to distinguish this one from the dynamic  
238 test) and abduction. We decided to carry these two test to reproduce the  
239 conditions of Wu’s investigation [28], since we employed his results for the  
240 validation of muscle forces.

241  
242 **2.5. Evaluation of the scaling protocol and each of the three scal-**  
243 **ing approaches consequences on consistency and muscle force**  
244 **production.**

245 For the evaluation of the consistency of the models, we followed the guide-  
246 lines established by Winby [21]. He recommended calculating the MMSE of  
247 the  $l_{m,norm}$  between the reference (GM) and each of the scaled models (SGMs  
248 and SMs). The MMSE is the average RMSE of the  $l_{m,norm}$  of all the mus-  
249 cles in the scaled models throughout the two dynamic tests. The lower the  
250 MMSE of a certain model is, the higher its consistency. Therefore, the scal-  
251 ing approach providing the most substantial improvement in the consistency  
252 compared with the SGMs (which we hypothesized that would be the least  
253 consistent models), would be that one yielding the lowest MMSE. Besides  
254 that, we also checked whether if the scaling approaches improved the working  
255 region of the muscles in the SGMs. In doing so, we compared the propor-  
256 tion of the total humeral elevation ROM that out-of-range muscles operated  
257 under physiological conditions before and after muscle parameter scaling.  
258 Out-of-range muscles are those muscles which spent more than one step of

259 the simulation working out of the physiological area in the F-L curve (Fig.  
 260 1). If a particular MTU worked within bounds throughout the entire ROM,  
 261 it received a value of 1.

262

263 Improving the working region of the muscles had consequences into their  
 264 muscle force generation ability. We compared the difference in force pro-  
 265 duction of four rotator cuff muscles in the SGMs and the SMs. In his in-  
 266 vestigation, Wu [28] also scaled an upper-limb model [17] in Opensim using  
 267 Modenese’s algorithm. Therefore, we expected to obtain similar variations  
 268 in muscle forces.

269

### 270 3. Results

271 The protocol employed in the current research to scale OFL and TSL  
 272 delivered physiologically feasible values [34, 28]. Table 1 contains the dif-  
 273 ferences in the length of the segments (clavicle, humerus, and radius) and  
 274 muscle parameters in the SMs compared to the GM. Values over or below  
 275 one means that the segment or parameter is longer or shorter than in the  
 276 GM, respectively.

277

	Subject 3	Subject 5
Length of clavicle	0.89	1.05
Length of humerus	0.93	0.97
Length of radius	0.95	1.02
<b>Total</b>	<b>0.92</b>	<b>1.013</b>
Optimal Fiber Length (avg)	0.9502	1.085
Tendon Slack Length (avg)	1.0491	1.035

Table 1: Variations in length of the model segments (due to geometrical scaling) and of muscle parameters (constrained approach). These values are expressed as ratios between the length in the SM and the GM. (e.g.,  $l_{clav}^{subj}/l_{clav}^{ref}$ ). Therefore, if the length of the clavicle in SM3 is 0.89,  $l_{clav}^{subj} = 0.89 * l_{clav}^{ref}$ . The row named "Total" contains the averaged value of the three segments. For the OFLs and TSLs, the ratios are the average of the 31 muscles in the DSEM.

278 The constrained approach delivered muscle parameters which did not fol-  
 279 low the variation in the segments’ length of either of the two SMs. For subject

280 5 (S5), scaling increased the length of both, muscle parameters and model  
 281 segments, although not in the same proportion. While OFLs and TSLs were  
 282 elongated 8.5% and 3.5%, the bones of SM5 were just 1.3% longer than in  
 283 the GM. Furthermore, in subject 3 (S3), not only did the muscle parameters  
 284 not decrease proportionally to the segments, but the TSLs increased 4.91%  
 285 on average.  
 286

### 287 3.1. Consistency of the Scaled models.

288 Figure 2 shows the normalized length excursions of the scapular section  
 289 of the deltoid during the scaption trial. This muscle operated out of range  
 290 (below  $0.5 l_{m,norm}$ , Fig 2) from  $30^\circ$  in SGM3 (dashed red line) and  $60^\circ$  in  
 291 SGM5 (dashed green line) until the end of the trial and  $70^\circ$  respectively.  
 292

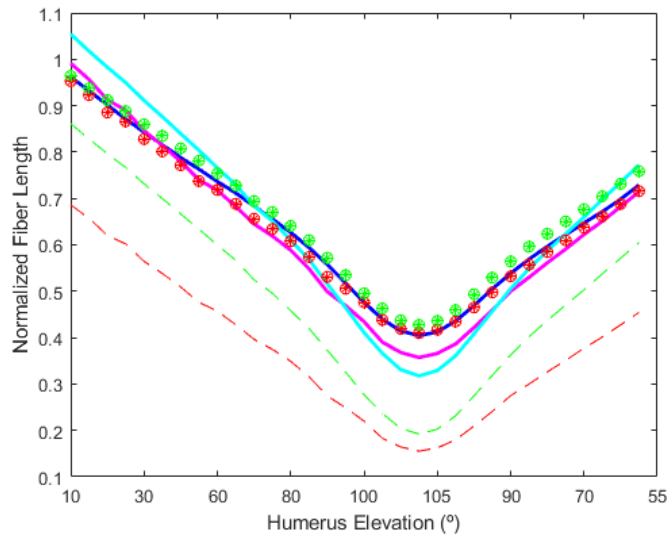


Figure 2: **Variations in the length excursion of the scapular section of the deltoid (one of the muscles working out of range in the SGMs) throughout the scaption trial of Subject 3.** In blue, the normalized length excursion of the muscle in the GM (reference model). The dashed lines depict the deviation in SGM3 (red) and SGM5 (green) due to geometrical scaling. The circles represent the length excursion in SM3 (red) and SM5 (green) after having their parameters scaled with the constrained approach. The linear technique delivered identical results (star marks) in SM3 (red) and SM5 (green). Finally, the solid lines in magenta (SM3) and cyan (SM5) illustrate the excursion of the fibers after scaling the muscle parameters using the 2-step approach.

293 The constrained (circles mark) and linear (stars mark) adjustment of  
 294 muscle parameters provided the best fit with the GM (solid blue line). The  
 295 same remark holds for all the muscles that actuated out of bounds in the  
 296 SGMs, like the deltoid.

297  
 298 The median of the out-of-range muscles in SGM3 was 0.26 (Fig 3). The  
 299 constrained estimation of  $l_o^m$  and  $l_s^t$ , brought that number down to 0.027. The  
 300 other two approaches also achieved substantial reductions in MMSE for out-  
 301 of-range muscles. The 2-step scaling lowered the MMSE from 0.21 in SGM3  
 302 and 0.23 in SGM5 to 0.034 and 0.096, respectively. The linear approach  
 303 decreased those values to 0.08 and 0.068. The most considerable reduction  
 304 was achieved by the constrained technique, which yielded a 0.028 and 0.046  
 305 MMSE for SM3 and SM5 (in red in Table 2).

306

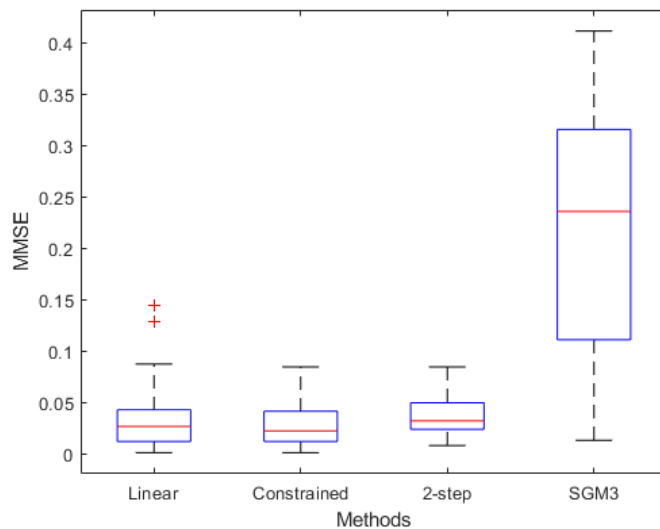


Figure 3: Level of consistency delivered by geometrical scaling (SGM3) and muscle parameter scaling (Linear, Constrained and 2-step). The lowest the MMSE, the highest the consistency. The MMSE is the averaged RMSE of all the muscles out of range (Appendix A) during the dynamic trials of Subject 3. The red line in the boxplots indicates the median, meaning that half of the muscles in the DSEM showed MMSEs lower than this value. The upper and lower sides of the boxplots represent the 25th and 75th percentile. These percentiles indicate that one quarter and three quarters, respectively, of the muscles in the DSEM showed lower MMSEs. The cross markers illustrate the outliers.

	Subject 3				Subject 5			
	lin	cns	2stp	SGM	lin	cns	2stp	SGM
OR Musc	0.038	0.028	0.034	0.21	0.068	0.046	0.096	0.23
WR Musc	0.03	0.029	0.03	0.11	0.038	0.031	0.044	0.112
All Musc	0.03	0.029	0.03	0.127	0.043	0.03	0.053	0.14

Table 2: MMSE of the thirty-one muscles in the DSEM throughout the two dynamic trials ('All Musc'). For more information about the relation between MMSE and consistency refer to Fig. 3. Each column correspond to each of the three scaling approaches (lin = linear, cns = constrained, 2stp = 2-step). The column labelled 'SGM' contains the MMSE of the geometrically scaled models (SGM). In red ('OR Musc'), the averaged results taking into account only muscles operating out of range (Appendix A). In green ('WR Musc'), the results from muscles operating within physiological range.

307 Figure 4 displays the pectoralis major's length excursions throughout the  
308 flexion trial. For muscles that operated under physiological conditions (pec-  
309 toralis major among them), the reductions delivered by the three approaches  
310 were not as remarkable as for muscles out of range (Fig. 3 and Fig. 5). The  
311 median of the MMSE of fibers actuating within bounds was 0.085 already  
312 for the SGM5 (SGM5 in Fig 5). However, the constrained method managed  
313 to lower that value to 0.019. This technique achieved the most significant  
314 reductions again, decreasing the MMSE from 0.11 and 0.112 to 0.029 and  
315 0.028 for SM3 and SM5, respectively (in green in Table 2).

316

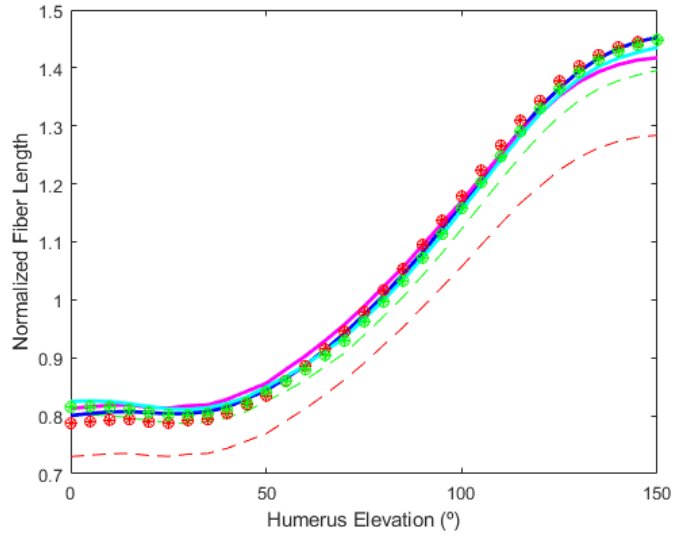


Figure 4: Variations in the length excursion of the pectoralis major (one of the muscles working under physiological conditions in the SGMs) throughout the forward flexion trial of Subject 5. For more information about the lines and markers in the figure, refer to Fig. 2

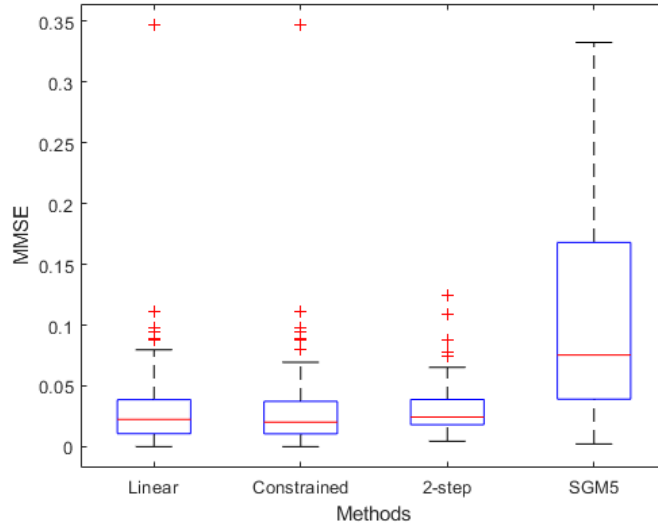


Figure 5: Level of consistency delivered by geometrical scaling (SGM5) and muscle parameter scaling (Linear, Constrained, 2-step). The lowest the MMSE, the highest the consistency. The MMSE is the averaged RMSE of all the muscles within range during the dynamic trials of Subject 5. For more information about the figure, refer to Fig. 3

317 Figures 6 and 7 illustrate the working range of the muscles actuating  
 318 out of bounds in the SGMs throughout the dynamic trials. The Y-axis  
 319 incorporates the twenty-two muscles operating out of range in SGM3 (Fig.  
 320 6) and SGM5 (Fig. 7). The dark blue regions depict the working area of these  
 321 muscles in the SGMs. The green zones represent the improvements delivered  
 322 by the constrained approach. Constrained scaling of  $l_o^m$  and  $l_s^t$  brought every  
 323 muscle to work under physiological conditions but for the serratus anterior in  
 324 Figure 6. It even achieved that out-of-range muscles operated within bounds  
 325 for a higher percentage of the humeral ROM in the SMs than in the GM (in  
 326 green in Table 3).



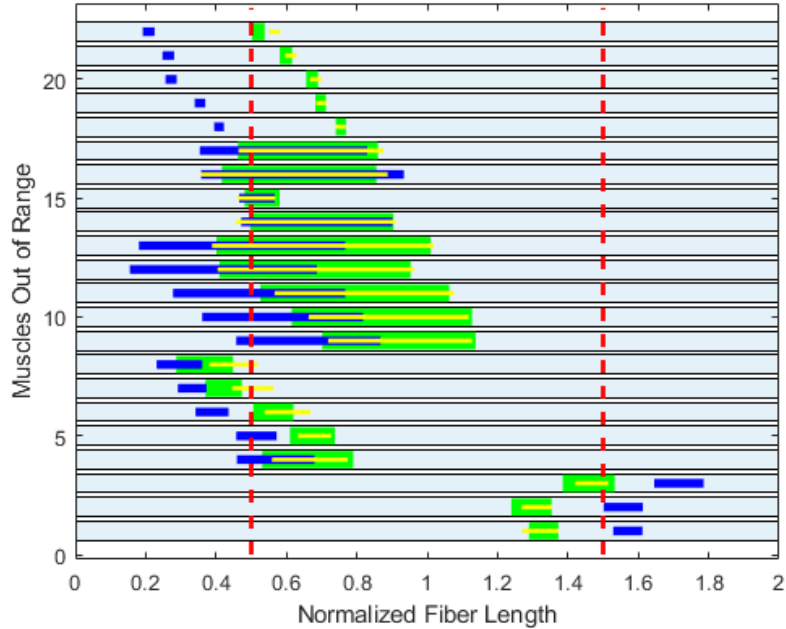


Figure 6: Shifts in the working region of out-of-range muscles in S3 caused by scaling OFL and TSL (constrained approach). The blue area depicts the operating range of muscles out of range (outside of the zone defined by the red dashed lines) in SGM3 due to geometrical scaling (e.g., teres minor and triceps). The yellow lines show the operating region of the same set of muscles in the GM (reference model), which should be preserved after geometrical modifications according to Winby [21]. The green regions represent the improvement in the working area after scaling OFL and TSL with the constrained approach. Therefore, muscles in which the green and yellow regions overlap, are appropriately scaled (e.g., scapular and clavicular part of the deltoides). The name of the twenty-two muscles displayed on the Y-axis are specified in Appendix A, table A.6.

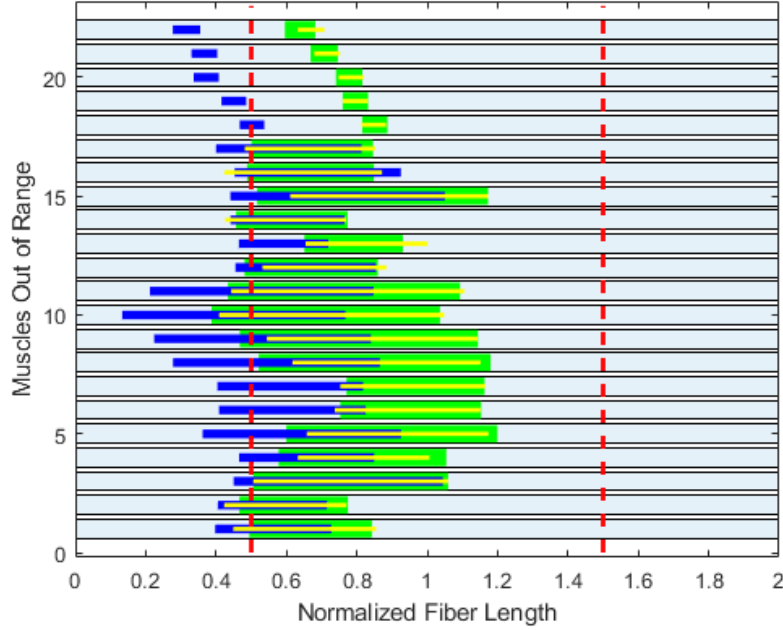


Figure 7: Shifts in the working region of out-of-range muscles in S5 caused by scaling OFL and TSL (constrained approach). Muscles in which the green and yellow regions overlap, are appropriately scaled (e.g., pectoralis minor and serratus anterior). The name of the twenty-two muscles displayed on the Y-axis are specified in Appendix A, table A.7. For more information about the figure and the consequences of muscle parameter scaling on their working area, refer to Fig. 6.

	OR Musc				All Musc			
	lin	cns	2stp	SGM	lin	cns	2stp	SGM
<b>S3</b>	0.9	0.92	0.88	0.59	0.97	0.98	0.98	0.91
<b>S5</b>	0.93	0.94	0.9	0.66	0.96	0.98	0.98	0.93
<b>GM</b>	0.9				0.9805			

Table 3: Averaged proportion (out of 1, being 1 the whole ROM) of the humeral elevation ROM that muscles spent working within the physiological conditions. In 'Musc. OR', the values for muscles working out of range for longer than one step of the simulation. In 'All musc', the results taking into account the thirty-one MTUs in the DSEM. The color code is the same as in Fig. 6 and 7. The information contained in the colored rows and columns together with the mentioned figures illustrate the improvement in the working area of the muscles delivered by muscle parameter scaling. For more information about the columns and rows' labels, refer to Table 2.

327 The 2-step approach outperformed the constrained method for muscles  
 328 whose TSL is zero in the SGM (Appendix B and Fig. 8). In this case, both  
 329 linear and constrained scaling delivered higher MMSE values than geomet-  
 330 rical scaling. The 2-step technique was the only one reducing the MMSE  
 331 compared to the SGM (Fig 9 and highlighted in green in Table 4).

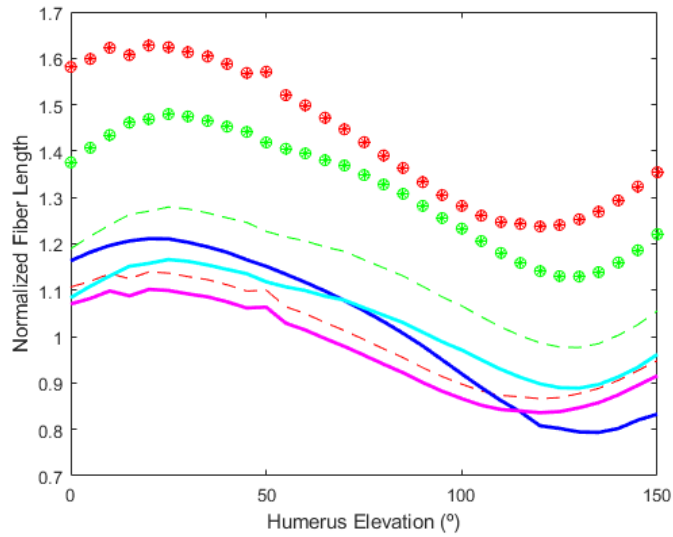


Figure 8: Variations in the length excursion of the serratus anterior (one of the muscles whose original tendon slack length is zero) throughout the forward flexion trial of Subject 5. For more information about the graphic, refer to Fig. 2

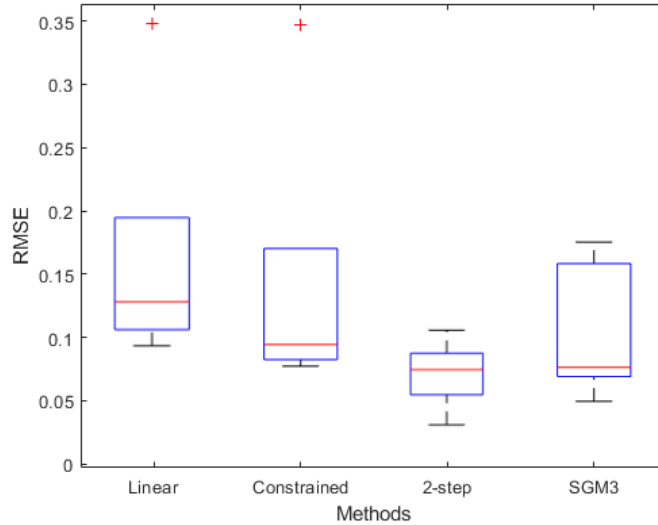


Figure 9: Level of consistency delivered by geometrical scaling (SGM3) and muscle parameter scaling (Linear, Constrained, 2-step). The lowest the MMSE, the highest the consistency. Only muscles whose original TSL was zero (Appendix B) in the GM are considered for this graphic. For more information about the boxplots, refer to Fig. 3.

	Linear	Constrained	2-step	SGM
<b>S3</b>	0.175	0.145	0.06	0.105
<b>S5</b>	0.155	0.109	0.077	0.079

Table 4: MMSE of the muscles whose original TSL is zero (Appendix B) throughout the two dynamic trials for both subjects 3 and 5. In green, the only values lower than the MMSEs in the SGMs, corresponding to the 2-step approach. For more information about the relation between MMSE and consistency refer to Fig.3.

332 *3.2. Consequences on muscle force production.*

333 The averaged forces of five of the rotator cuff muscles (clavicular and  
 334 scapular deltoid, supraspinatus, infraspinatus, subscapularis, and teres mi-  
 335 nor) are shown in Table 5. There were three muscles whose variation in  
 336 the force generation did not match the results from Wu’s research: the  
 337 supraspinatus, and subscapularis in SM3 and the infraspinatus in SM5 (in  
 338 red in Table 5). The teres minor was the muscle that experienced the most  
 339 substantial increase in force production due to constrained scaling.

	<b>Subject 3</b>	<b>Subject 5</b>	<b>Reference [28]</b>
Deltoid	-3.17 %BW	-3.88 %BW	-1.75 %BW
Infraspinatus	-0.36 %BW	3.61 %BW	- 4.21 %BW
Supraspinatus	27.73 %BW	-2.8 %BW	-1.27 %BW
Subscapularis	7.12 %BW	-4.29 %BW	-4.19 %BW
Teres Minor	-19.78 %BW	-15.75 %BW	-
<b>Total Musc Force</b>	<b>-1.1 %BW</b>	<b>-1.2 %BW</b>	<b>- 1.9 %BW</b>

Table 5: Differences in force production (expressed as the percentage of the Body Weight of the subject) before and after scaling OFL and TSL using the constrained approach in five rotator cuff muscles. A positive value means that the force generated by a muscle is larger in the SGM than in the SM. Conversely, a negative value implies that the force in the SGM is smaller than in the SM. The reference column shows the difference in muscle force production from a study using the same scaling technique [28]. In red, the muscle forces that did not follow the variation (after muscle parameter scaling) observed in Wu’s publication. Although the reference study did not consider the Teres Minor, we included it on this table because it is the muscle experiencing the largest increase in force production. The last row indicates the averaged variation in force generation of the thirty-one MTUs in the SMs.

#### 340 4. Discussion

341 We hypothesized that adjusting OFL and TSL in geometrically scaled  
342 models will improve their consistency. Our results have shown that the three  
343 scaling approaches broadly achieve that. Constrained, linear, and 2-step scal-  
344 ing of muscle parameters, in that specific order, deliver the lowest MMSE  
345 values (Fig. 3 and 5). That means, they provide the highest consistencies  
346 compared to geometrically scaled models.

347  
348 The constrained approach yields MMSEs as low as 0.029 for SM3 (Table  
349 2). That indicates that the muscles in SM3 show a behavior 97.1% similar  
350 to the GM, despite the geometrical modifications. Therefore, a particular  
351 muscle reaches its maximal force at the same humeral elevation angle with a  
352 2.9% error in the SM3 as in the GM (Figure 1). For that reason, there is only  
353 a 2.9% loss in consistency in SM3 with respect to GM3. Furthermore, muscle  
354 parameter constrained adjustment preserves the extent of the humeral eleva-  
355 tion ROM in which muscles work under physiological conditions in the SMs  
356 (0.98) in the same level as in the GM (0.9805, Table 3). Avoiding the reduc-  
357 tion of this ratio implies that the force generation capability of the model

358 does not diminish, regardless of geometrically scaling.

359

360 The consistency analysis of the SGMs (whose muscle parameters are not  
361 adjusted) provides very different results. Firstly, the MMSE values in the  
362 SGMs are 78% higher than in the SMs (Table 2). That implies that SGMs  
363 are 78% less consistent than SMs. In other words, not adjusting OFL and  
364 TSL after geometrically scaling the DSEM causes a significant loss on consis-  
365 tency. Secondly, geometrical scaling brought twenty-two muscles to operate  
366 outside the physiological fiber length range (Fig. 6 and 7, and Appendix A).  
367 They work as much as 41% of the humeral elevation ROM out of range (Ta-  
368 ble 3, SGM3). During that extent, their force production capacity is limited  
369 to 1% of their maximum force [30], restricting the force production of the  
370 whole model. Consequently, the load sharing algorithm of the DSEM may  
371 fail to find a solution for the distribution of muscle forces [19]. Nevertheless,  
372 adjusting their OFLs and TSLs to the new MTU lengths reduces the MMSEs  
373 as much as 84% (in red in Table 2). Moreover, the adjustment brings these  
374 muscles back to work within range for at least 92% of the humeral elevation  
375 (in green in Table 3).

376

377 Therefore, geometrically-scaled models are inconsistent, and inconsistent  
378 models are unreliable since the behavior of their muscles is altered compared  
379 with the reference model, the GM (in which they exhibit their theoretically  
380 correct behavior). This is due to differences in its operating region and fiber  
381 length excursion caused by geometrical scaling. We have demonstrated that  
382 such inconsistencies are fixed by adjusting OFL and TSL to the scaled MTUs  
383 length. **In consequence, we acknowledge that the results endorse our  
384 first hypothesis. Adjusting OFL and TSL in geometrically scaled  
385 upper-limb models improves their consistency.**

386

387 Scaling OFL and TSL provokes an increase in the muscle force capacity  
388 of the models as well. Muscles such as the Teres Minor, whose three con-  
389 tractile elements were out of range in the SGMs (elements from eighteen to  
390 twenty in Figures 6 and 7), experience the most considerable increase in force  
391 generation (Table 5). Tuning the OFLs and TSLs of those three elements  
392 allows them to work under physiological conditions. Therefore, the 1% re-  
393 striction on their maximal force ceases, and their force production increases.  
394 The same reasoning applies for any of the muscles that were working out of  
395 range in the SGMs and that, thanks to scaling their muscle parameters, are

396 back to operating under physiological conditions. **Scaling OFL and TSL**  
397 **produces an increase in muscle force production. Not only mus-**  
398 **cle parameters must be adjusted to preserve consistency, but also**  
399 **to avoid the reduction in the force generation due to geometrical**  
400 **scaling.** Accordingly, SGMs show lower force generation capacity than SMs  
401 (Table 5). Although producing consistent scaled models is an important step  
402 in the quest to represent the muscle capacity of a subject, further research is  
403 needed to evaluate the influence of other muscle parameters in the generation  
404 of force, such as the PCSA.

405  
406 To the best of our knowledge, this is the first study evaluating the effect  
407 of scaling OFL and TSL on consistency in upper-limb models. Validating  
408 the presented results is thus a challenging task. The only solution plausible  
409 is comparing our MMSEs to those from an article employing a lower-limb  
410 model [22]. Even though our MMSEs are slightly higher, they are consistent  
411 in magnitude (0.029 and 0.03, Table 2) with the values shown in Modenese’s  
412 study (maximal MMSE of 0.019). Likewise, our correlations are not as high  
413 (0.99), but they are above 0.95 (Appendix C, Tables C.8 and C.9). Con-  
414 sequently, we can ratify that the consistency levels reached in our study are  
415 almost identical to those in Modenese’s paper [35].

416  
417 The new values for OFLs and TSLs fall within range with data from  
418 corpses of similar dimensions to S3 and S5 [28, 34]. Hence, we guarantee  
419 that the muscle parameters delivered by the constrained approach are phys-  
420 iologically valid. The literature on the topic suggests that bone dimensions  
421 and muscle parameter scaling hold a non-linear relation [29, 8]. The results  
422 presented in this study support that statement as well (Table 1).

423  
424 The constrained approach struggles, however, with muscles whose original  
425 TSL is zero. It even weakens their consistency and those fibers show lower  
426 MMSEs in the SGMs than in the constrained SMs. The 2-step technique,  
427 by contrast, delivers the smallest MMSEs in this situation (Figure 9 and in  
428 green in Table 4) and thus, the highest consistency. The non-varying tendons  
429 in our model may be the reason for the poor performance of the linear and  
430 constrained approaches. Modenese has stated that his algorithm struggles  
431 to estimate the OFL and TSL in muscles ”...whose tendon length does not  
432 stretch significantly” [22]. Tendons in the DSEM are stiff elements, meaning  
433 they do not stretch at all [30]. Additionally, for muscles whose original TSL

434 is zero (Appendix B), the linear and constrained techniques find solving Eq.  
435 4 truly challenging. Probably, our MMSEs and correlations values are not  
436 as ideal as in Modenese’s article due to the stiff tendons in the DSEM as well.

437  
438 Wu’s investigation [28] allows us to validate the muscle force variation.  
439 We have compared the differences in forces of four rotator cuff muscles be-  
440 fore and after scaling OFL and TSL. Although most of those muscles show a  
441 similar increase in force generation, three of them do not follow that fashion  
442 (in red in Table 5). The subscapularis, supraspinatus (S3) and infraspinatus  
443 (S5) produce larger forces in the SGMs than in the SMs. This discrepancy  
444 may be due to different load-sharing algorithms. Wu’s model distributes the  
445 net joint moments “...proportionally among synergistic muscles” [17]. Con-  
446 versely, the DSEM load-sharing algorithm distributes the muscle forces to  
447 minimize the energy expenditure [19]. The difference in this criterion may  
448 be the cause of the discrepancy in the force difference in the rotator cuff  
449 muscles. Nevertheless, both studies agree on the increase in the total muscle  
450 force production in SMs with respect to SGMs (Table 5).

451  
452 The scaling algorithm employed in this study introduces two limitations.  
453 In the first place, it has not been demonstrated that the normalized fiber  
454 length excursion and the force-angle relation (Figure 1) are the same in dif-  
455 ferent people. Secondly, Modenese’s algorithm regards the working ranges of  
456 the muscles in the reference model (GM) as representative of a healthy indi-  
457 vidual. However, our generic model was created using data from a cadaver.  
458 In consequence, the scaling protocol in this paper should be used carefully  
459 with samples such as elite athletes.

460  
461 The sample (two subjects) of this investigation is too reduced for the  
462 results to be representative. We therefore recommend repeating the current  
463 study with a larger sample. Furthermore, a future study could include Max-  
464 imal Voluntary Contraction (MVC) tests. We have assessed the effects of  
465 muscle parameter scaling in the muscle force production for dynamic tests,  
466 but the impact on MVCs is still unknown.

467  
468 Lastly, the validation performed is limited. We only found three articles  
469 about scaling muscle parameters in upper-limb models [27, 28, 14], and none  
470 of them evaluated the effects on consistency. Since the literature on the topic  
471 is scarce, alternative validation techniques should be considered. Applying



472 the scaling protocol contained in this article to Nikooyan geometrically scaled  
473 models represents a reliable option [19]. In this way, the estimated contact  
474 forces could be compared with experimental data from instrumented endo-  
475 prostheses.

## 476 5. Conclusion

- 477 • Any research which intends to modify the geometrical parameters of  
478 the DSEM (or any other upper-limb MSK model) must adjust the OFL  
479 and TSL accordingly, in order to preserve the consistency and muscles  
480 behavior in the scaled version. Inconsistent models are unreliable and  
481 not capable of representing the muscle force capacity of the scaled sub-  
482 ject.
- 483 • Scaled versions of the DSEM whose OFLs and TSLs have been adjusted  
484 are 78% more consistent and their MTUs produce up to 1.2 %BW larger  
485 forces than geometrically scaled versions.
- 486 • The scaling protocol contained in this paper delivers losses in consis-  
487 tency lower than 5%. Furthermore, it does not require other experimen-  
488 tal data than ROM recordings and it is computationally inexpensive.

## 489 Appendix A. List of muscles working out of range.

490 The following tables contain the names of the muscles actuating out of  
491 range displayed on Figure 6 for Subject 3 and Figure 7 for Subject 5. These  
492 are also the muscles labeled as 'OR Musc' or out-of-range muscles in Tables  
493 2 and 3.

<b>Nr. in Fig. 6</b>	<b>Name of the muscle</b>
1, 2, 3	Trapezius Scapular Part
4	Pectoralis Minor
5, 6, 7, 8	Serratus Anterior
9, 10, 11, 12, 13	Deltoides Scapular Part
14	Deltoides Clavicular Part
15	Infraspinatus
16,17	Subscapularis
18, 19, 20	Teres Minor
21, 22	Triceps lateral part

Table A.6: Name of the muscles corresponding to the numbers shown on the Y-axis in Figure 6.

<b>Nr. in Fig. 7</b>	<b>Name of the muscle</b>
1, 2, 3	Trapezius Scapular Part
4, 5	Pectoralis Minor
6, 7	Serratus Anterior
8, 9, 10, 11	Deltoides Scapular Part
12, 13	Deltoides Clavicular Part
14	Infraspinatus
15, 16, 17	Subscapularis
18, 19, 20	Teres Minor
21, 22	Triceps lateral part

Table A.7: Name of the muscles corresponding to the numbers shown on the Y-axis in Figure 7.

494 **Appendix B. List of muscles whose original Tendon Slack Length**  
495 **is zero in the DSEM.**

496 The muscle fibers whose Tendon Slack Length (TSL) is zero in the refer-  
497 ence model (generic version of the DSEM) are: four elements of the Serratus  
498 Anterior and one element of the Subscapularis.

499 **Appendix C. Correlation values.**

500 We calculated the correlation coefficients between the fiber length ex-  
501 cursion in the scaled models and the GM (reference model) to evaluate the

502 similarity of their curves (such as the curves displayed on Fig 2, 4, and 8).  
 503 We compared these values to the correlation coefficients from Modenese’s  
 504 publication [22].

	Max	Min	Mean
SM3	1	0.3	0.97
SM5	1	0.15	0.95

Table C.8: Correlation coefficients of the scaption test for SM3 and SM5. Several muscles show a correlation of 1 (maximal value) but the minimal correlation corresponds to the brachioradialis and the serratus anterior in SM3 and SM5 respectively. The mean value is the averaged correlation coefficient of all the muscles in the DSEM.

	Max	Min	Mean
S3	1	0.45	0.98
S5	1	0.14	0.97

Table C.9: Correlation coefficients of the flexion test for SM3 and SM5. Several muscles show a correlation of 1 (maximal value) but the minimal correlation corresponds to the serratus anterior and the subscapularis in SM3 and SM5 respectively. The mean value is the averaged correlation coefficient of all the muscles in the DSEM.

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