

# Implementation of sensorless field oriented motor control in a solar car

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# Implementation of sensorless field oriented motor control in a solar car

by

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*This thesis is confidential and cannot be made public until January 30, 2023.*

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# Preface

## Abstract

In this thesis the implementation of Field Oriented Control in the car of the NUON Solar Team will be discussed. The team decided to do research into the possibilities of a custom motor controller, and this thesis covers the beginning of that process. First a comparison between different control methods is made, and sensorless FOC is decided as the method to be used. Then the implementation of FOC is discussed. The Texas Instruments InstaSPIN™ technology has the preference for this implementation. This because it has all the elements of the control embedded in one microcontroller, along with a software estimator which eliminates the use of expensive sensors like a shaft encoder. Also the ease of use and the familiarity of TU Delft staff with this technology played a big part in this decision. With this technology, a simulation set-up was made as a proof of concept, which can also be used to teach the NUON Solar Team members the basics of motor control. After that the connections from the controller to the inverter are discussed, so it can be connected to other inverters in the future. In the controller, a CAN-interface is also implemented, which is essential for using it in the Nuna car. With the information presented in this thesis, the NUON Solar Team can continue the development of a controller. It is recommended to eventually leave the development kits used during this project, and integrate the MCU directly into an inverter. This will allow for well-tuned, efficient control of the motor with a small footprint.

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# List of abbreviations

AC	Alternating Current
ADC	Analog-to-digital converter
BLDC	Brushless DC
CAN	Controller Area Network
DC	Direct Current
DTC	Direct Torque Control
EMF	Electromotive Force
EV	Electric Vehicle
FOC	Field Oriented Control
GPIO	General-purpose input/output
IDE	Integrated Development Environment
ISO	International Organization for Standardization
ISR	Interrupt service handler
MC	Motor Controller
MCU	Microcontroller unit
OCTW	Overcurrent & overtemperature warning
PCB	Printed circuit board
PI	Proportional Integral
PMSM	Permanent Magnet Synchronous Motor
PWM	Pulse Width Modulation
ROM	Read-Only-Memory
RTR	Remote Transmission Request
SPI	Serial Peripheral Interface
SVM	Space vector modulation



# 1

## Introduction

In electric vehicle (EV) applications, the motor and its control can have a huge impact on the efficiency of the entire system. If there are too many losses, a lot of different problems can occur. The motor might overheat, the car might not be able to climb a hill, and the range of one battery charge might be significantly reduced. This means a good motor/controller combination is essential to ensure the best performance of any electric vehicle.

There is a specific class of EV's where efficiency is more important than in any other category: solar cars. The Nuon Solar Team from the Delft University of Technology has been competing in the Bridgestone World Solar Challenge in Australia for quite a few years, and in 2017 they became World Champion for the seventh time in the challenger class. To keep this title safe, they are always looking for new ways to improve their car: Nuna. Since 2014 they are also competing in the Sasol Solar Challenge in South Africa, and that brings a new set of challenges to the table as the conditions of the race are quite different.

As a part of the Bachelor Graduation project a group of students got an assignment from the Nuon Solar Team to research the possibility of a custom motor controller for the Nuna solar car. At the moment the motor/controller combinations used in the different Nuna vehicles are not quite as efficient as the team would like. In the next section an overview of the current problems is given.

### 1.1. The problem

A few years ago the Nuon Solar Team switched to a different motor for their car. The motor previously used was an axial flux permanent magnet synchronous motor (PMSM) manufactured by Marand. Right now they are using a radial flux brushless DC (BLDC) motor manufactured by Mitsuba. The controller previously used is the Tritium WaveSculptor22, and the Mitsuba motor comes with its own controller, the Mitsuba M1596C.

The Mitsuba motor works with both of these controllers. Both of the combinations are not optimal however. The Mitsuba motor controller is less efficient than the Tritium controller. Also this controller has analogue parameter control, which means it cannot interface with Nuna's Control Area Network (CAN) in a native way. Right now they have an extra converter in the car to convert the CAN signals to analogue signals and vice versa, which is far from optimal. The Tritium controller thus has an advantage over the Mitsuba controller in both efficiency and controllability. However, that does not mean it's perfect. The Tritium controller switches to a different control method at a speed of around 25 km/h. This switching does not work well with the motor, so the car has to slow down again to allow this switching. This scenario is far from ideal, because at 25 km/h the car is almost always still accelerating. Also the Tritium controller is not capable of providing enough power to drive uphill, which is essential for the race in South Africa.

Both of the controllers are off-the-shelf products, which means they are essentially black box systems to the Nuon Solar Team. They only have a rough idea of how the controllers work, and are not able to modify them in a safe or efficient way.

## 1.2. The current solution

Currently the team uses different controllers for the races in Australia and South Africa.

- For the race in Australia they use the Tritium controller, as this has a higher efficiency than the Mitsuba controller. The fact that it cannot deliver as much power to the motor is not an issue here, because the race doesn't go through any mountainous areas. The issue with the switching during acceleration still remains however.
- For the race in South Africa the Mitsuba controller is used. This controller is needed because the Tritium controller cannot deliver enough power for the mountainous regions in South Africa. However, due to the lower efficiency, they are not able to drive according to their calculated energy consumption model. Especially uphill, the cruising speed is lower than the ideal speed because the motor might overheat otherwise.

## 1.3. The assignment

It is clear both of these controllers cannot deliver all the specifications needed for Nuna. That is why in this bachelor graduation project research is done on a better motor/controller combination than the ones currently existing. To build a complete controller would be far too much to ask from four students in a 10 week project, and that is why a focus is placed on a few subsystems. Two students made a simulation of the Marand and Mitsuba motors, to get the motors' specifications. The values gotten from these simulations are to be used as input for the controller. This thesis covers research into different control methods and an implementation of one of these methods. This means the inverter and motor are not considered in this thesis apart from some compatibility requirements. For the research about the motors in Nuna see [1]. The requirements for the control are as follows:

- **Efficiency** The whole system must be as efficient as possible.
- **Digital Interface** The controller must be able to interface with the CAN-bus in Nuna.
- **Monitoring** The voltages, currents, temperature and speed must be measured.
- **Flexibility** The controller must be able to handle different motor sizes, pole pairs etc.
- **User Interface** There has to be an interface where the configuration of the MC can be changed. For example the limits of the controller and error flags should be programmable.
- **Extra** The controller must be able to control both BLDC motors and PMSMs [1].

## 1.4. Deliverables

The requirements set in the previous section need to be translated into specific deliverables, so it is clear what the Nuon Solar Team can expect. This is also important for the project as it gives the students focus on what to work on. The following deliverables have been deducted from the requirements:

- A comprehensive study of control methods for BLDC motors and PMSMs has to be made. Here a comparison will be made to determine what control method can best be used for the Nuna car.
- After determining the best control method, a possible implementation solution needs to be found to make sure the chosen control method can be used practically.
- A small simulation set-up for testing and adjusting the control has to be made. This simulation can also be used to give the people in the Nuon Solar Team some basic motor control knowledge quickly.
- An extensive manual on how to make the simulation set-up is needed. This is paramount for a quick installation and will allow future contributors to this research to get started right away.
- A recommendation must also be given on how to implement the found solution.

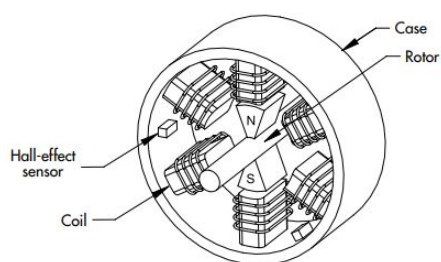
# 2

## Comparison of control methods

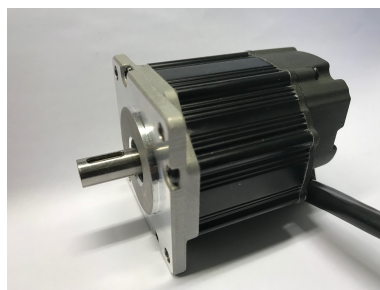
### 2.1. Introduction

First of all, the control method to be used by Nuna needs to be determined. Chapter 1 points out the control needs to be able to handle both BLDC machines and PMSMs. This chapter will compare different controlling techniques and make a decision on what technique should be used. For an introduction to motor types and how they work, see chapter 2 in [1].

Sensored motor control works with either Hall Effect sensors in the motor (BLDC control), or a rotary encoder placed on the shaft (PMSM control). Sensors and their wiring can, however, become quite expensive. Leaving the sensors out allows for a simpler construction and less wires from the motor. During recent years sensorless techniques have been developed thus far that efficiency is not an issue. This means that a sensorless technique is preferred, as it makes the construction simpler and cheaper. It will increase the complexity of the control algorithm, but due to the abundance of high quality microprocessors that is not a problem. Different sensorless techniques are available, and they all have their own advantages and disadvantages. A comparison is made between four popular methods.



(a) Hall Effect sensors in a motor ([2] Fig. 1).



(b) This motor has an encoder built in.

Figure 2.1: Sensored motor control techniques use Hall Effect sensors or encoders.

### 2.2. Sensorless control methods

#### Direct back-EMF

Direct back-EMF control is fairly simple compared to other sensorless techniques [3]. This works by detecting when the back-electromotive force of a phase crosses zero. Then after a set wait time the control switches to the next power stage [4]. It does, however, have a few drawbacks. It is sensitive to noise when detecting the zero crossing, and at low speeds, the low back-EMF will make it difficult to determine the actual zero crossing.

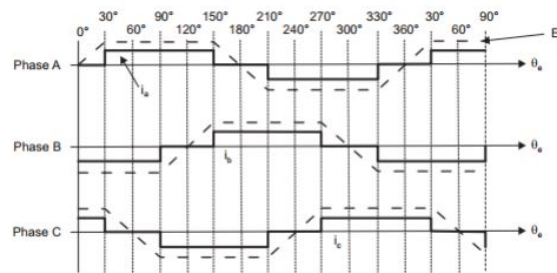


Figure 2.2: The phase back-EMFs and the switching behaviour with direct back-EMF control ([3] Fig. 3-2).

### Indirect back-EMF

The problems that occur with direct back-EMF control can be partially solved by using indirect back-EMF control. Here the back-EMF is integrated about the zero crossing until a certain threshold is reached. This reduces the noise sensitivity. However, both back-EMF methods don't work optimal at low speeds because there is a low back-EMF from the motor [5].

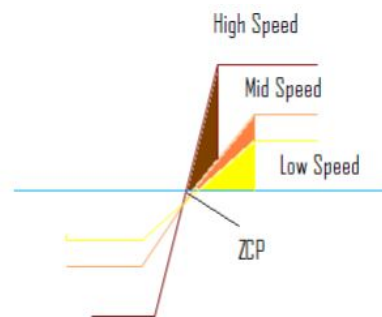


Figure 2.3: The integration of the back-EMF with indirect back-EMF control ([3] Fig. 3-4)

### Direct Torque Control

Direct Torque Control (DTC) works with torque and flux reference vectors. Using a model estimation of the motor, the torque and flux in the motor are calculated with measurements of two phase currents, the intermediate circuit DC voltage and the state of the power switches [6]. Then the calculated torque and flux are compared to the reference and control is applied accordingly. DTC has quite large torque ripple [7]. This strains the construction of the car and often introduces audible noise.

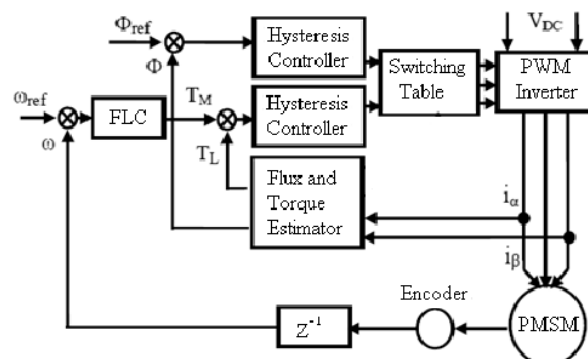


Figure 2.4: The block diagram of DTC.  $\omega$  can also be estimated, so no encoder is needed ([8] Fig. 2).

### Field Oriented Control

Field Oriented Control (FOC) is, like DTC, also vector-based. It transforms the torque and flux vectors so they are orthogonal to each other, and compares them to reference vectors. A more in-depth explanation of FOC will be given in chapter 3. While FOC is a little slower than DTC, it performs better on areas like torque-ripple and distortion [9]. However, FOC needs to know the position of the rotor, and so extra processing power is needed. This is not a big issue though, as microprocessors are fast, efficient and cheap.

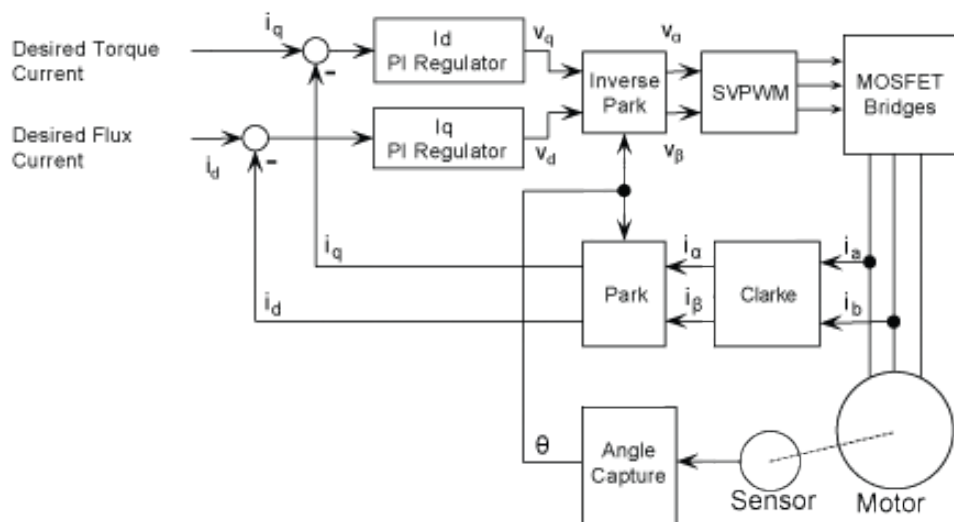


Figure 2.5: A basic implementation of Field Oriented Control with an encoder. The angle can also be estimated, removing the need for an encoder ([10]).

### 2.3. Results

In table 2.1, some of the main differences of the control methods have been summarized. There are several points of interest, some of which are more important than others.

Table 2.1: Comparison of different sensorless control methods

	Direct B-EMF	Indirect B-EMF	DTC	FOC
Computational simplicity	++	+	-	--
Reaction time	-	-	++	+
Efficiency at high speed	+	+	+	+
Torque control at zero/low speed	--	--	-	+
Torque ripple	-	-	-	++

Looking back at the assignment presented in chapter 1, it is clear that torque control at zero/low speed is important. This will allow the Nuna vehicle to accelerate better when pulling away from a traffic light or to overtake other traffic more easily. From the comparison it became clear that FOC was the way to go. The separate torque control will allow the team to tune their car on the fly for different conditions. Also the torque ripple is very low (zero even when using a PMSM). This will strain the construction of the car less, and will provide a more comfortable ride for the driver.

### 2.4. FAST™ software encoder

Texas Instruments sells a unique solution for FOC, which implements the FAST™ software encoder. This technique is provided exclusively by Texas Instruments, and provides a more accurate control than any other solutions from other manufacturers. FAST™ is not a physical encoder, but rather an estimation algorithm implemented in the ROM of a microcontroller. Using the measured phase currents and voltages it estimates the flux, angle, speed and torque in the motor. Also it can identify some motor parameters like the inductances and stator resistance just by running a certain script. The stator

resistance can even be recalculated while the motor is running. This allows the FOC to be constantly tuned to the motor parameters, which keeps the control as accurate as possible.

## 2.5. Implementation

For implementation of FOC Texas Instruments InstaSPIN™ technology will be used. Texas Instruments have different development boards and shields available for this technology. The technology works with the FAST™ software encoder, which makes it very accurate. The basics of the control have already been programmed, and with some minor adjustments it will work with different kinds of motor. This means if the Nuon Solar team decides to switch motors, they will just need to adjust a few values. The supervisor of this project, as well as other staff of the TU have used InstaSPIN™ technology before, so technical support can be found just down the hall. The FAST™ algorithm, the familiarity of TU Delft staff and the ease of use were the reasons this specific technology was chosen for the project. More decisions regarding the controller board are discussed in chapter 4.



# 3

## Field Oriented Control

### 3.1. Introduction

Field oriented control (FOC) applies to brushless motors, not only AC but also DC, that operate in a sinusoidal mode. This means that all three wires are energized with currents that have a sinusoidal waveform. Each of the waveforms are 120 degrees apart from each other [10]. However in sinusoidal commutation, PI controllers have a limited bandwidth to keep a system stable. In motor control at higher speeds the time variant variables speed and frequency go up. This will result in a phase lag in the control loop and a gain error in the motor currents [11]. A visual implementation of field oriented control with an encoder is shown in fig. 2.5. Field oriented control uses the three phases of the inverter current output to change these into 2 parts: a torque generating current and a magnetic field generating current. These currents are time-invariant due to the transformations explained in section 3.2. After that the input user currents are calculated from the torque and speed in section 3.3. And finally the desired user currents are controlled using two PI controllers explained in section 3.4.

### 3.2. Coordinate System

A 3-phase synchronous machine is mostly represented in a two dimensional coordinate system with three axes, all 120 degrees apart from each other. Therefore none of the axes are orthogonal to each other. Field Oriented Control uses a rotating reference frame to control the components of the motor stator currents aligned with the rotor flux. By changing it to a rotating frame the currents, which are controlled, are time-invariant. Therefore the PI controllers work equally well at low and high speeds [11]. To change the 3-phase reference frame into a rotating reference frame there are two transformations needed: first the Clarke transformation to change from 3 phases into an two dimensional coordinate system with two orthogonal axes and secondly the Park transformation to make it rotational. See fig. 3.1 for a visual representation of the coordinate systems.

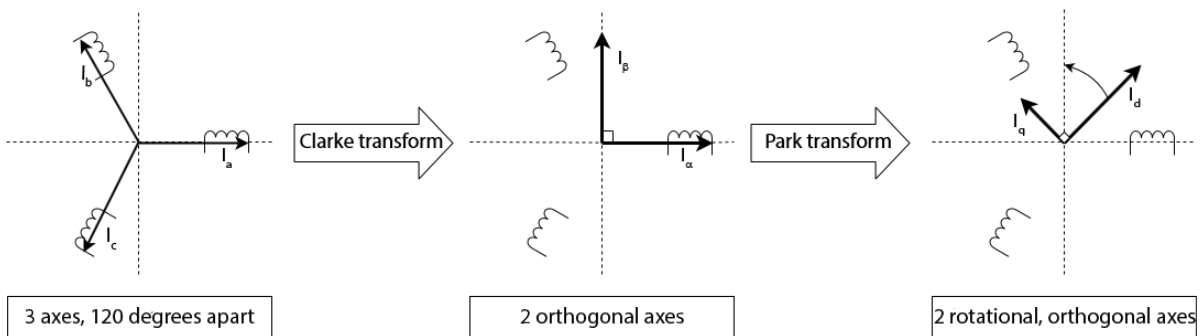


Figure 3.1: A visual representation of The Clarke and Park transformations

### Clarke Transformation

The Clarke transform is expressed in mathematical form using the following equations[12]:

$$i_\alpha = \frac{2}{3}i_a - \frac{1}{3}(i_b - i_c) \quad (3.1)$$

$$i_\beta = \frac{2}{\sqrt{3}}(i_b - i_c) \quad (3.2)$$

or in matrix form:

$$\begin{bmatrix} i_\alpha \\ i_\beta \end{bmatrix} = \frac{2}{3} \begin{bmatrix} 1 & -\frac{1}{2} & -\frac{1}{2} \\ 0 & \sqrt{3} & -\sqrt{3} \end{bmatrix} \begin{bmatrix} i_a \\ i_b \\ i_c \end{bmatrix} \quad (3.3)$$

with  $i_\alpha$  and  $i_\beta$  the components in the orthogonal coordinate system.

In the case that  $i_\alpha$  is superposed with  $i_a$  and  $i_a + i_b + i_c$  equals zero, the Clarke transformation is expressed like:

$$i_\alpha = i_a, \quad (3.4)$$

$$i_\beta = \frac{1}{\sqrt{3}}(i_a + 2i_b) \quad (3.5)$$

$$i_a + i_b + i_c = 0 \quad (3.6)$$

### Park Transformation

To create a rotating reference frame for the Park transformation, the geometrical functions sine and cosine are needed. The direct and quadrature component in the Park transformation are represented by the following equations [12]:

$$i_d = i_\alpha \cos \theta + i_\beta \sin \theta \quad (3.7)$$

$$i_q = i_\beta \cos \theta - i_\alpha \sin \theta \quad (3.8)$$

or in matrix form:

$$\begin{bmatrix} i_d \\ i_q \end{bmatrix} = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} i_\alpha \\ i_\beta \end{bmatrix} \quad (3.9)$$

where  $i_d$  is the direct component,  $i_q$  is the quadrature component and  $\theta$  is the angle between the positive x-axis and the  $i_d$  current vector. The direct component is used to control the flux input of the motor and the quadrature component is used to control the torque input of the motor.

### Inverse Park Transformation

To get back from a rotating reference coordinate system to a non-rotating frame, the inverse park transformation is needed. The transformation is given in the following mathematical equations [12]:

$$v_\alpha = v_d \cos \theta - v_q \sin \theta \quad (3.10)$$

$$v_\beta = v_d \sin \theta + v_q \cos \theta \quad (3.11)$$

Where  $v_d$  and  $v_q$  are the direct, and respectively quadrature, voltage as the output of the two PI controllers. And  $v_\alpha$  and  $v_\beta$  are the orthogonal components of the three phase voltage system. These values are then used in the space vector modulation to drive the inverter.

## 3.3. Current control

The  $i_{q,ref}$  and  $i_{d,ref}$  or commanded torque and flux current can be calculated in multiple ways: The Q-axis current control or Maximum Torque per Amp (MTPA) control [13]. This depends on the state of the motor. In normal operation or during acceleration Q-axis current control is to be used. However, when driving above the rated speed field weakening is desired and MTPA control is preferred to be used.

### Q-axis current control

First in the Q-axis current control,  $i_{d,ref}$  is set to zero. Therefore the flux can't be controlled. However the torque can be controlled using the following formula [13]:

$$T = \frac{3P}{4}\psi_m i_{q,ref} - (L_q - L_d)i_{d,ref}i_{q,ref} \quad (3.12)$$

where  $T$  is the input torque,  $P$  is the total number of poles,  $\psi_m$  is the magnitude of the complex rotor flux vector,  $L_q$  and  $L_d$  are the motor inductances and  $i_q$  and  $i_d$  are the direct and quadrature reference currents. As  $i_{d,ref}$  in Q-axis current control is zero and  $L_q$  and  $L_d$  are assumed equal, as the motors used by the Nuon Solar Team are both surface PMSM [1]. The formula can be rewritten into:

$$T = \frac{3P}{4}\psi_m i_{q,ref} \quad (3.13)$$

$$i_{q,ref} = \frac{4T}{3P\psi_m} \quad (3.14)$$

This can be further simplified using:

$$K_e = \frac{4}{3P\psi_m} \quad (3.15)$$

Where  $K_e$  is the electrical motor constant. Now the commanded torque current becomes:

$$i_{q,ref} = \frac{T}{K_e} \quad (3.16)$$

To calculate the torque commanded current from the demanded speed, a Speed PI regulator is needed. This is shown in the block scheme of fig. 3.2. The gain factor  $K$  and time constant  $\tau$  are dependent on the user case. Each motor needs different parameters as every motor is different.

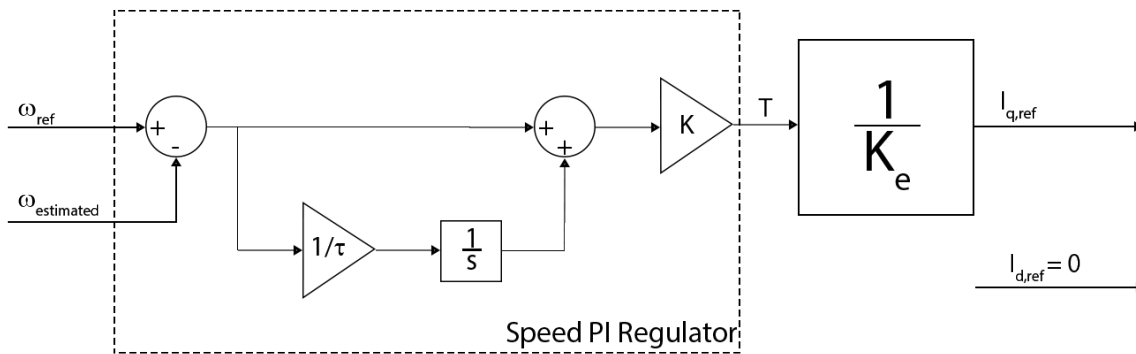


Figure 3.2: A Block scheme of the Speed control loop with the outputs  $I_q$  and  $I_d$ .

### MTPA control

To push the DC motor beyond its rated speed, field weakening can be used. The mechanical power is defined as torque times the speed. As the power is constant for rated speed, the speed cannot be increased due to the increasing back-emf, which is speed dependent.  $i_{d,ref}$  will start to grow negatively, so the back-EMF is reduced. Now the electrical torque will reduce and the speed will increase. The speed increases until the back-EMF increases again and therefore there cannot be any more current drawn [14]. This is all done by using MTPA (Maximum Torque per Ampere) control. The following equations are used for  $i_{d,ref}$  and  $i_{q,ref}$  [13]:

$$i_{d,ref} = \frac{1}{4(\xi - 1)L_d}(\psi_m - \sqrt{\psi_m^2 + 8i_s^2(\xi - 1)^2L_d^2}) \quad (3.17)$$

$$i_{q,ref} = \sqrt{i_s^2 - i_d^2} \quad (3.18)$$

Where  $\xi$  is the saliency ratio  $L_q/L_d$  and  $i_s$  is the input current. Now the torque can be maximized using the given magnitude of the current.

### 3.4. PI Control

After the MOSFET bridges the three currents are measured as shown in fig. 2.5. These currents are changed into the flux current ( $i_d$ ) and into the torque current ( $i_q$ ) using the Clarke and Park transformations, which are explained in section 3.2. After this the torque and flux currents are the input in two different PI Regulators to control the motor. An example of the  $i_q$  PI Regulator is shown in fig. 3.3. In this PI controller the variables  $K$  and  $\tau$  need to be determined by the user. These variables are different for every motor and depend on the motor parameters. The input of the  $i_q$  PI controller is the  $i_{q,ref}$  minus the estimated  $i_q$ . In fig. 3.3  $1/s$  is the Laplace transform of the integral. Furthermore the

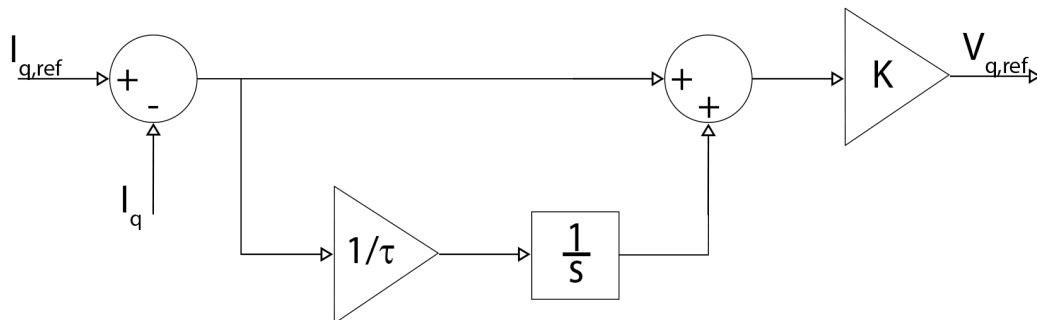


Figure 3.3: A Block scheme of the  $I_q$  PI regulator in fig. 2.5

output  $v_{q,ref}$  is then transformed back to a non-rotating frame (using the inverse park transformation, see section 3.2) to use it as an input for the SVPWM. The PI controller of  $i_d$  looks the same, except that the input is  $i_{d,ref}$  minus  $i_d$ , the output is  $v_{d,ref}$  and the variables  $K$  and  $\tau$  are different.

# 4

## Controller Hardware

### 4.1. Controller choice

As discussed in chapter 2, the InstaSPIN™ technology by Texas Instruments is used for the controller. There are several microcontrollers available with this technology already implemented in the ROM. This will greatly simplify the development of the controller for the Nuna car. Thus, a decision has to be made on which one of these MCUs will be used. On the Texas Instruments website, fig. 4.1 can be found [15], in which a comparison of the specifications of the MCUs is laid out.

	InstaSPIN Solution	MHz	FPU	CLA Co-Processor	Motors	Flash (KB)	12b ADC Chs	PGA	CAN	QEP	USB	SPI	UART	I2C	Pins	Temp
F28069M	-MOTION	90	Y	Y	1 or 2	256	16 or 12	--	1	1	1	2	2	1	100/80	-40 to 105°C
F28068M	-MOTION			--		256										
F28069F	-FOC			Y		256										
F28068F	-FOC			--		256										
F28062F	-FOC			--		128										
F28054M	-MOTION	60	--	--	1 or 2	128	16	4	1	1	--	1	3	1	80	
F28054F	-FOC					128										
F28052M	-MOTION					64										
F28052F	-FOC					64										
F28027F	-FOC					64										
F28026F	-FOC	60	--	--	1	32	13	--	--	--	1	1	1	48		

Figure 4.1: "TI's InstaSPIN™-enabled real-time controllers"

In addition to fig. 4.1, there are only a few MCUs available on the LaunchPad™ development platform. From the InstaSPIN™ enabled MCUs, only the F28027F and F28069M are available on a ready-to-go development board. This means the choice only depends on one particular requirement: CAN-interface capabilities. The F28069M is CAN compatible, and the F28027F is not. It is worth mentioning that fig. 4.1 shows the F28069M uses InstaSPIN-MOTION. This actually means it can use this as well as InstaSPIN-FOC and there is no conflict in control method. InstaSPIN-MOTION adds extra features that serve well in small household appliances [16], but are not needed for EV applications. InstaSPIN-FOC is what will be used. In conclusion the LAUNCHXL-F28069M is the only board that fits all of the requirements, so this will be used for the project.

Texas Instruments also have their own environment for programming MCUs, with a lot of different functions. For this application, the two most important tools are the Code Composer Studio IDE and

MotorWare™, which is the software and documentation package for developing InstaSPIN™ applications.

## 4.2. Process

In order to program a controller for the Nuna motor, several steps have to be taken. A small set-up with low-power BLDC motors will be built, which can be used to simulate races with actual data from the Nuon Solar Team. This will be useful for the students to understand the motor behaviour, and can be used by any future members of the Nuon Solar Team. In this way, work on the controller can continue after the project is done.

### 4.2.1. Components

The Launchpad development board has already been decided on in section 4.1. The next choice that has to be made is the inverter shield that will go on top of the LaunchPad. There are several BoosterPack™ shields available from Texas Instruments. For this project it is important to be able to connect the inverter to both the small motors used in the simulation as well as the motors used in Nuna. In this way the motor can be controlled up to a certain power. The final controller in Nuna will be connected to a high-power inverter, but it will be good to show the Nuon Solar Team some control features without the use of a high-power inverter. Of course the inverter board should still be able to deliver as much power as possible. This is why the decision had been made to use the BOOSTXL-DRV8323RH shield. This works up to 54V and with a continuous current of 15A [17].

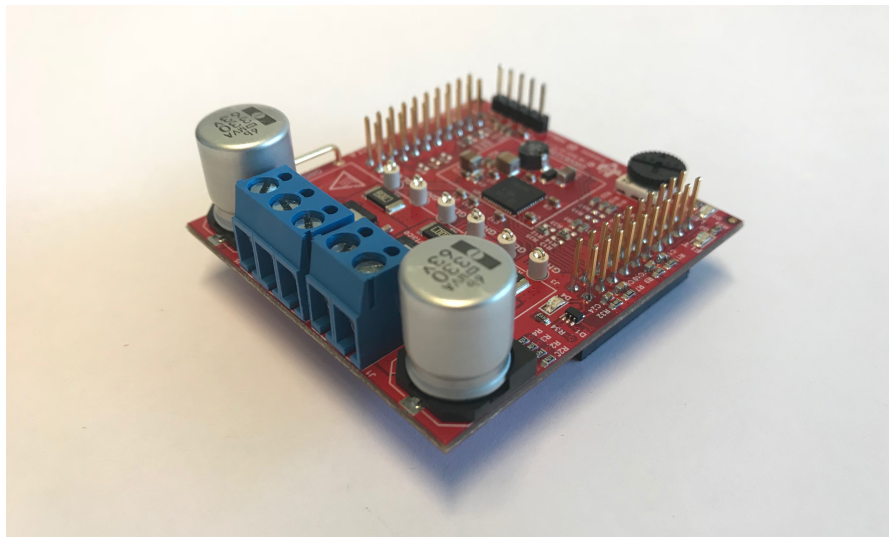


Figure 4.2: The BOOSTXL-DRV8323RH inverter

In order to have a small simulation set-up, some small motors are also needed. The 2MTR-DYNO evaluation module from Texas Instruments provides two low-power BLDC motors with a shaft coupler. This is exactly what is needed for the set-up. One motor will be tested as the actual motor while the other one acts as an active load. A schematic overview of the simulation set-up is given in fig. 4.3. A 30V 10A power supply was used, because that was available in the lab space. The communication between the PC's and the LaunchPads can be done either over USB or over CAN.

### 4.2.2. Development

After all the parts were ordered and had arrived, development could begin. However, there was a problem with the Launchpad/BoosterPack combination. The BOOSTXL-DRV8323RH turned out to not be directly compatible with the LAUNCHXL-F28069M. At first it seemed like a software problem, so all kinds of different software packages from Texas Instruments were downloaded to try and make it work. This did not work, and eventually an entry on the Texas Instruments E2E forum was found with [18] attached. A lab technician from the TU helped to solder some SMD capacitors to the BoosterPack, which were needed to make it work (see fig. 4.4). According to [18], only a few adjustments had to

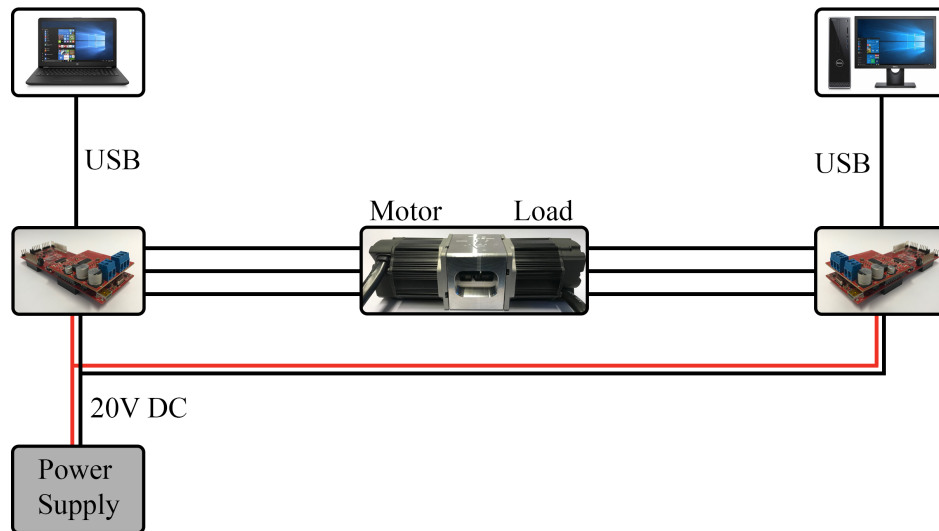
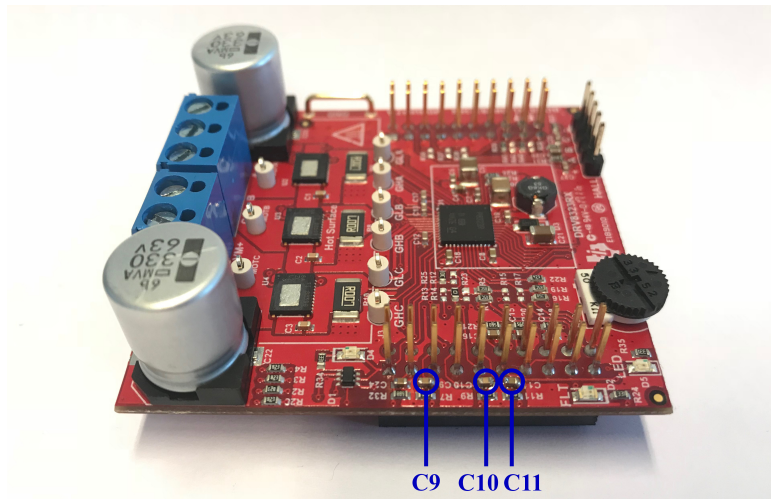


Figure 4.3: Schematic overview of the simulation set-up

Figure 4.4:  $0.1\mu F$  capacitors had to be soldered on C9, C10 and C11.

be made in Code Composer Studio to make the boards compatible. However, the hardware quick start guide found is for the DRV8323RS, which uses a Serial Peripheral Interface (SPI) for communication between the LaunchPad and the BoosterPack. The BoosterPacks ordered are DRV8323RH, which uses a hardware interface. Help was sought on the Texas Instruments E2E forum, but the answers gotten were too vague. To make the boards compatible several adjustments in the code had to be made regarding pins and register usage. Since neither of the students had prior experience with Code Composer Studio or any of the projects, this would be a near impossible task within the time scheduled for this project. So it was decided to order different BoosterPacks, that would work right out of the box with the LAUNCHXL-F28069M. This way CAN-capabilities can still be used. If the Nuon Solar Team desires to use the DRV8323RH in the future, extra programming will be needed, but it can be used.

The BoosterPack that was chosen was the BOOSTXL-DRV8301. This works up to 24V and with a continuous current of 10A. This is a significant drop in power compared to the DRV8323RH, but it can still be used for the simulation and driving the Nuna motor at low power. Since this BoosterPack is only used for the development and demos, it does not really matter how much power it delivers. In a later stage of development the Nuon Solar Team will still have to switch to a different inverter, which then will be controlled by the MCU that is used on the LAUNCHXL-F28069M. With the new BoosterPack, the

development of the controller could finally begin.

To get familiar with Code Composer Studio and MotorWare™ the different tutorial labs available were followed. After this was done, it was clear all the tools to develop a controller for Nuna are there, and with some careful rearranging of code a proper controller could be developed from the labs. The installation of the software and setting up the simulation environment can be found in appendix A.

The most complete overview of the control for Nuna is given in Texas Instruments `proj_lab11a`. This is the lab that will be used for the motor controller the simulation set-up. The features of this lab are explained in section 5.2. For the torque controller in the simulation set-up, lab 4 will be used. How to use this lab will be briefly discussed in appendix A, and an in-depth explanation of this lab is given in [14].

#### 4.2.3. Further development

As pointed out in section 4.1 and section 4.2.1, the LAUNCHXL-F28069M and the BOOSTXL-DRV8301 will only be used for the simulation, low-power demos & early prototyping on the Nuna motor. In a further stage of controller development, it is recommended to leave the current prototyping environment. If it is decided to design a custom inverter for Nuna, the LAUNCHXL is not the best solution, because it has a lot of connections that are unnecessary. The LAUNCHXL-F28069M is a platform build around the TMS320F28069M MCU for experimentation. When developing a custom solution for motor control this MCU can be integrated with the inverter. This will of course require a custom PCB, which is a lot of work. However, the best possible integration of the control can be guaranteed. A custom inverter will need extra measurement circuits to interface with the MCU so custom PCBs are already needed. Customizing the design will also allow for the controller/inverter combination to have the smallest footprint possible and have all the connections in a convenient place.

### 4.3. Pinout LAUNCHXL-F28069M

For the LAUNCHXL-F28069M to be connected to a different inverter than the BOOSTXL-DRV8301, it is needed to know where the different inputs and outputs are and what kind of signal type they use. To connect the controller to an inverter, the pins should be connected to the inverter as in fig. 4.5. Where these pins are located on the LAUNCHXL-F28069M is shown in fig. 4.6.

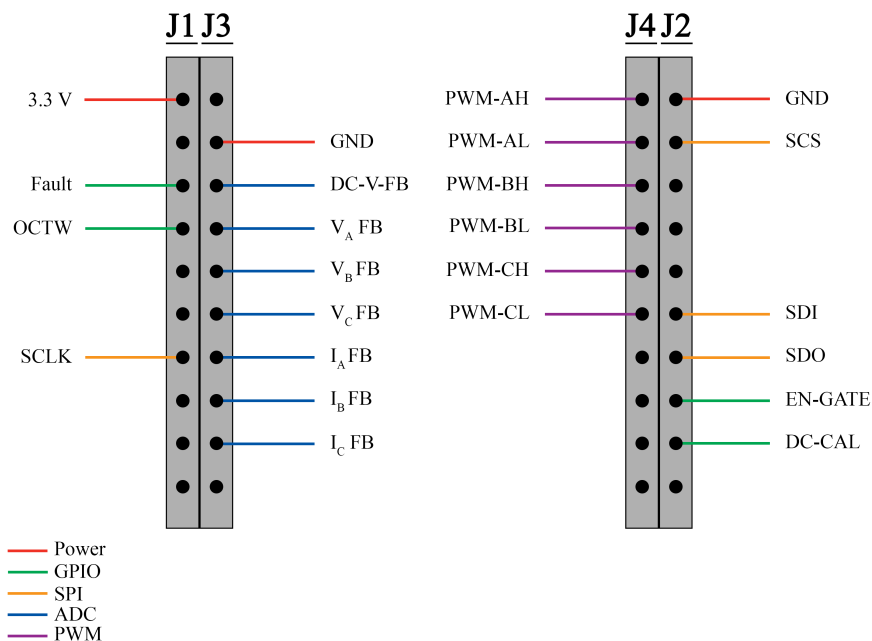


Figure 4.5: The pinout of the controller. Different signal types are represented by different colours.



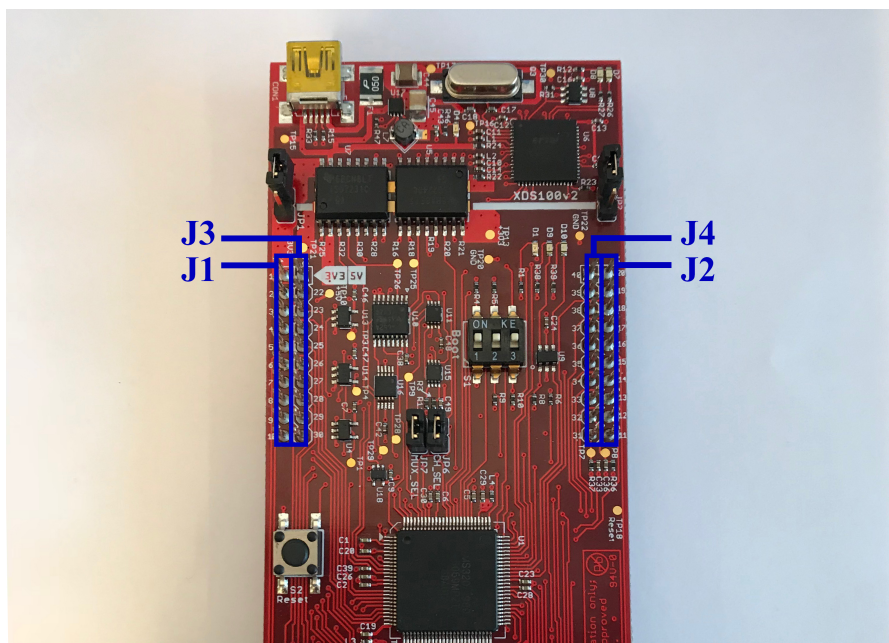


Figure 4.6: The location of the GPIO pins on the LAUNCHXL-F28069M.

### Power signals

To power the controller, 3.3V is needed. The CAN-bus from Nuna works on 12V so a small buck-converter is recommended for getting the power from the CAN-bus. The BOOSTXL-DRV8301 also powers this pin through a buck-converter, but when using a larger inverter it is better to take the signal from the CAN-bus, as this has a lower voltage and a small converter can be used.

### GPIO signals

These signals are specified for the feedback of the BOOSTXL-DRV8301. They will probably need to be redefined for use with a different inverter, as it presumably has a different communication standard. The signals are, however, quite useful for the functionality of the control and inverter, so they will be discussed here. This will give an idea of useful signals when setting up a different inverter with the LAUNCHXL-F28069M.

### Fault (IN)

On the fault pin, the controller can see if a shutdown event has occurred in the inverter [19]. This can happen due to events such as overcurrent, overtemperature, overvoltage or undervoltage.

### OCTW (IN)

This pin lets the controller know when there has been an overcurrent or overtemperature event. Depending on the threshold and behaviour settings this may or may not lead to a shutdown event [19].

### EN\_GATE (OUT)

This pin is used to set the state of the gate driver, charge pump, current shunt amplifier, and internal regulator blocks of the BOOSTXL-DRV8301 [19]. This means energy can be saved with a low signal. It can also be used as a reset. With a short reset ( $< 10\mu\text{s}$ ) only the gate driver will be reset, and with a long reset ( $> 20\mu\text{s}$ ) all the blocks will be reset to a known state.

### DC\_CAL (OUT)

The DC\_CAL pin is used for calibration to keep the DC offset and drift overtemperature low [19]. This signal will disconnect the load and short the input of the shunt resistor.

## SPI signals

The Serial Peripheral Interface specification is used to set-up the BOOSTXL-DRV8301 [19]. In the SPI registers on the BOOSTXL-DRV8301 the thresholds and protection settings are stored. When using a different inverter, the signals are only relevant if the inverter also uses SPI for these settings.

## ADC signals (IN)

### Voltage measurement

Voltage feedback is needed for the FAST estimator to function properly. It takes a direct measurement from the motor phases, so some hardware settings for the voltage feedback need to be set [16]. The DRV-8301 also measures the voltage on the DC bus. The ADC input can only handle a maximum input of 3.3 V, so some kind of circuit is needed to keep the input in that range. Figure 4.7 shows a voltage

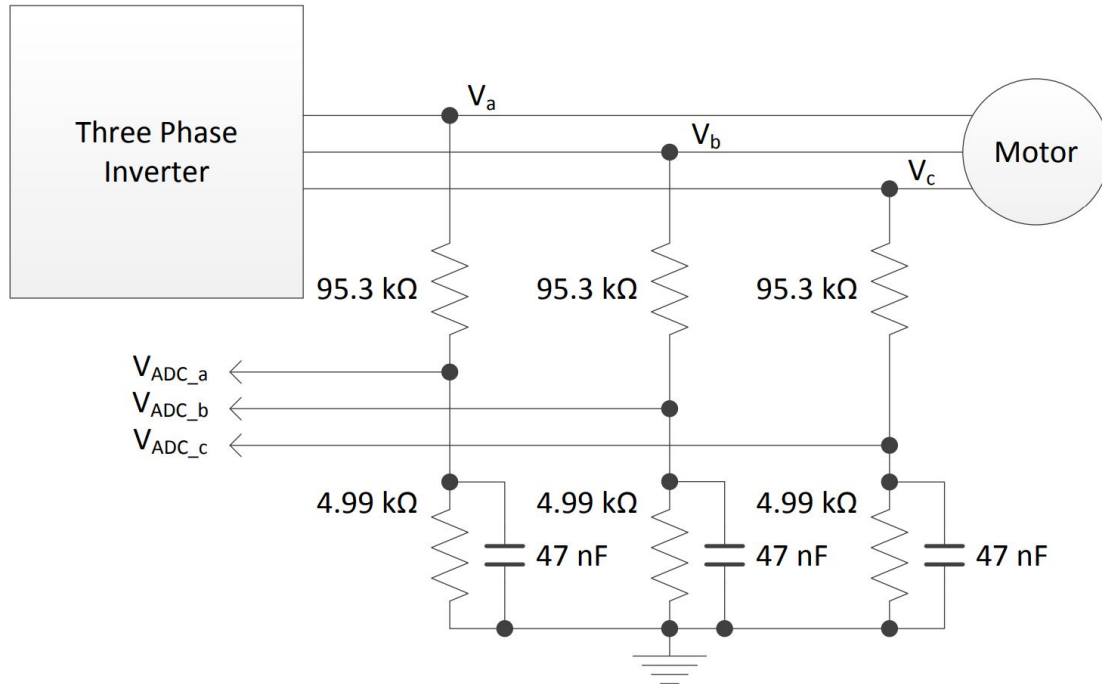


Figure 4.7: A voltage feedback circuit ([16] Fig. 5-7)

feedback circuit example. In this example the maximum phase voltage that can be sensed can be calculated as follows:

$$V_a^{max} = V_{ADC\_a}^{max} \times \frac{4.99k\Omega + 95.3k\Omega}{4.99k\Omega} = 66.3V \quad (4.1)$$

This value can be adjusted in the `user_j1.h` file:

```
//! \brief Defines the maximum voltage at the input to the AD converter
#define USER_ADC_FULL_SCALE_VOLTAGE_V (66.3)
```

For the BOOSTXL-DRV8301 this value is  $V_{ADC\_a}^{max} = 26.314V$ . The value of  $V_a^{max}$  should leave some headroom, so it should be about 20-30% higher than the rated voltage of the machine. The divider example from fig. 4.7 is ideal for a 48 V machine [16].

The switching nature of the inverter makes it hard to accurately measure the phase voltage. This is why the feedback signal needs to be filtered, which can be done using a capacitor. The filter needs to smooth out the signals, while still being able to let a high-speed voltage signal pass through. For a switching frequency of around 20 kHz a cutoff frequency of a few hundred Hz should be sufficient. In the case of the BOOSTXL-DRV8301, the voltage sensing circuit is as shown in fig. 4.8. To accurately detect the feedback voltage, the FAST estimator needs to know the pole of this filter. The frequency of

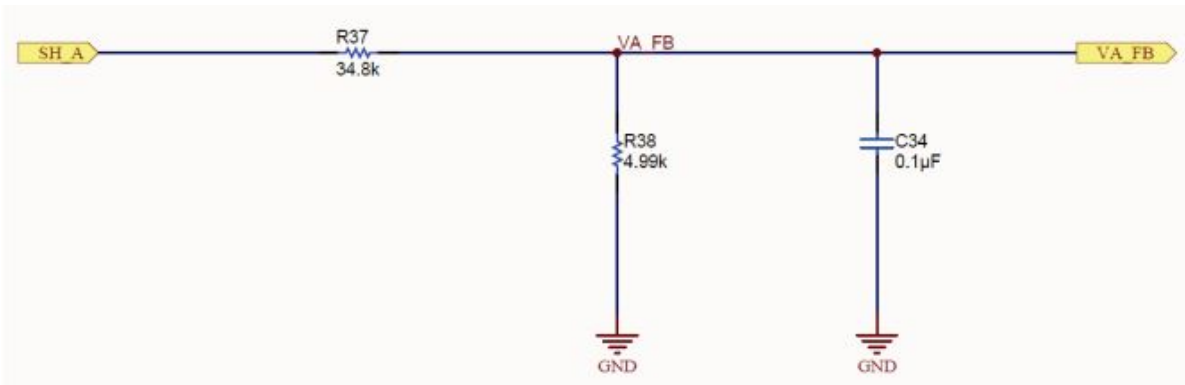


Figure 4.8: The voltage feedback circuit of the BOOSTXL-DRV8301 ([20] Fig. 6)

the pole can be calculated as follows (with the values of the BOOSTXL-DRV8301)[16]:

$$F_{filter\_pole} = \frac{1}{2\pi \times R_{parallel} \times C} = \frac{1}{2\pi \times \frac{34.8k\Omega \times 4.99k\Omega}{34.8k\Omega + 4.99k\Omega} \times 0.1\mu F} = 364.682Hz \quad (4.2)$$

The value of the filter pole’s frequency for the FAST estimator can be changed in the `user_j1.h` file:

```

//! \brief POLES
// *****
//! \brief Defines the analog voltage filter pole location, Hz
//! \brief Must match the hardware filter for Vph
#define USER_VOLTAGE_FILTER_POLE_Hz (364.682)
    
```

### Current measurement

The ADC’s input range from 0 V to 3.3 V needs to be able to measure both positive and negative currents. To be able to tell the sign of the signal, a reference voltage of 1.65 V needs to be made. This can quite easily be done by making a buffered voltage divider, as shown in fig. 4.9 [16]. Using the 1.65 V as a reference voltage, the current can be sensed using a differential amplifier like in fig. 4.10.

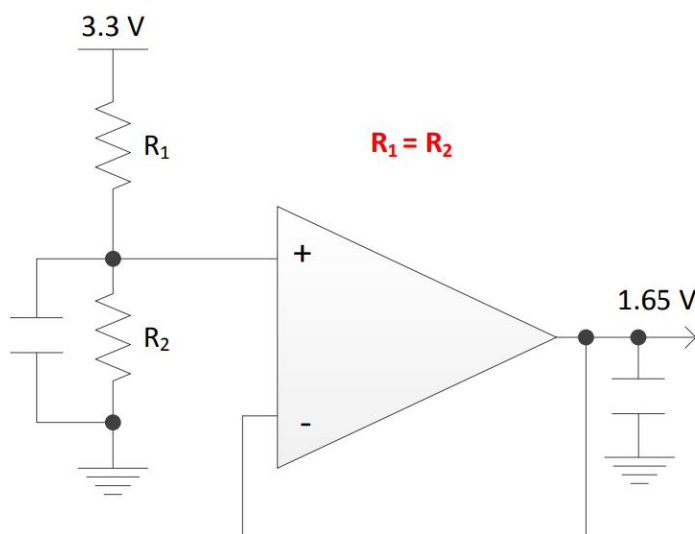


Figure 4.9: A voltage divider with a voltage follower to generate a 1.65 V reference signal ([16] Fig 5-2)

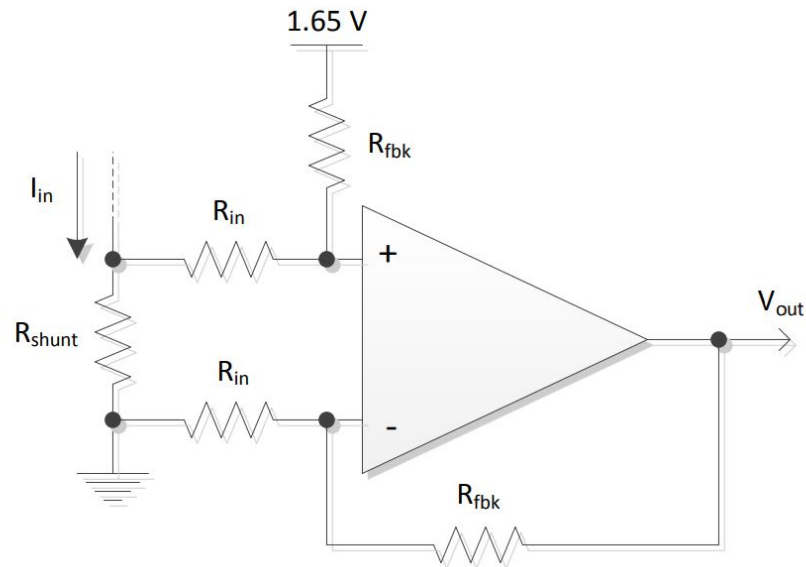


Figure 4.10: A differential amplifier circuit, which can be used for the current sensing ([16] Fig 5-3)

The transfer function of the circuit in fig. 4.10 is [16]:

$$V_{out} = 1.65 + I_{in} \times R_{shunt} \times \frac{R_{fbk}}{R_{in}} \quad (4.3)$$

With the values of the resistances, the maximum measurable current can be set. The maximum output voltage should be 3.3 V, and with the shunt resistor known, the other resistor values can be calculated. The maximum peak-to-peak current to be measured should be specified in the software. So if the phase current of the motor is  $\pm 10$  A a value of 20 A should be specified. This can be adjusted in `user_j1.h`:

```
//! \brief Defines the maximum current at the AD converter
#define USER_ADC_FULL_SCALE_CURRENT_A      (33.0)
```

How well the current measurement represents the actual current depends heavily on the slew rate of the operational amplifier [16].

The op-amp of the differential amplifier can be configured to have either positive or negative current feedback. It is important to know which configuration is used, so that the MCU can have an accurate current measurement. In fig. 4.11 the two options are shown.

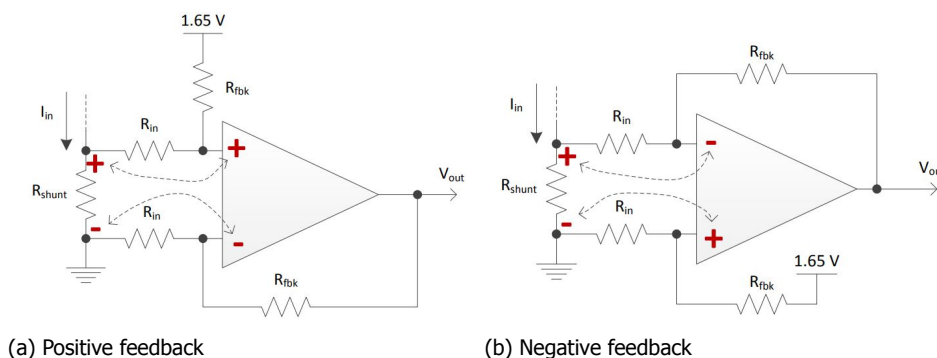


Figure 4.11: The two possible op-amp configurations for the differential amplifier ([16] Fig. 5-5 & 5-6)

The polarity of the feedback loop should be taken into account in the value of the current offset values. For a positive feedback the values of the offset should be negative, and for a negative feedback the values of the offset should be positive. The values can be set in `user_j1.h`:

```
#define I_A_offset (-0.8331743479) #define I_A_offset (0.8331743479)
#define I_B_offset (-0.8355930448) #define I_B_offset (0.8355930448)
#define I_C_offset (-0.8392037153) #define I_C_offset (0.8392037153)
```

(a) The current offset values for positive feedback

(b) The current offset values for negative feedback

Not all the phases of an inverter necessarily have a shunt resistor to measure the current. The number of shunt resistors (2 or 3) can be specified in `user_j1.h`, so the Clarke transform can properly convert the three phase system to a two phase system. If three shunt resistors are available, they should all be used as that would give the most accurate result.

```
//! \brief Defines the number of current sensors used
//! \brief Defined by the hardware capability present
//! \brief May be (2) or (3)
#define USER_NUM_CURRENT_SENSORS (3)
```

In fig. 4.12 a schematic overview of the measurement circuits together is given. This shows how to connect the voltage and current measurement circuits to the ADC pins on the LAUNCHXL-F28069M.

### PWM signals (OUT)

The PWM signals coming out of the LAUNCHXL-F28069M use 0 V as low and 3.3 V as high. The frequency of the PWM signals can be changed to provide a suitable frequency for the motor provided. To keep the ripple low, motors with a lower inductance usually need a higher PWM frequency [16]. To make sure the control does not make audible noise, it is recommended the frequency is at least 20 kHz. The PWM frequency can be changed in `user_j1.h`:

```
//! \brief Defines the Pulse Width Modulation (PWM) frequency, kHz
#define USER_PWM_FREQ_kHz (20.0)
```

How the PWM signals are configured precisely is beyond the scope of this project, but it is explained in [21].

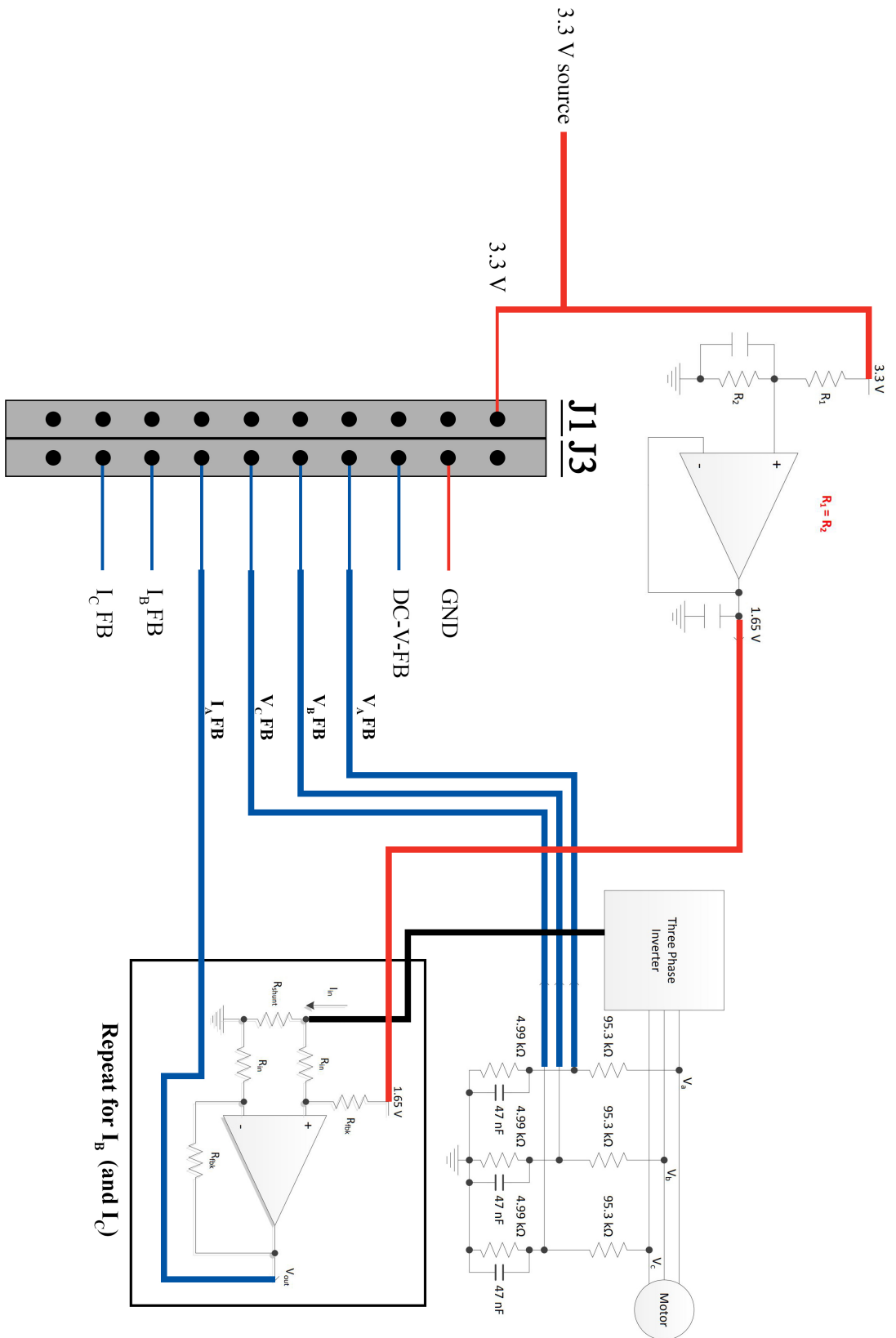


Figure 4.12: An overview of connecting the ADC pins

# 5

## Controller Software

To understand how the FOC is implemented and how different motor specifications can be set in the controller it is essential to look at some sections of the C code used by the Texas Instruments labs. This chapter will focus on the code of lab 11a, where the motorcontroller itself is specified. For motor identification lab 2 can be used, and the torque load in the simulation will use lab 4. How these labs can be used is briefly discussed in appendix A. A more in depth explanation of the functions is given in [14]. In this project Code Composer Studio version 7.3.0, MotorWare™ version 1.01.00.18 and C2000Ware version 1.00.02.00 are used.

### 5.1. Adjustments for motor types

To use any kind of motor with the software provided, it must first be specified in the code what kind of motor it is. This can be done in the `user.h`, `user_j1.h`, and `user_j5.h` files. The `user_j1.h` and `user_j5.h` files are the same, with only one difference. The `user_j1.h` file is read when connecting the BoosterPack to the top slot of the LAUNCHXL-F28069M (closest to the USB port), and the `user_j5.h` file is for use of the bottom slot. Only `user_j1.h` will be used, as this project only uses the top slot. Which slot is used can be changed in the `user.h`:

```
// select whether to use the inverter on connector J1 or J5 of the LaunchPad
#define J1
```

The following section will show where to adjust the parameters for the motor in the code. Without these parameters, the control of the motor will not work properly. This is also where the values of the motor determined in [1] will eventually be entered. First, a motor must be defined. This is done in the `user_j1.h` file:

```
//! \brief USER MOTOR & ID SETTINGS
// *****

//! \brief Define each motor with a unique name and ID number
// BLDC & SMPM motors
#define Estun_EMJ_04APB22          101
#define Anaheim_BLY172S          102
#define Tamagawa_A0100            103
#define Teknic_M2310PLN04K        104
#define Drone_A2212_1000KV        105
#define Drone_A2313_960KV         106

// IPM motors
// If user provides separate Ls-d, Ls-q
// else treat as SPM with user or identified average Ls
#define Belt_Drive_Washer_IPM      201
```

```
#define Anaheim_Salient          202

// ACIM motors
#define Marathon_5K33GN2A      301
```

There are already several motor types ready to use, but when using a new motor it will need to be specified. In the case of a BLDC or PMSM it can be defined here with the unique identifier 107. The simulation set-up uses the Teknic M2310PLN04K motors, which are already defined here, so that does not need to be added. Of all the motors defined, one must be selected. This can be done directly below the defining of the motors in `user_j1.h`:

```
//! \brief Uncomment the motor which should be included at compile
//! \brief These motor ID settings and motor parameters are then available
        to be used by the control system
//! \brief Once your ideal settings and parameters are identified update
        the motor section here so it is available in the binary code
//#define USER_MOTOR Estun_EMJ_04APB22
//#define USER_MOTOR Anaheim_BLY172S
//#define USER_MOTOR Tamagawa_A0100
//#define USER_MOTOR Drone_A2313_960KV
#define USER_MOTOR Teknic_M2310PLN04K
//#define USER_MOTOR Belt_Drive_Washer_IPM
//#define USER_MOTOR Marathon_5K33GN2A
//#define USER_MOTOR Anaheim_Salient
```

This will leave all the other motors with a grey layout in the code below. Only the selected motor will have a white background because it is used. The motor parameters show in the code as follows:

```
#elif (USER_MOTOR == Teknic_M2310PLN04K)
#define USER_MOTOR_TYPE          MOTOR_Type_Pm
#define USER_MOTOR_NUM_POLE_PAIRS (4)
#define USER_MOTOR_Rr            (NULL)
#define USER_MOTOR_Rs            (0.3918252)
#define USER_MOTOR_Ls_d          (0.00023495)
#define USER_MOTOR_Ls_q          (0.00023495)
#define USER_MOTOR_RATED_FLUX    (0.03955824)
#define USER_MOTOR_MAGNETIZING_CURRENT (NULL)
#define USER_MOTOR_RES_EST_CURRENT (1.0)
#define USER_MOTOR_IND_EST_CURRENT (-0.5)
#define USER_MOTOR_MAX_CURRENT   (7.0)
#define USER_MOTOR_FLUX_EST_FREQ_Hz (20.0)
```

If a new motor is introduced, with unidentified parameters, these values might need to be determined first. A new motor can be entered in the following way (assuming it is BLDC or PMSM) [14]:

- **USER\_MOTOR\_TYPE**  
Here the motor type is defined. In this case it should be `MOTOR_Type_Pm`.
- **USER\_MOTOR\_NUM\_POLE\_PAIRS**  
Here the number of pole pairs of the motor needs to be defined. In the case of the Teknic M2310PLN04K this number is 4. When adding the Mitsuba motor used by Nuna this number should be 16.
- **USER\_MOTOR\_Rr**  
The rotor resistance of the motor. Since this is irrelevant for BLDC machines and PMSMs this value should always be `NULL`.
- **USER\_MOTOR\_Rs**  
The stator resistance of the motor. A calculated value can be inserted here. If you want this value to be estimated by the software, `NULL` should be inserted here. Then after running an initialisation the estimated value can be copied here.



- **USER\_MOTOR\_Ls\_d**  
The inductance of the motor can, like Rs, be entered or measured. In case an estimation needs to be done, enter NULL here.
- **USER\_MOTOR\_Ls\_q**  
Since the motor specified is a BLDC (in the simulation set-up) or a surface PMSM (the Nuna motors), this value should approximately be the same as Ls\_d. That means either NULL or the same calculated or estimated value.
- **USER\_MOTOR\_RATED\_FLUX**  
The total flux linkage between the rotor and the stator. For now this value should be set to NULL, and after the initial estimation it should be updated.
- **USER\_MOTOR\_MAGNETIZING\_CURRENT**  
This value is only used with induction motors, so it should be set to NULL.
- **USER\_MOTOR\_RES\_EST\_CURRENT**  
When in identification mode, the motor has to be started in open loop. This value is used to set the current peak during the initial startup. This value is used in the estimation of Rs. After the identification of the motor is complete this value is not used anymore. It is recommended to set this value at 10-20% of the rated current of the motor.
- **USER\_MOTOR\_IND\_EST\_CURRENT**  
This current can be set to the negative of USER\_MOTOR\_RES\_EST\_CURRENT. This is the value of the maximum current that will be used to estimate Ls.
- **USER\_MOTOR\_MAX\_CURRENT**  
Should be set to the maximum nameplate current of the motor.
- **USER\_MOTOR\_FLUX\_EST\_FREQ\_Hz**  
When identifying the motor, this will be used as the maximum commanded speed of the flux. For a PMSM motor, 20.0 Hz is a good starting point.

## 5.2. Functions in lab 11a

Lab 11a of the Texas Instruments manual shows most of the features that are needed for Nuna motor control. The most important functions are [14]:

- Keeping the controller as much out of ROM as possible. This will allow for modifications to the control to be implemented easily.
- Not using any motor identification. This should have already been done, with previous measurements or the values found in [1].
- Offset recalculation during standstill. This will allow for the control to be (re)calibrated when needed.
- Rs recalculation. This is also useful for (re)calibration.
- Rs Online. This will allow for the stator resistance to be recalculated while running the motor. This is very important, as this value will be used to calculate the temperature in the motor. This can be used to stop the motor from overheating.
- Speed and Id ramps. By not using steps to change the speed and Id reference overcurrents and overvoltages can be avoided.
- Space vector over-modulation. The lab will also allow for over-modulation to be used if desired. This thesis will not discuss over-modulation in detail.
- Field weakening is also available. This will allow the motor to spin beyond its rated speed by reducing the field in the motor.

- 1/Vbus compensation. This feature will adjust the output voltage to how much Vbus has dropped. This means the output voltage is always correctly compensated to match Vbus.
- CPU usage calculation. Here the percentage of the CPU used can be seen. This will allow for developers to check how extra functions impact the calculations, or show them they need to free up some space.
- The PID controllers can be independently tuned.

These features make for a great place to start developing Nuna's own controller, as a lot of control parameters can be adjusted beforehand and while running. How to use this lab is explained in appendix A. How these extra functions are implemented in the C code can be found in [14] under the lab 11a explanation.

### 5.2.1. FOC on the MCU

A block diagram of how FOC is implemented on the microprocessor is given in fig. 5.1 [16]. There is one big difference between the figure and lab 11a: the figure shows all of the control blocks inside a "CTRL" object that is called from the main loop, which is not used in lab 11a. Instead all the blocks seen here are directly implemented in the main interrupt service routine (ISR). This can be done because no motor identification is needed. The identification process is specified in the CTRL object, so if that is needed a previous lab should be used. Lab 11a provides a more open structure, because all parts of the control can be seen from the main ISR. This makes it easier to comprehend the control and modify specific parts.

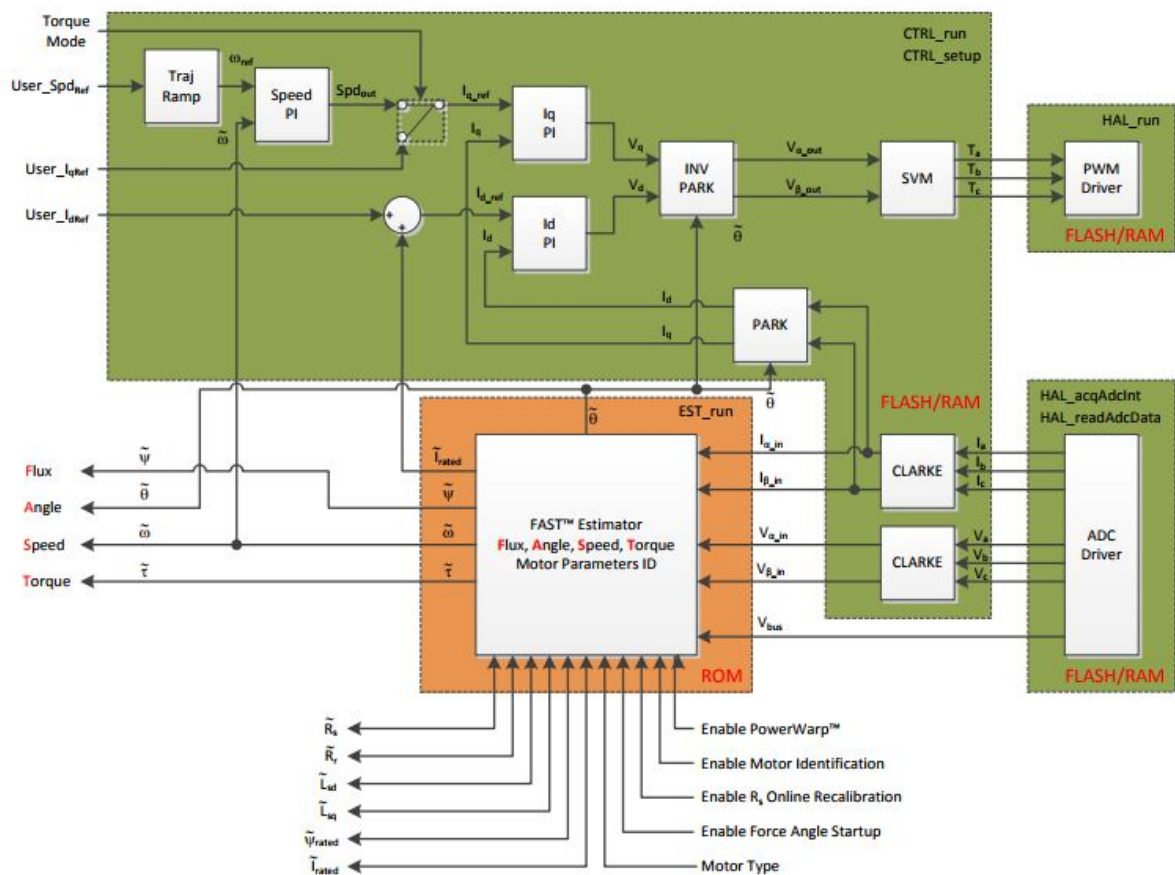


Figure 5.1: An overview of the way FOC is implemented with the TMS320F28069M MCU ([16] Fig. 1-3)

### 5.2.2. Field weakening in lab 11a

In lab 11a automatic field weakening is included. In fig. 5.2 the block diagram of this field weakening is shown. First, the output of the Id and Iq controller are used to calculate the output vector  $V_s$ . The output vector is then compared to  $V_{sRef}$ , the maximum allowed output vector calculated from the limits set by the user. If  $V_s$  becomes larger than  $V_{sRef}$ , field weakening will be applied [14]. As the motor's speed increases,  $V_s$  will become larger than  $V_{sRef}$ , and at that point  $I_{dRef}$  will start to grow negative. This will produce field weakening and keep  $V_s$  controlled to  $V_{sRef}$  [14]. The changing of  $I_{dRef}$  is done in the Field Weakening Controller. This controller uses a  $V_{sRef}$  signal to determine the adjustment of  $I_{dRef}$ , as shown in fig. 5.3. This field weakening method is an example, and other field weakening algorithms can be implemented in the motor controller [14].

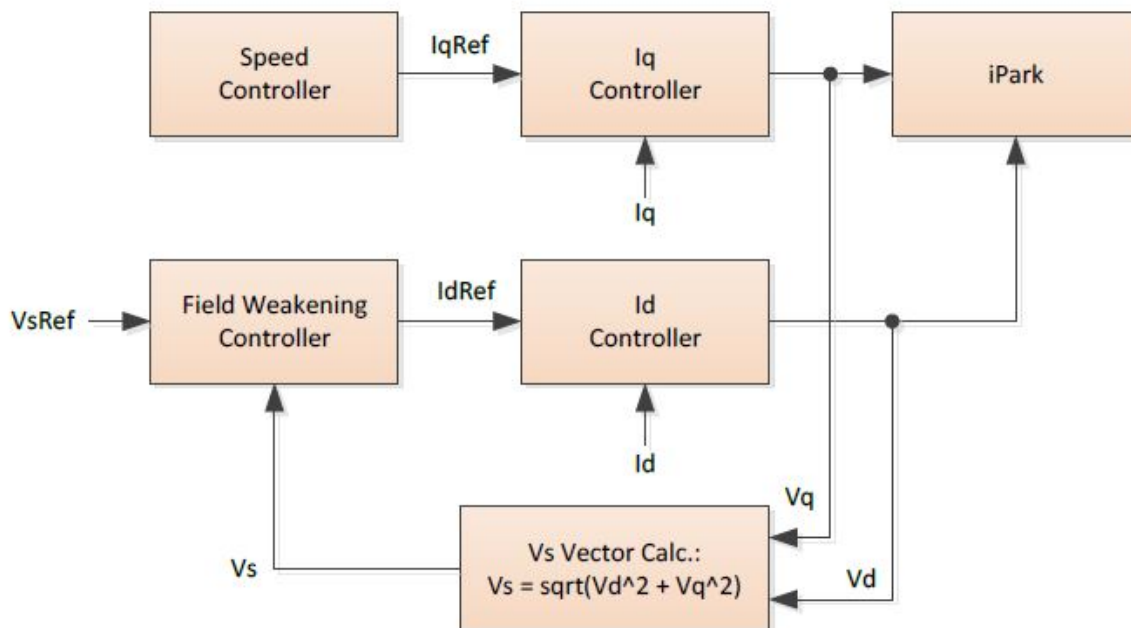


Figure 5.2: The block diagram of the field weakening implemented in lab 11a ([14])

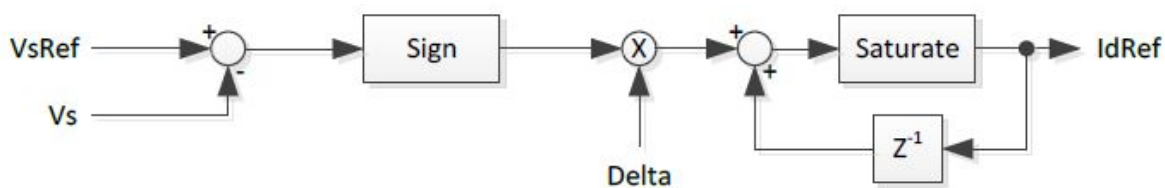


Figure 5.3: The field weakening controller ([14])

### 5.3. Lab 11a - Main ISR

The Code Composer Studio project for Lab 11a is very large. Here some of the basic functions of the project will be explained. Starting with the main interrupt service routine, this will give a proper overview of how the control works while running. This explanation can also be found in [14].

#### Forward FOC

Here data values are received from the ADC, the offset is applied to the currents and voltages, and the Clarke transforms on the currents and voltages are done.

```
// acknowledge the ADC interrupt
```

```

HAL_acqAdcInt(halHandle, ADC_IntNumber_1);
// convert the ADC data
HAL_readAdcDataWithOffsets(halHandle, &gAdcData);
// remove offsets
gAdcData.I.value[0] = gAdcData.I.value[0] - gOffsets_I_pu.value[0];
gAdcData.I.value[1] = gAdcData.I.value[1] - gOffsets_I_pu.value[1];
gAdcData.I.value[2] = gAdcData.I.value[2] - gOffsets_I_pu.value[2];
gAdcData.V.value[0] = gAdcData.V.value[0] - gOffsets_V_pu.value[0];
gAdcData.V.value[1] = gAdcData.V.value[1] - gOffsets_V_pu.value[1];
gAdcData.V.value[2] = gAdcData.V.value[2] - gOffsets_V_pu.value[2];
// run Clarke transform on current
CLARKE_run(clarkeHandle_I, &gAdcData.I, &Iab_pu);
239
// run Clarke transform on voltage
CLARKE_run(clarkeHandle_V, &gAdcData.V, &Vab_pu);

```

### Estimator Run

This is the main function to ROM, to run the FAST™ estimator.

```

// run the estimator
EST_run(estHandle,
&Iab_pu,
&Vab_pu,
gAdcData.dcBus,
gMotorVars.SpeedRef_pu);

```

### Extracting Estimated Variables

To actually control values with FOC, a few variables need to be extracted from the estimator. These are the following values:

- **Flux** - The value of Id.
- **Angle** - The angle of the rotor.
- **Speed** - The speed at which the rotor is turning.
- **Torque** - The value of Iq.

```

// generate the motor electrical angle
angle_pu = EST_getAngle_pu(estHandle);
speed_pu = EST_getFm_pu(estHandle);
// get Idq from estimator to avoid sin and cos
EST_getIdq_pu(estHandle, &gIdq_pu);

```

Reading the Id and Iq values from the estimator is not necessary, but it saves execution cycles compared to getting phasor values from them and performing a Park transformation.

### Speed Control

This is the first control block, which takes a reference from a global variable and an actual value from the estimator. The frequency at which the controller is activated can be set in `user_j1.h`.

```

// when appropriate, run the PID speed controller
if(pidCntSpeed++ >= USER_NUM_CTRL_TICKS_PER_SPEED_TICK)
{
// clear counter
240
pidCntSpeed = 0;
// run speed controller

```

```
PID_run_spd(pidHandle[0],
gMotorVars.SpeedRef_pu,
speed_pu,
&(gIdq_ref_pu.value[1]));
}
```

### Id control

The controller of Id is executed next.

```
// get the reference value
refValue = gIdq_ref_pu.value[0];
// get the feedback value
fbackValue = gIdq_pu.value[0];
// run the Id PID controller
PID_run(pidHandle[1], refValue, fbackValue, &(gVdq_out_pu.value[0]));
```

### Iq control

The controller for Iq is the last control block executed.

```
// get the Iq reference value
refValue = gIdq_ref_pu.value[1];
// get the feedback value
fbackValue = gIdq_pu.value[1];
// calculate Iq controller limits, and run Iq controller
outMax_pu = _IQsqrt(_IQ(USER_MAX_VS_MAG_PU * USER_MAX_VS_MAG_PU)
- _IQmpy(gVdq_out_pu.value[0], gVdq_out_pu.value[0]));
PID_setMinMax(pidHandle[2], -outMax_pu, outMax_pu);
PID_run(pidHandle[2], refValue, fbackValue, &(gVdq_out_pu.value[1]));
```

Using the value for available voltage from an output vector, as well as a limit set in `user_j1.h`, the output limit of the control is calculated before actually running the controller.

### Inverse FOC

The outputs of the Id and Iq controllers go through an inverse Park transform and space vector modulation. For the inverse transform the most recent angle estimation is used in combination with a compensation factor. This compensation is based on the estimated speed and the frequency of the PWM module. This is needed because of the delay of the previous executions.

```
// compensate angle for PWM delay
angle_pu = angleDelayComp(speed_pu, angle_pu);
// compute the sin/cos phasor
phasor.value[0] = _IQcosPU(angle_pu);
241
phasor.value[1] = _IQsinPU(angle_pu);
// set the phasor in the inverse Park transform
IPARK_setPhasor(iparkHandle, &phasor);
// run the inverse Park module
IPARK_run(iparkHandle, &gVdq_out_pu, &Vab_pu);
```

The voltages out of the inverse Park transform need to be compensated for any drop in Vbus. The  $1/V_{bus}$  calculation is read from the estimator, and the space vector modulation is executed with the compensated values.

```
// run the space Vector Generator (SVGEN) module
oneOverDcBus = EST_getOneOverDcBus_pu(estHandle);
Vab_pu.value[0] = _IQmpy(Vab_pu.value[0], oneOverDcBus);
Vab_pu.value[1] = _IQmpy(Vab_pu.value[1], oneOverDcBus);
SVGEN_run(svggenHandle, &Vab_pu, &(gPwmData.Tabc));
```

### Writing PWM values

The final step of the interrupt service routine is writing the newly calculated PWM values to the PWM module through the hardware abstraction layer (HAL).

```
// write the PWM compare values  
HAL_writePwmData(halHandle, &gPwmData);
```

At the end of this routine a full cycle of control like in fig. 5.1 has been executed.

# 6

## CAN-interface

### 6.1. CAN Protocol

The Controller Area Network (CAN, or CAN Bus) is a method designed to let devices communicate with each other without using multiple wires. CAN is an International Organization for Standardization (ISO) defined serial communications bus [22]. It is designed to let control units and devices communicate with each other over two lines: a CAN-H (CAN High) and a CAN-L (CAN Low) wire. These are connected to all the parts of the network and finally ended with a CAN Data Bus terminal, like figure 6.1. This is often a 120 ohm resistor, preventing that data is reflected at the ends of the CAN line [23].

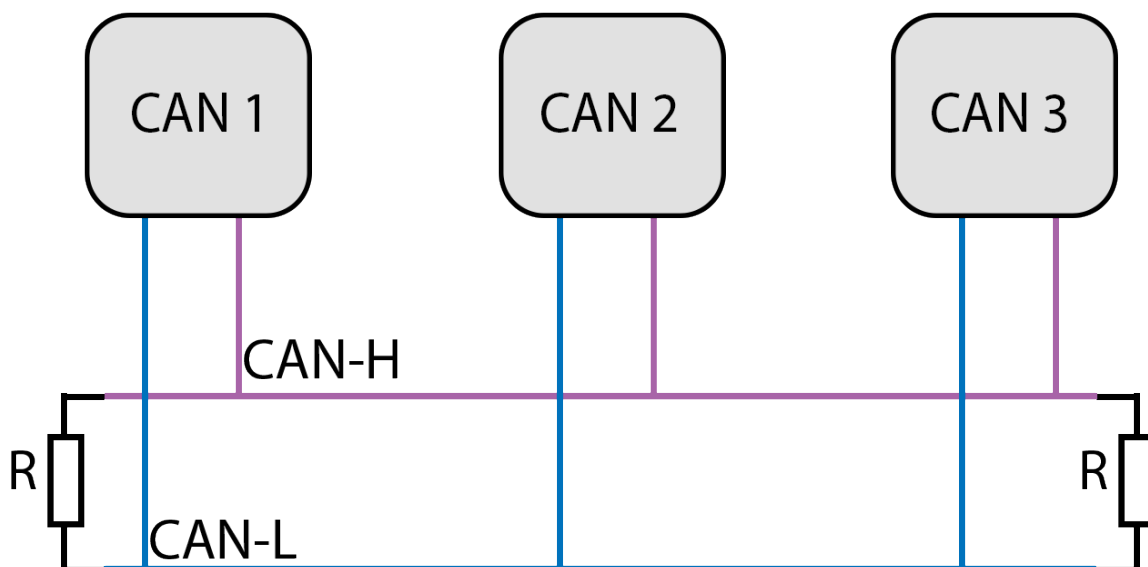


Figure 6.1: A simplified implementation of a CAN interface

CAN bus communication protocol is a carrier-sense, multiple-access protocol with collision detection and arbitration on message priority. [22] The sequence that is brought onto the lines is equal, however their amplitudes are opposite. Meaning a pulse on the CAN-H line goes from for example 7.5V to 4V, the pulse on the CAN-L goes from 0.5V to 4V and vice versa. This provides a better noise resistance and therefore less corrupted data. When the two CAN-bus lines (CAN-H and CAN-L) are 7.5 volt and respectively 0.5 volt, the voltage difference is at the maximum and the status of the bit is in dominant state with the value of 0. When both lines hit the 4 volt, the bit goes in recessive state and the value is 1 [23].

The transfer process, using figure 6.1, works as following:

1. CAN 1 provides the data to the CAN 1 controller.
2. The CAN 1 controller sends the data over the lines using electrical signals, if the line is free.
3. CAN 2 and 3 controllers receive the data.
4. Both the nodes check if they need the data and decide to accept or reject the data.

There are two kinds of CAN protocols. The protocol for low speed CAN, ISO 11898-3, with speeds up to 125 kb/s (maximum distance of 500 meters). And ISO 11898-2, high speed CAN up to 1 Mb/s (maximum distance of 40 meters). These can be further divided into the length of the identifier (ID) [23]:

- Standard length of 11 bits.
- Extended length of 29 bits. Using a standard 11 bit identifier with an 18 bit extension.

The car of the Nuon Solar Team uses the ISO 11898-2 protocol, with preferably the Standard CAN identifier length.

If two or more devices try to send a message on the bus. The message, which has the highest priority or most dominant bits, will be sent first. The others are placed in the queue. Figure 6.2 shows how a CAN message is structured.



Figure 6.2: A standard CAN message structure: 11-Bit Identifier [22]

In short:

- SOF: Start Of Field (1 bit), indicates a message is sent with a dominant bit.
- Identifier (11 bits), this is the priority of the message. How more dominant bits the identifier is, how more important the message is.
- RTR: Remote transmission request (1 bit). This bit is dominant if some other information is required.
- IDE: Identifier Extension (1 bit). If this bit is a zero the standard identifier is used. If this is a recessive 1 bit, the extended version is used.
- r0 (1 bit), reserved bit (for possible use by future standard amendment).
- DLC (4 bits), displays how much items were sent in the data field.
- Data (up to 64 bits), the actual information that was sent.
- CRC: Cyclic Redundancy Check (16 bits). This field is used to check if there were any faults in the message.
- ACK, Acknowledge Field (2 bits). All the receivers acknowledge in this field, they have received the data.
- EOF: End Of Field (7 bits). The end of the data protocol.



- IFS: Interframe Space (bit). The time required by the controller to move a correctly received frame to its proper position in a message buffer area.

The extended CAN message structure is the same as the Standard CAN message with the addition of:

- SRR: Substitute Remote Request (1 bit). Replaces the position of the RTR bit.
- IDE: Identifier Extension (1 bit), is a recessive 1.
- 18-bit extension identifier
- r1, an additional reserved bit. Following after the 18-bit identifier, the RTR bit and followed by the r0 bit. [22].

## 6.2. Requirements

To implement the microcontroller into the new Nuna, the following requirements for CAN were given:

- Minimum CAN bus supply voltage: 9 volt.
- Maximum CAN bus supply voltage: 15 volt.
- Nominal Can bus supply voltage: 12 volt.
- CAN bus data rate: 500 kbps.
- CAN bus isolation from high power DC bus: 1000 volt.
- CAN protocol ISO 11898-2 is used.
- *Standard Identifier: 11 bits.*

The requirement in italic is not mandatory, but preferable.

## 6.3. The enhanced Controller Area Network (eCAN)

The enhanced CAN module uses a serial communication protocol. It is ideal to use in noisy environments like the automotive and some other industrial fields. The enhanced CAN module has at least the following features [24]:

- Up till 32 mailboxes in extended mode.
- Supports data rates up to 1 Mbps.
- Fully compliant with ISO 11898-2 (version 2.0B).
- Configurable as receive or transmit mailbox, as well as standard or extended identifier.
- Composed of 0 to 8 bytes of data.

The eCAN module exists out of multiple parts. The most important are the mailboxes and the control and status registers. There are 32 mailboxes and here is the message defined that is received or needs to be transmitted. The control and status registers are used to control the mailboxes.

### eCAN mailboxes

The mailboxes exist of 4 parts:

- **MSGID – Message Identifier (32 bits)**  
These bits set the identifier extension bit and acknowledge the identifier. The last 29 bits for the extended version and bit 28 till 18 for the standard identifier.
- **MSGCTRL – Message Control (32 bits)**  
These bits set the remote-transmission-request bit and define the data-length of the code.

- **CANMDL – Message Data Low (4 bytes)**  
The first 4 bytes of the actual data.
- **CANMDH – Message Data High (4 bytes)**  
The last 4 bytes of the actual data.

### eCAN Control and Status Registers

In the Control and Status registers there are 26 registers each of 32 bits. The most important ones are:

- **CANME – Mailbox Enable**  
In this register every bit is used to enable or disable the individual mailboxes.
- **CANMD – Mailbox Direction**  
Every bit is used to set the direction of each individual mailbox. By writing a 1 the mailbox is configured to receive, set it to 0 the mailbox is a transmit mailbox.
- **CANTRS – Transmission Request Set**  
If one of the mailboxes is ready to transmit a message. This register is set and the transmission is started. The bit can't be cleared by itself. The CPU writes to the transmission-request-reset register when a transmission is send or aborted.
- **CANTA – Transmission Acknowledge**  
If the message was sent successfully, the bit of the transmission acknowledge is set. The number of the bit, that is set, is the number of the mailbox that has sent that message. To clear the bit a 1 must be written to the corresponding bit.
- **CANRMP – Received Message Pending**  
If a message is received in the mailbox, the corresponding bit of the received message pending register is set. This bit can only be reset by the CPU. If there is received a new incoming message, the old one is overwritten.
- **CANMC – Master Control**  
This register controls the settings of the CAN module. Some bits are protected from writing directly. The most important settings are:
  - Standard CAN Configuration bit. This bit defines if the eCan module is half or fully used.
  - Change-configuration request. When this bit is set the configuration register CANBTC can be changed.
  - The data byte order. This bit determines if the least significant or most significant byte is received or transmitted first.
  - The Self test mode bit. If the CAN module is in self test mode, it sends its own acknowledge bits so the code can be tested. To put it in normal CAN mode this bit needs to be zero.
- **CANBTC – Bit-Timing Configuration**  
The network-timing parameters are defined in this register. This register needs to be programmed before using the CAN module and to program this register the Change-configuration request bit in the Master Control register needs to be set.
- **CANES – Error and Status**  
The Error and Status register gives the actual status of the CAN module. It also displays the bus error flags and the status error flags.
- **CANTIOC – TX I/O Control**  
The CANTX pin should be configured for CAN use. Therefore in this register the transmit functionality is assigned to the CANTX pin.
- **CANRIOC – RX I/O Control**  
The CANRX pin should be configured for CAN use. Therefore in this register the receive functionality is assigned to the CANRX pin.

- **CANTSC – Time-Stamp Counter**

In this register the counter at any given moment is displayed. It counts on the bit clock of the CAN bus. So for a 500 kilohertz clock the counter counts every 2 microseconds.

## 6.4. CAN code

The eCAN is not fully supported in MotorWare™. Later, a header file was added, which is a good introduction in the CAN support. However to use the CAN interface a C file needs to be added to the project. This is done using the steps of the SCI/UART tutorial [25]. Nevertheless, a user on the Texas Instruments E2E forum had the same problem and integrated the CAN module himself using the eCAN selftest of the F28069M development board [26]. How the code can be added to lab 11a can be found in appendix A.

The most important functions used in the CAN.c file in appendix D are:

- **ECAN\_init**

Allocate memory to the different registers.

- **ECAN\_setBitrate**

Change the bitrate of the CAN module. There can be chosen to set it on 1 MHz, 500 kHz, 250kHz, 125kHz, 100kHz, 83kHz, 50kHz or 20kHz. The default setting is 500 kHz.

- **ECAN\_setBTCreg**

Configure the rest of the Bit timing configuration register.

- **ECAN\_clearMSGCTRL**

Clear the Message Control of the mailboxes.

- **ECAN\_clearMSGID**

Clear the Message ID's of the mailboxes.

- **ECAN\_clearMDL**

Clear the Data Low of the mailboxes.

- **ECAN\_clearMDH**

Clear the Data High of the mailboxes.

- **ECAN\_enableAllMailbox**

Set the CANME register of all mailboxes to 1 to enable the mailboxes.

- **ECAN\_setTXIO**

Set the CANTXIO to 1 to enable the transmit functionality.

- **ECAN\_setRXIO**

Set the CANRXIO to 1 to enable the receive functionality.

- **ECAN\_setSCCmode**

Use the Standard CAN configuration mode. The CAN module uses only 16 mailboxes instead of 32.

- **ECAN\_setECANmode**

Use the full functionality of the CAN module. The module uses all 32 mailboxes.

- **ECAN\_clearCANTA**

Write to every CANTA register a 1 to clear all the transmission acknowledgements.

- **ECAN\_clearCANRMP**

Write to every CANRMP register a 1 to clear all the received message pending register bits.

- **ECAN\_SelfTest**

Define if the eCAN module has to use Self Test or use normal CAN mode.

- **ECAN\_setMailboxDir**  
Set the directions of each mailbox. This is done by writing a 1 to let a mailbox receive or set a 0 to transmit.
- **ECAN\_configMailbox**  
Configure the mailbox completely: Enable it, Set the Message ID, Specify number of bits that will be transmit or received. And finally define what mailbox direction is used.
- **ECAN\_putDataMailbox**  
Write data to the mailbox MDL and MDH registers.
- **ECAN\_configMasterReg**  
Configure the master control register.
- **ECAN\_sendMSG**  
Send a message. First specifying the Data in the MDL and MDH register. Than set the CANTRS register to send the actual message and finally wait for an acknowledgement in the CANTA register.

# 7

## Conclusion

In this thesis the different subjects presented in section 1.3 and section 1.4 have been discussed. A proper study has been done on different control methods and field oriented control was chosen as the most effective technique. FOC is effective at low speeds, and has a low torque ripple. Both of these characteristics make it a good solution for Nuna.

To get started with developing the FOC, Texas Instruments InstaSPIN™ technology was used. This provides an extensive developing environment, including ready to go development boards. The integrated FAST™ algorithm makes this solution unique and accurate. The ability to quickly and accurately estimate the flux, angle, speed and torque, as well as calculating motor parameters while running, was a big factor in the decision to use this technology. The project supervisor and other staff at TU Delft have experience with this developing environment already, which made the decision for this technology even easier. The LAUNCHXL-F28069M was used in combination with the BOOSTXL-DRV8301 Rev. B. The MCU on the LAUNCHXL already has FOC implemented in it, with a software encoder algorithm to keep the control fully sensorless.

Using these two boards together with a set of development motors, a simulation set-up was made. The set-up will allow people from the Nuon Solar Team to understand and interact with the controller quite easily. The Nuna motors can also be driven at low power with the development boards. How the control is implemented in the software is explained in this thesis. The connections on the LAUNCHXL-F28069M have been discussed as well. This means the Nuon Solar Team can connect the controller to a different inverter in a further stage of development. The CAN-interface capabilities have also been implemented, so the Nuon Solar Team can specify which values they want to input and output during driving.

For use of the simulation set-up, an elaborate manual was made. This will guide users through the installation of the required software from Texas Instruments and setting up the hardware. The Texas Instruments environment can be quite hard to grasp, because all kinds of different software packages have to be installed. With this manual it will become more clear on what is needed and what is not needed to set up the controller development.

Of the deliverables stated in section 1.4 all are done. The control method study can be found in chapter 2, the implementation choices and simulation set-up are explained in chapter 4 and chapter 5, the manual can be found in appendix A, and the recommendations for further research are in chapter 8.



# 8

## Discussion & Recommendations

### 8.1. Discussion

While all the deliverables have been achieved, one big issue came up that delayed the project and had influence on the quality of the delivered result. The incompatibility of the BOOSTXL-DRV8323RH with the LAUNCHXL-F28069M was a major setback on the progress of the project. On the Texas Instruments website the LAUNCHXL-F28069M is listed on the page of the BOOSTXL-8323RH as a product that is compatible. However, when both the development boards arrived and were connected to each other, it became clear quite quickly that they were not properly configured to work together. The students did not understand why this was the case, because the boards were from the same manufacturer, the same product range and had the same technology on them.

Figuring out why the board did not work cost quite some time, and when the Hardware Quick Start Guide of the DRV8323RS was found, the problem seemed to have been solved. When the hardware adjustments (described in section 4.2.2) were made according to this guide, it became clear that software adjustments also had been made. At this point already almost two weeks had been spent on trying to get the boards to work together, as it was the first time either of the students worked with the Texas Instruments environment and could not fully comprehend what was going wrong. The decision was made to switch to the BOOSTXL-DRV8301 Rev. B, which worked properly the moment it was connected to the LAUNCHXL-F28069M.

A lot of time went into figuring out what was wrong with the first board, and that time could have been used more efficiently to explore more features of the control. This would not have been an issue if Texas Instruments had a clearer website. During this project, it became clear that the Texas Instruments environment is mostly built for people who know what they want and already have an idea of how to achieve that. Texas Instruments could benefit from making their software and support more beginner-friendly, as it is quite complicated and confusing when starting out.

In retrospective, it would have been wiser to switch to the BOOSTXL-DRV8301 sooner, because it only became clear what was wrong when the project had progressed quite a bit further. The understanding of the hardware and software came later because it took the students working with the BOOSTXL-DRV8301 to get how the boards interact and how the control works. The BOOSTXL-DRV8323RH can still be used with the LAUNCHXL-F28069M, but before it will work the communication with the boards has to be adjusted. The DRV8323RH works through a GPIO interface, while the DRV8301 works with SPI.

### 8.2. Recommendations

While some things did not go as planned, this project has still made a good start on the development of a motor controller. It is clear that the path started with this thesis can be a very fruitful one for the Nuon Solar Team. Some recommendations are done for future research based on this thesis.

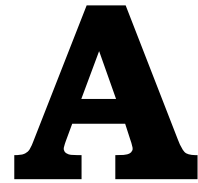
- While the BOOSTXL-DRV8323RH can be made to work with the LAUNCHXL-F28069M, it is not recommended to put any more time in doing this. The BoosterPacks are just tools to get the simulation set-up running, running demos on the Nuna motors and doing early prototyping on

the control. While the DRV8323RH can deliver more power than the DRV8301, it will still not be able to drive the motor properly. For the applications stated, the DRV8301 does the job well enough and the DRV8323RH provides very little benefits. In a further stage of development, another inverter will have to be used anyway, and until then the DRV8301 is sufficient.

- The CAN-interface has been integrated to work with lab 11a, and values can be read and sent while the motor is running. It is still necessary for the Nuon Solar Team to specify exactly which values should be sent over the CAN-bus and what mailboxes to use. With this added the control will be able to properly interface with the rest of the car.
- When looking at inverters in the future, it is probably wise to leave the LaunchPad development kit in use right now. An inverter can be connected to the GPIO pins, and it will work, but the solution is not ideal. The pins on the LAUNCHXL-F28069M are quite fragile and the durability is questionable at best. Instead it is a good idea to design a custom PCB for the TMS320F28069M MCU. This is the same MCU as on the LaunchPad, but with a custom PCB it can be much better integrated. The signals coming from the inverter and the phases need to be processed with tuned circuits and on a custom PCB these could all be integrated in an efficient and durable way. Connections can also be placed in a convenient way. If the Nuon Solar Team decides to also look into building a custom inverter, the measurements and control could even be integrated right into the inverter, making the whole combination a reliable block.

With the basis presented in this thesis and the recommendations named above, developing a motor controller for Nuna should prove a fruitful endeavor, with which they can keep their championship title for years to come!





# InstaSpin™ manual

## A.1. Introduction

This manual is to help people regarding the combination of the TI LAUNCHXL-F28069M in combination with the TI BOOSTXL-DRV8301 and two Teknic inc. Hudson BLDC motors. It helps by telling how the software needed has to be installed and in what order. Furthermore it explains how a FOC control (and CAN capabilities) can be implemented using Motorware.

## A.2. Hardware

To build the simulation set-up the following equipment is needed:

- 2x Texas Instruments LAUNCHXL-F28069M

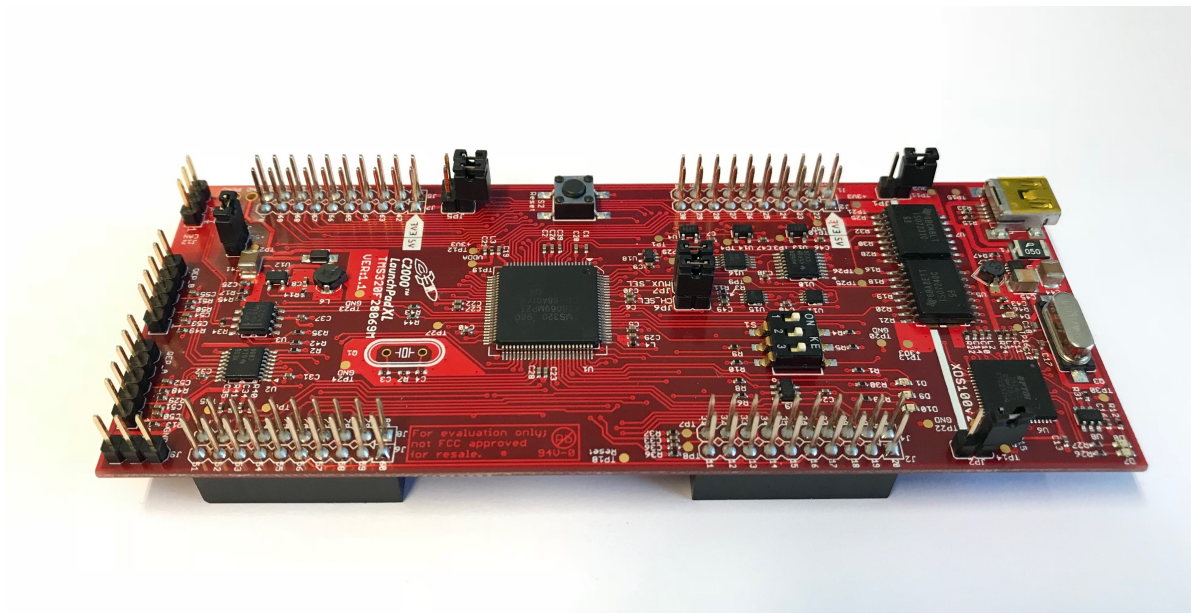


Figure A.1: TI LAUNCHXL-F28069M

- 2x Texas Instruments BOOSTXL-DRV8301 rev. B

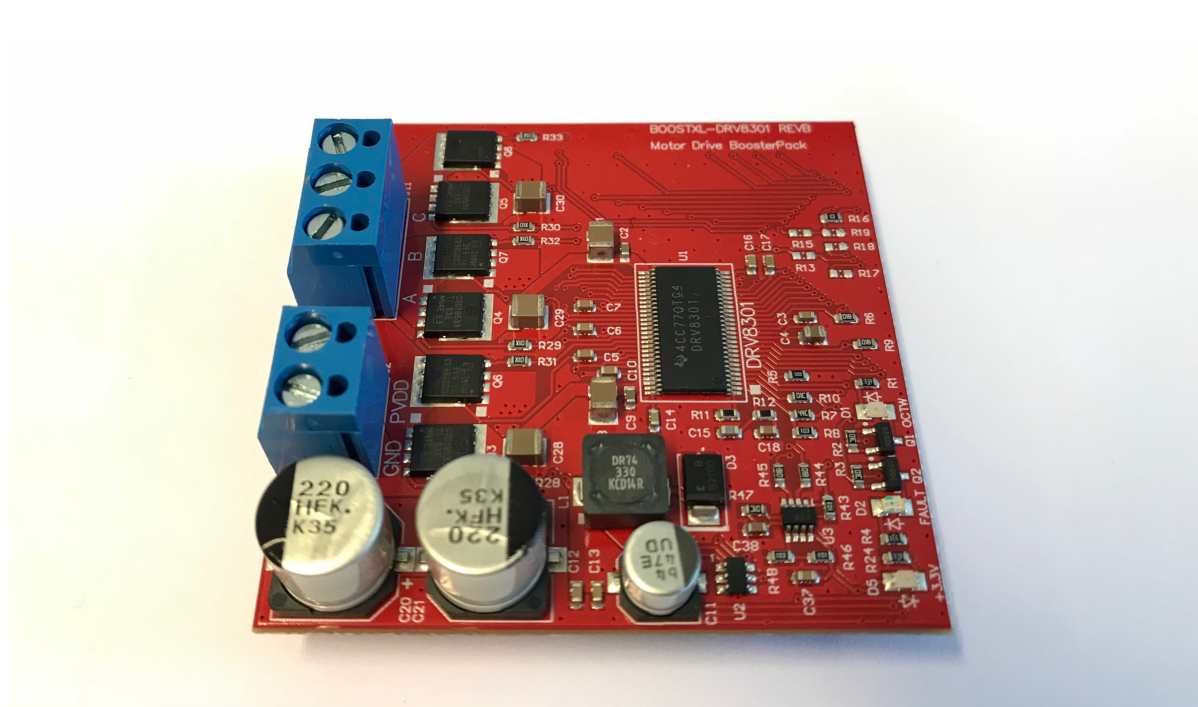


Figure A.2: TI BOOSTXL-DRV8301 Rev. B

- 1x Texas Instruments 2MTR-DYNO InstaSPIN-FOC Evaluation Module (this includes 2x Teknic Hudson M-2310, a shaft coupler and a frame mount for stability)

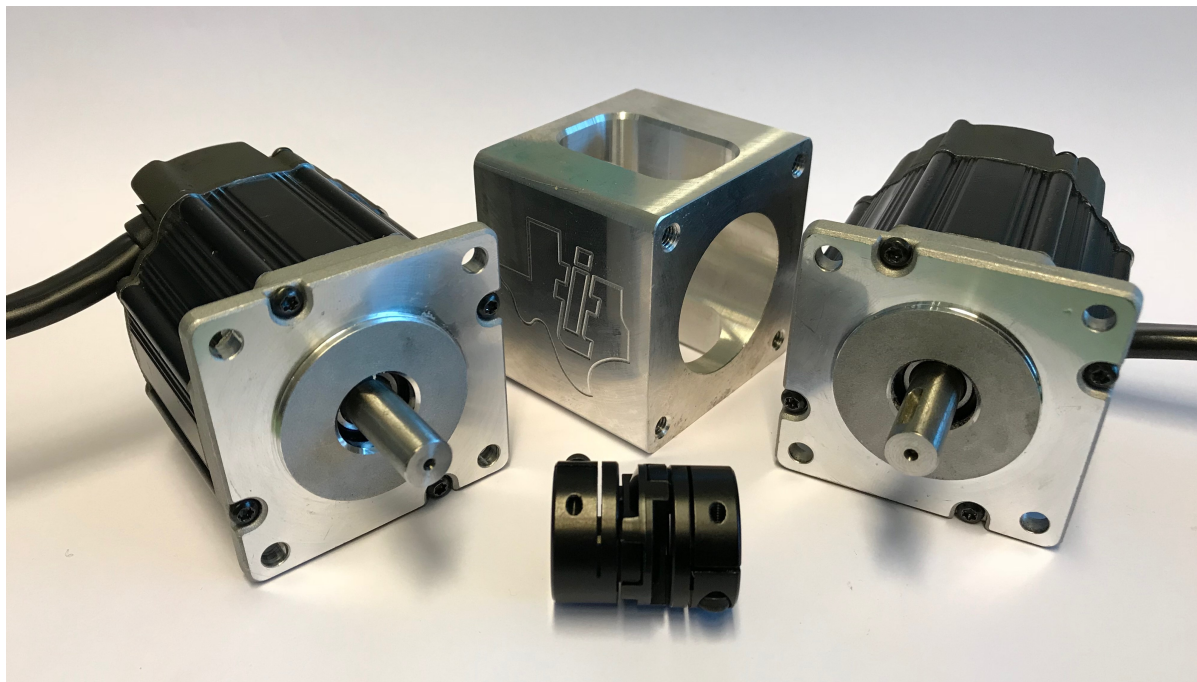


Figure A.3: Components of the 2MTR-DYNO kit

- 1x Power supply of 30 volt and 10 ampère
- Clamps to secure the set-up to the table
- 2x Personal computer running Microsoft Windows (in this manual Windows 10 Home is used)
- Cables to connect the BOOSTXL to the power supply

## A.3. Software installation

The following software is needed to get the set-up running:

1. Code Composer Studio IDE
2. MotorWare™
3. C2000Ware

### A.3.1. Code Composer Studio

1. Go to [http://processors.wiki.ti.com/index.php/Download\\_CCS](http://processors.wiki.ti.com/index.php/Download_CCS).
2. Download either the offline or online installer for Windows of the latest version of Code Composer Studio (in this manual the offline installer for Code Composer Studio 7.3.0 is used).

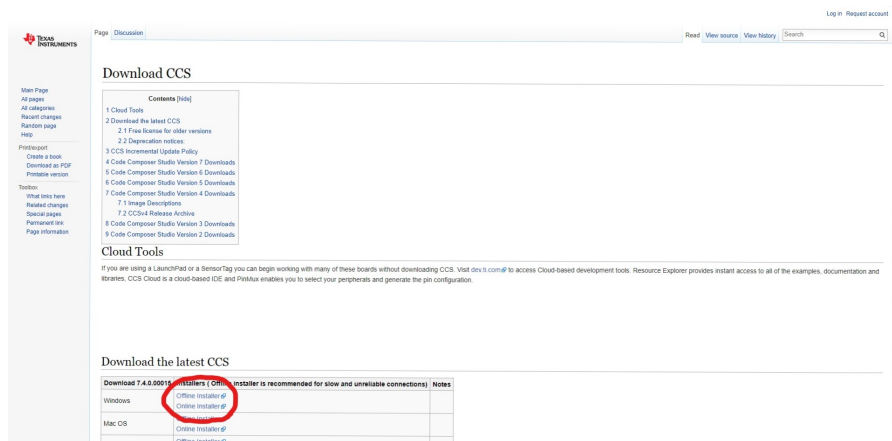


Figure A.4: step 2

3. Unzip the file and open `css_setup_[version].exe`

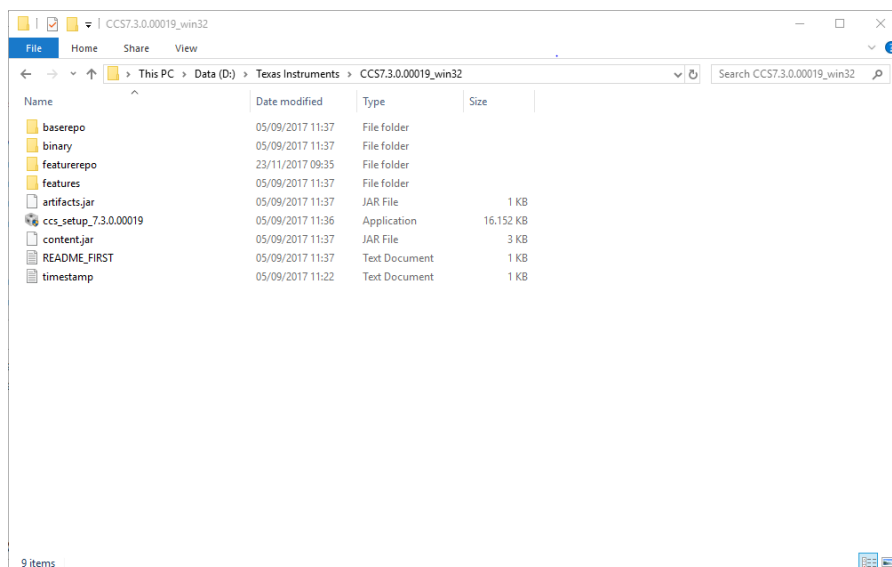


Figure A.5: step 3

4. A security warning will pop up. Click "Yes".

5. Click "Continue".

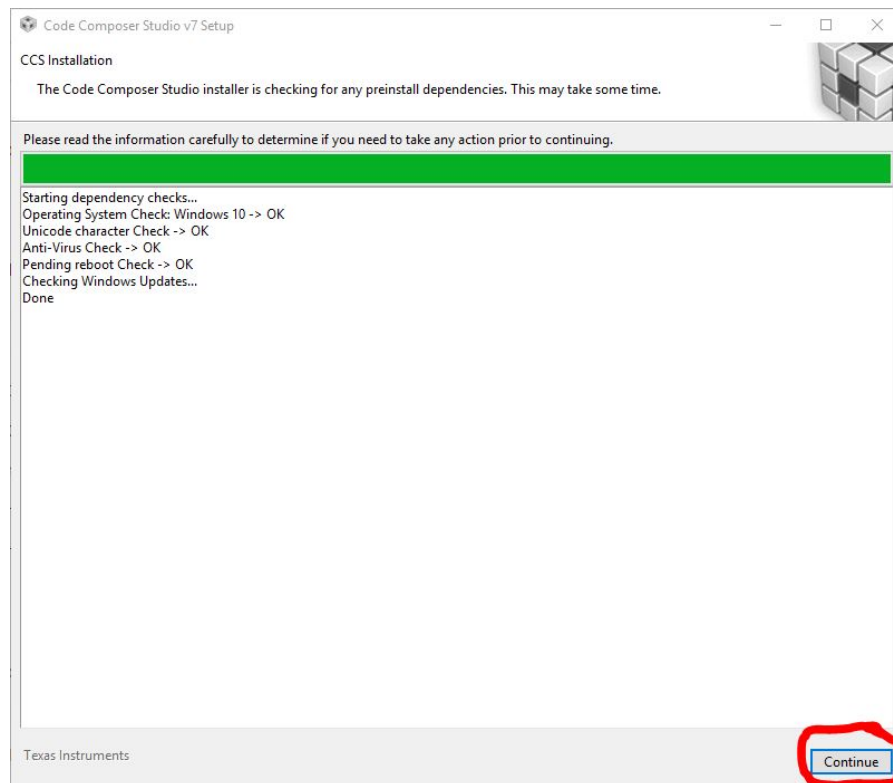


Figure A.6: step 5

6. Accept the terms of the license agreement and click "Next".

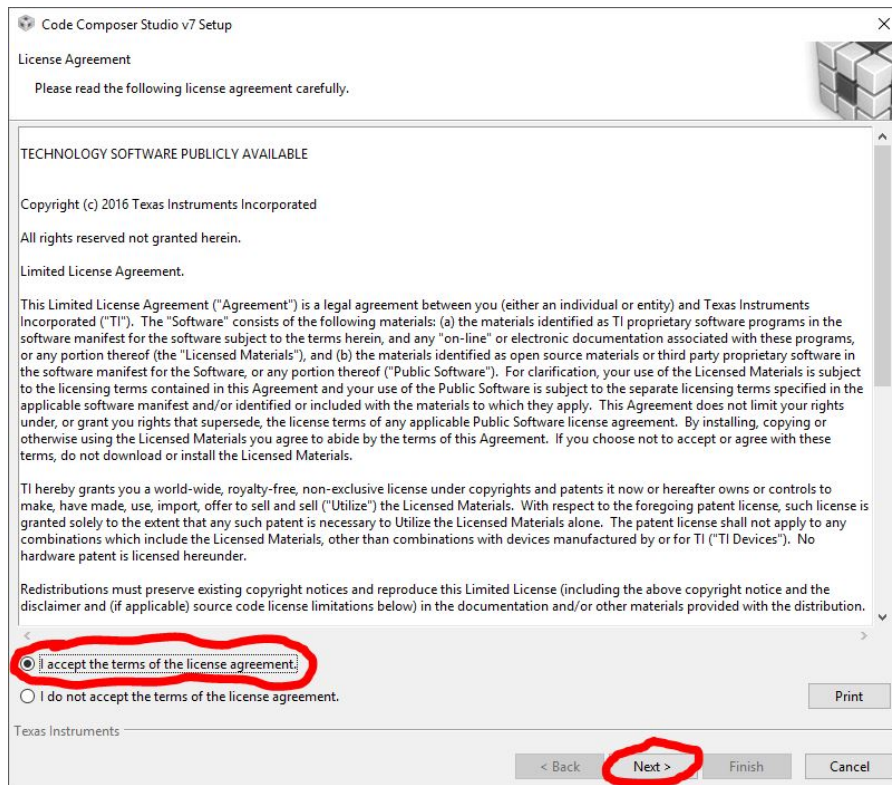


Figure A.7: step 6

7. Select a directory to install to and click "Next". (c:\ti is recommended).

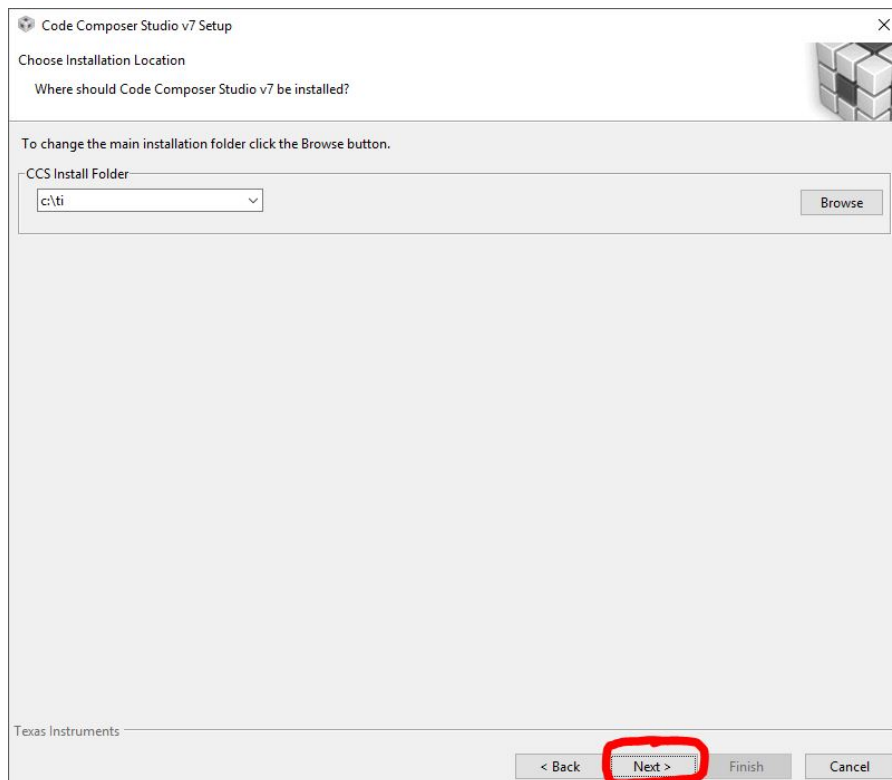


Figure A.8: step 7

8. Select the C2000 real-time MCUs family to be installed and click "Next".

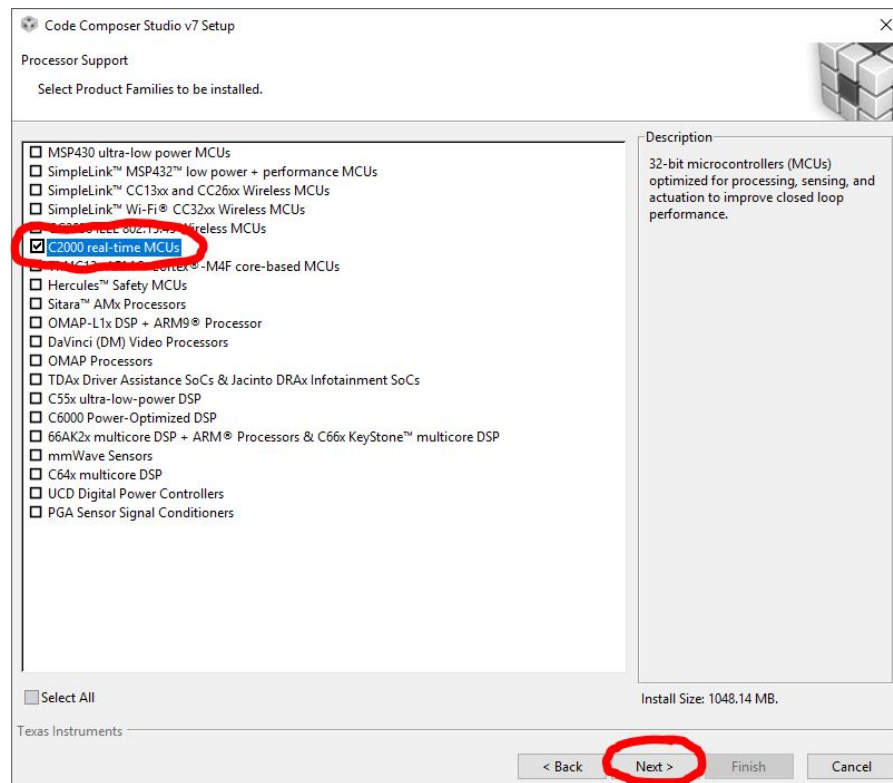


Figure A.9: step 8

9. Make sure the TI XDS Debug Probe Support is selected and click "Finish".

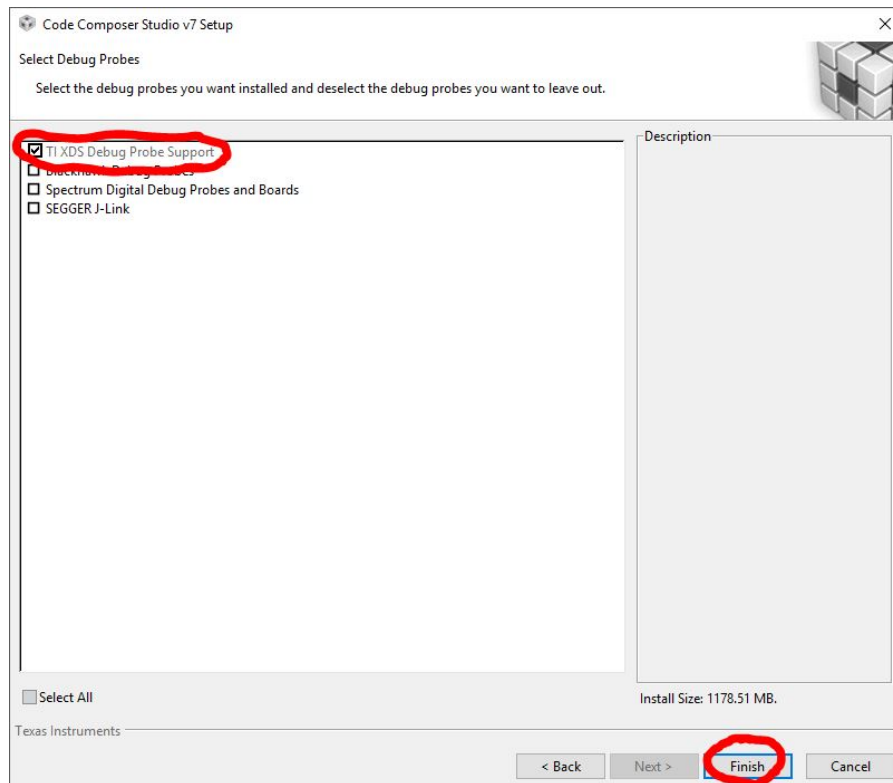


Figure A.10: step 9

10. Wait for the installer to install Code Composer Studio and the packages (this will take a few minutes).

11. Deselect "Launch Code Composer Studio" and any other options you don't want.

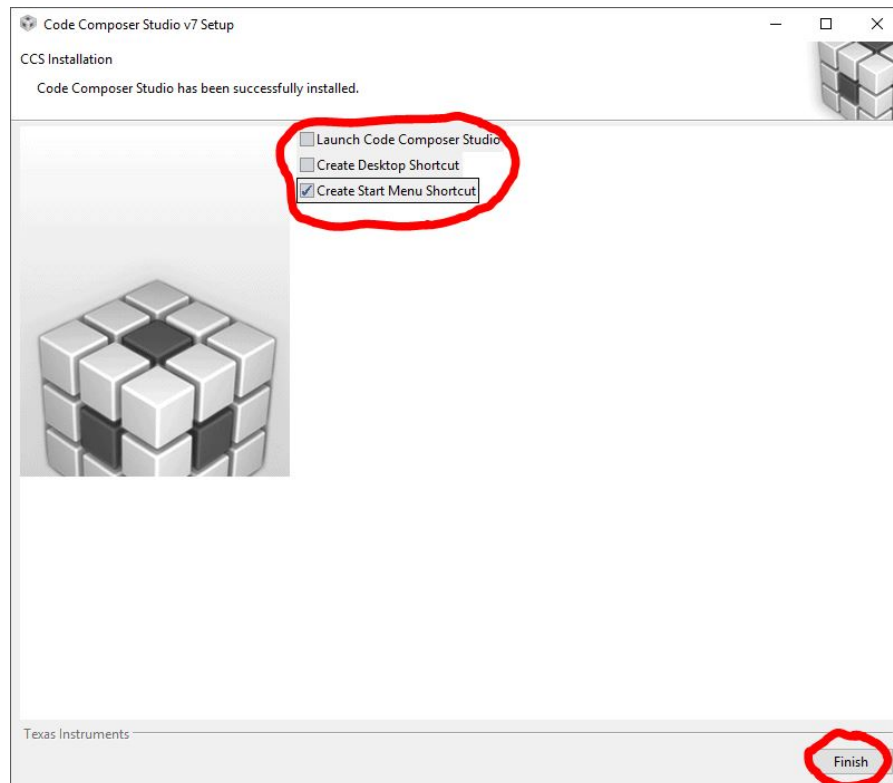


Figure A.11: step 11

### A.3.2. MotorWare™

1. Go to <http://www.ti.com/tool/MOTORWARE>.
2. Click the download button.

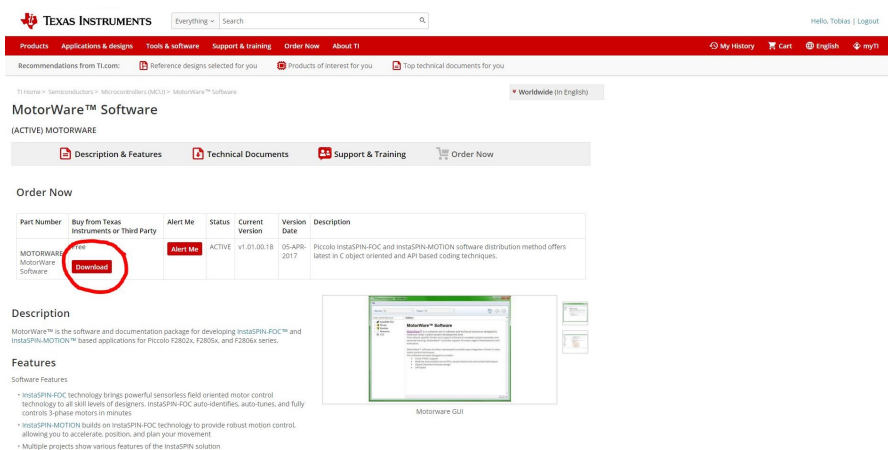


Figure A.12: step 2

3. Register a new MyTI account or log in if you already have an account.



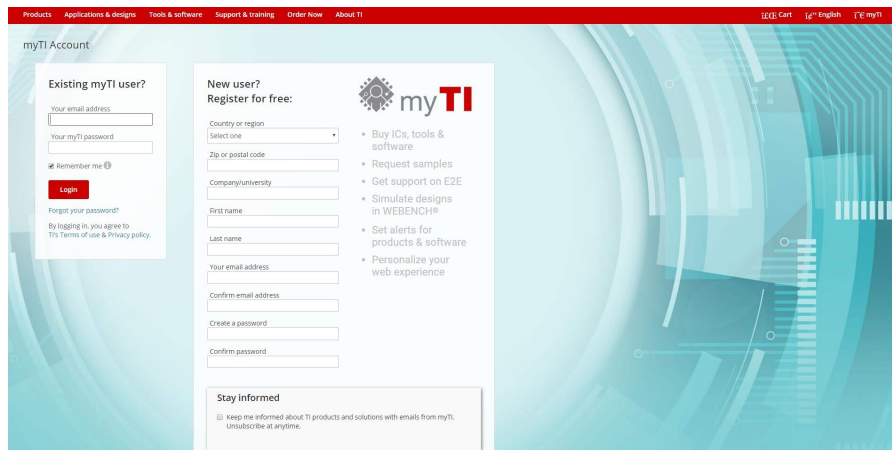


Figure A.13: step 3

4. You will need to fill out a U.S. Government Export Approval form to be able to download MotorWare™. Select “Civil” in the application category, and select “Yes” at “I CERTIFY ALL OF THE ABOVE IS TRUE:”. Then submit the form.

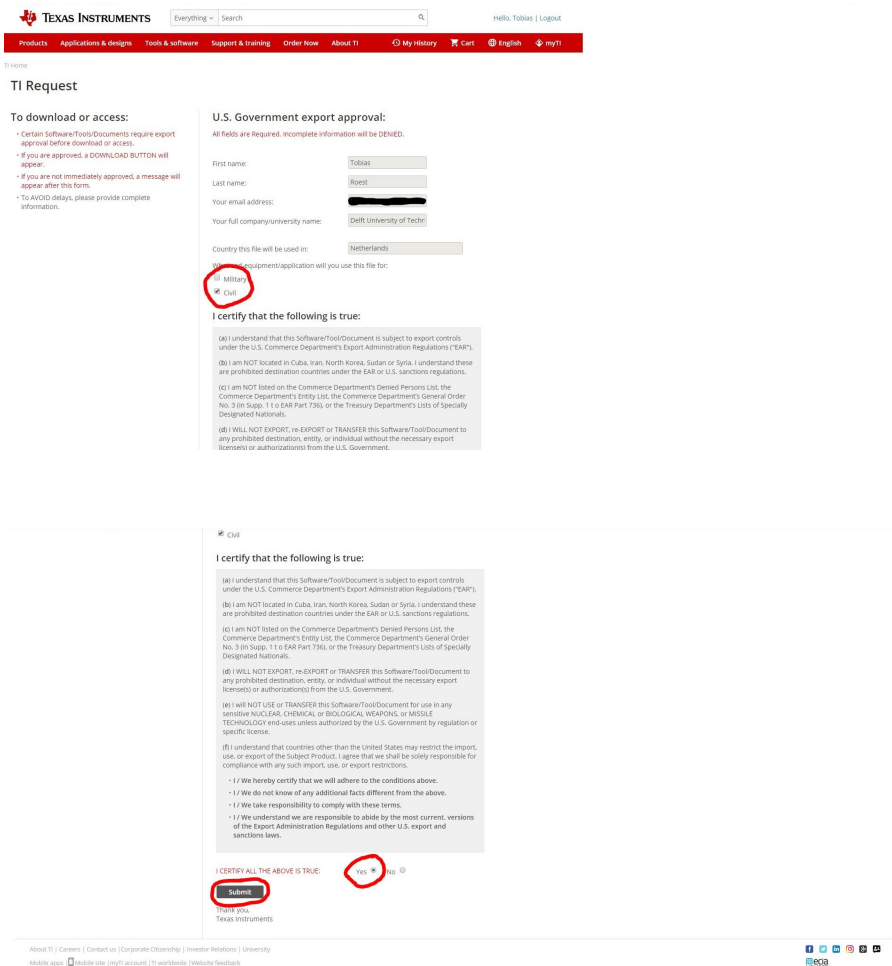


Figure A.14: step 4

5. Click “Download”.

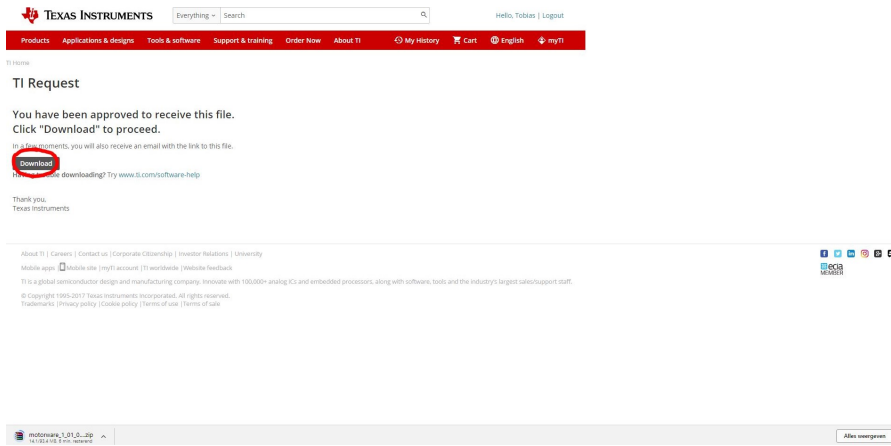


Figure A.15: step 5

## 6. Unzip motorware\_[version].zip and run motorware\_[version]\_setup.exe

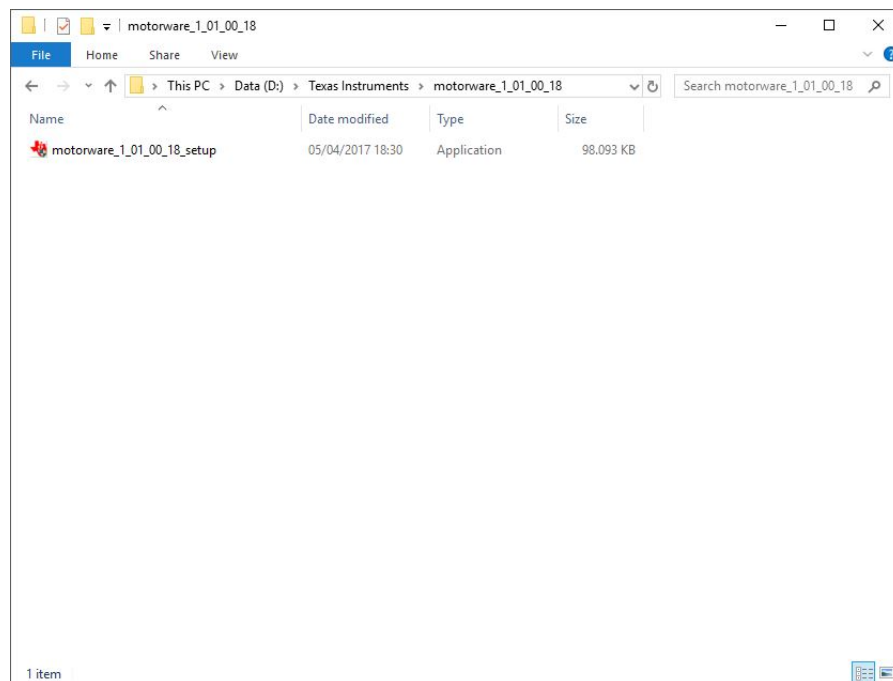


Figure A.16: step 6

7. A security warning will pop up. Click "Yes".

8. Click "Next".

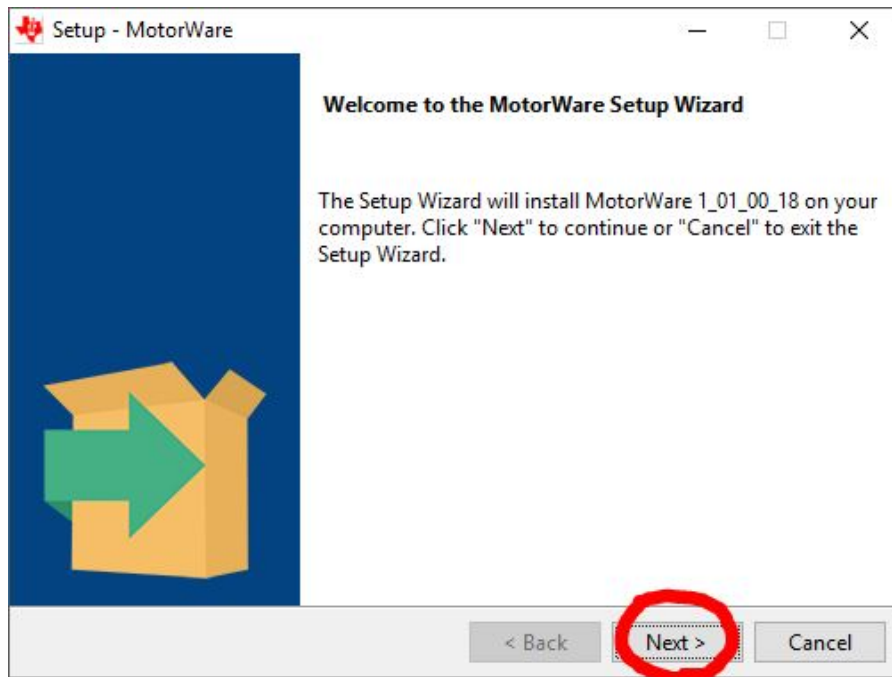


Figure A.17: step 8

9. Accept the End-User License Agreement and click "Next".

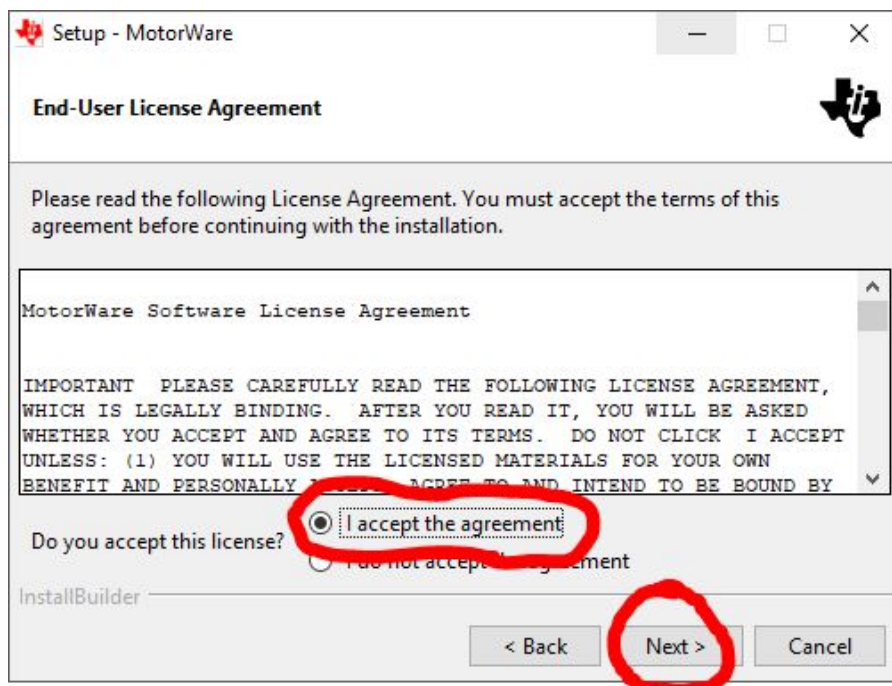


Figure A.18: step 9

10. Select a directory to install to and click "Next". (c:\ti\motorware is recommended). Make sure the directory is in the same folder as Code Composer Studio.

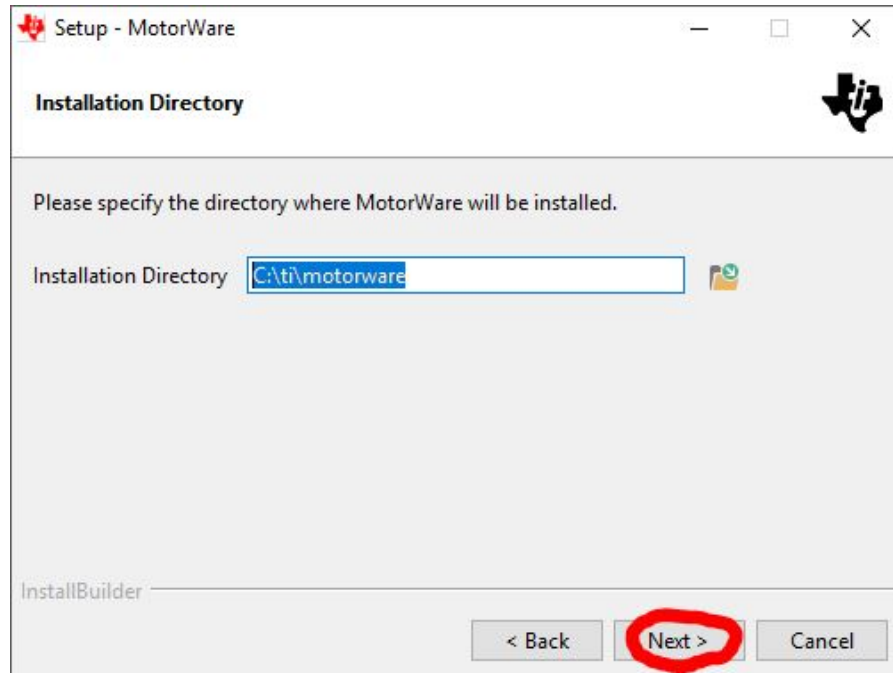


Figure A.19: step 10

11. Click "Next".

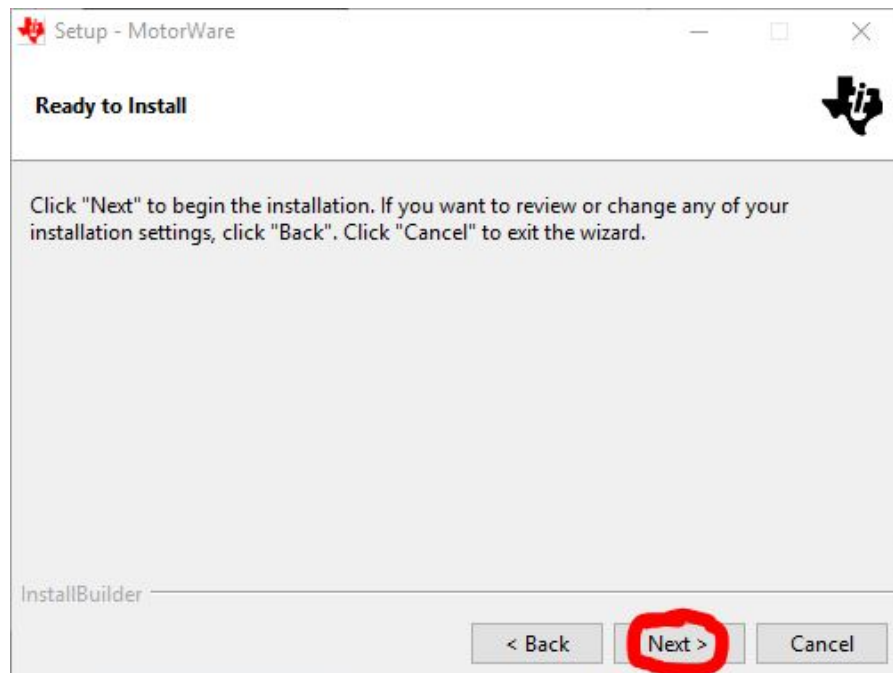


Figure A.20: step 11

12. Wait for the installer to install MotorWare™.
13. Click "Finish".

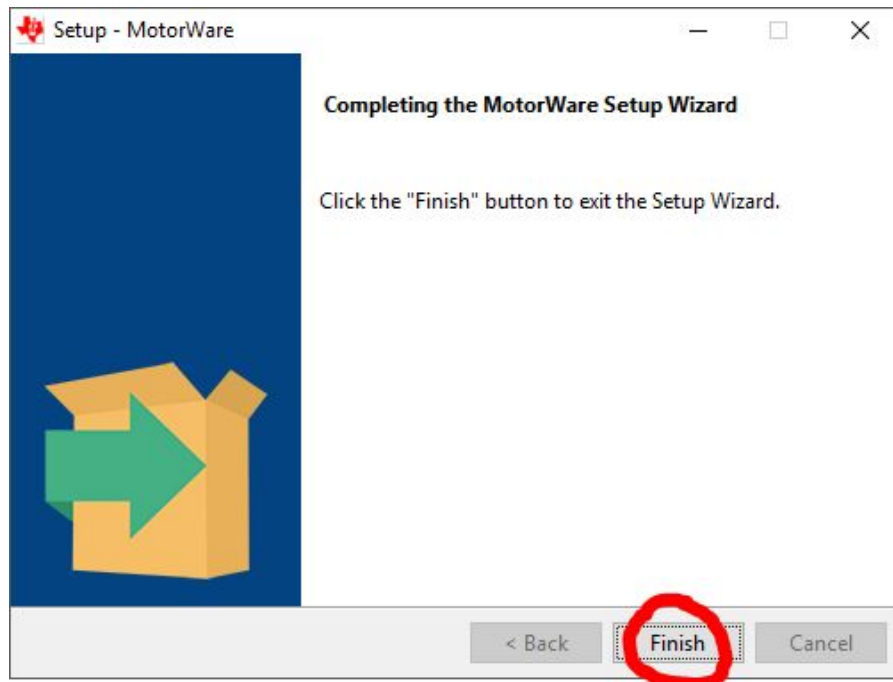


Figure A.21: step 13

### A.3.3. C2000Ware

1. Go to <http://www.ti.com/tool/C2000WARE>.
2. Click the "Get Software" button.

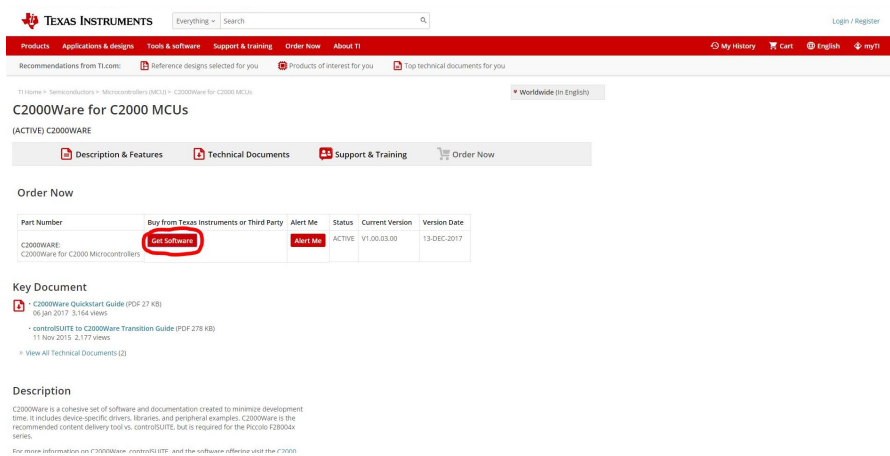


Figure A.22: step 2

3. Click the link for the Windows installer.

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### C2000Ware for C2000 Microcontrollers

C2000WARE\_1.00.03.00  
Release Date: 13 Dec 2017

View release notes Supported Platforms What's New? Release information

This page contains specific information about C2000Ware for C2000 Microcontrollers release package. Refer to the table below for download links and related content.

#### Product downloads

Download requires export approval (1 minute)

Title	Version	Description	Size
C2000Ware Installers			
Windows installer for C2000Ware	1.00.03.00	Windows Installer for C2000Ware	184239K
macOS installer for C2000Ware	1.00.03.00	macOS Installer for C2000Ware	180282K
Linux installer for C2000Ware	1.00.03.00	Linux Installer for C2000Ware	182092K
C2000Ware Documentation			
TI Resource Explorer	1.00.03.00	C2000Ware in Cloud TI Resource Explorer	
C2000Ware Quick Start Guide	1.00.03.00	C2000Ware Quick Start Guide	
ControlSUITE to C2000Ware Transition Guide	1.00.03.00	ControlSUITE to C2000Ware Transition Guide	

#### Supported Platforms

Platform	Supported Devices
Piccolo	F2802X F2803X

Figure A.23: step 3

4. Register a new MyTI account or log in if you already have an account. (Account as probably been made before while installing MotorWare™).

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Your myTI password  
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Company/university

First name

Last name

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Confirm email address

Create a password

Confirm password

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- Simulate designs in WEBENCH®
- Set alerts for products & software
- Personalize your web experience

Figure A.24: step 4

5. You will need to fill out a U.S. Government Export Approval form to be able to download MotorWare™. Select "Civil" in the application category, and select "Yes" at "I CERTIFY ALL OF THE ABOVE IS TRUE:". Then submit the form.

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Last name: Roest

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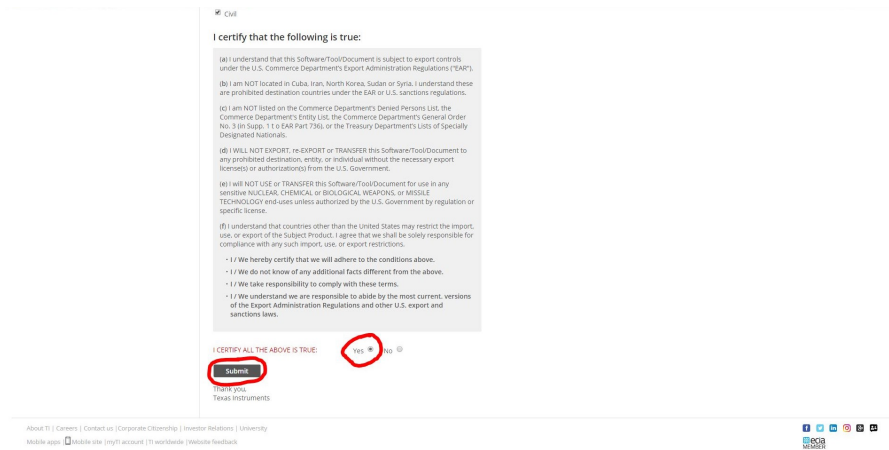


Figure A.25: step 5

6. Click "Download".

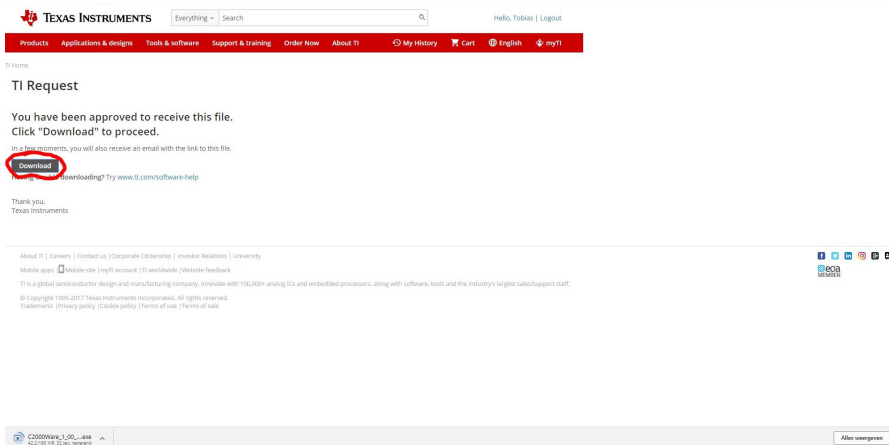


Figure A.26: step 6

7. Run C2000Ware\_[version]\_setup.exe

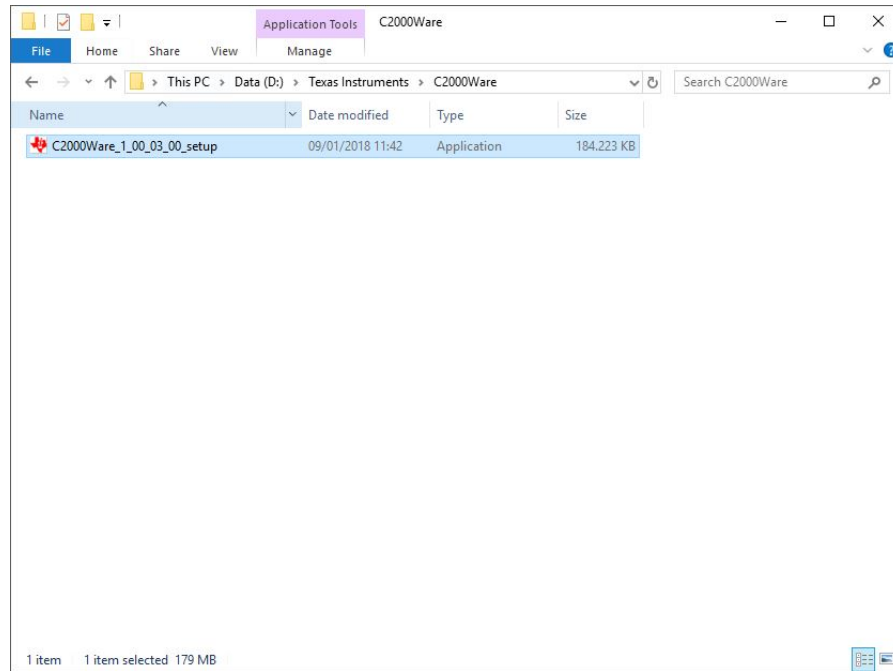


Figure A.27: step 7

8. Click "Next".

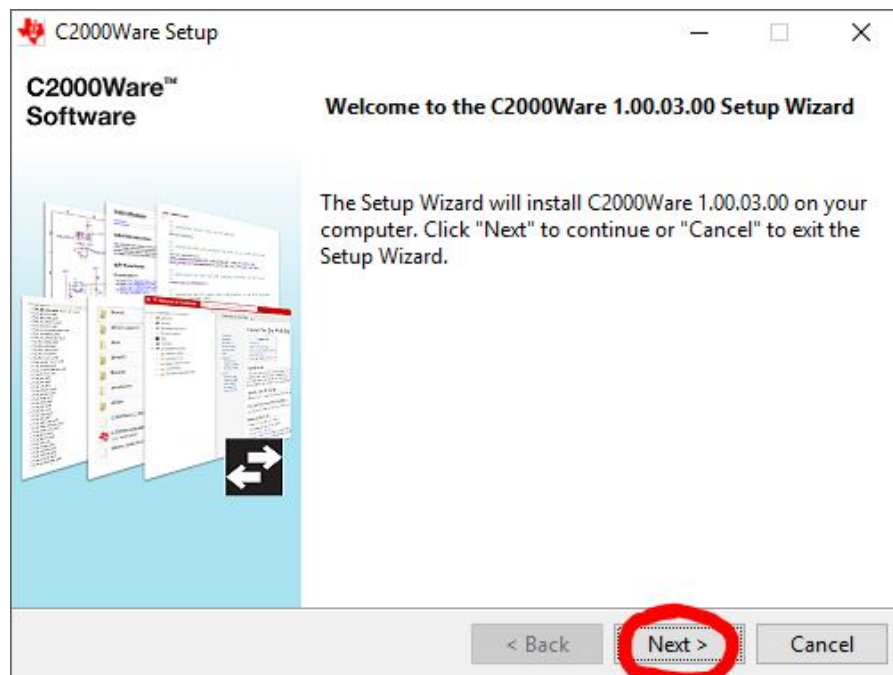


Figure A.28: step 8

9. Accept the End-User License Agreement and click "Next".



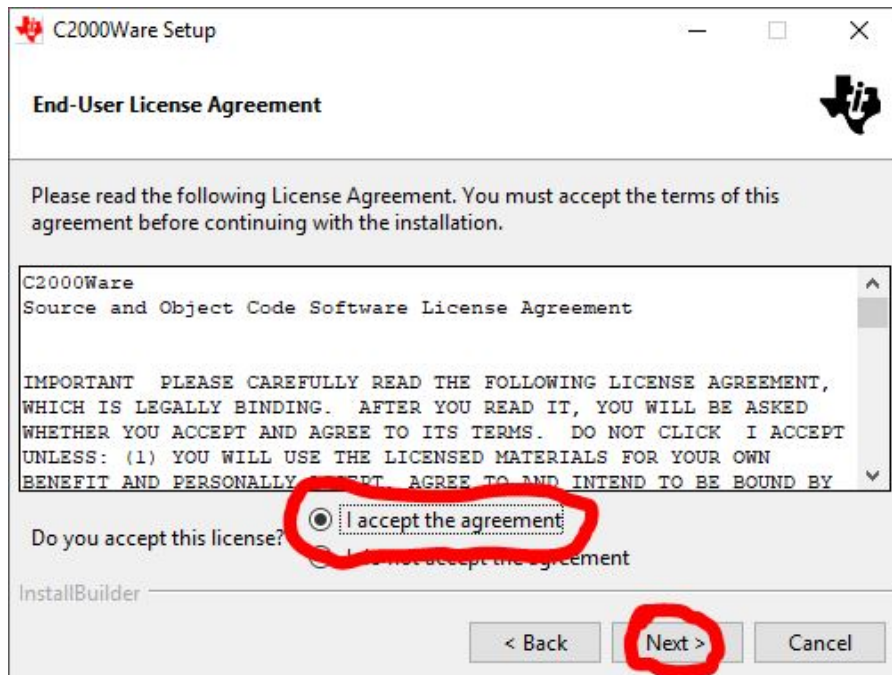


Figure A.29: step 9

- 10. Select a directory to install to and click "Next". (c:\ti\c2000 is recommended). Make sure the directory is in the same folder as Code Composer Studio and MotorWare™.

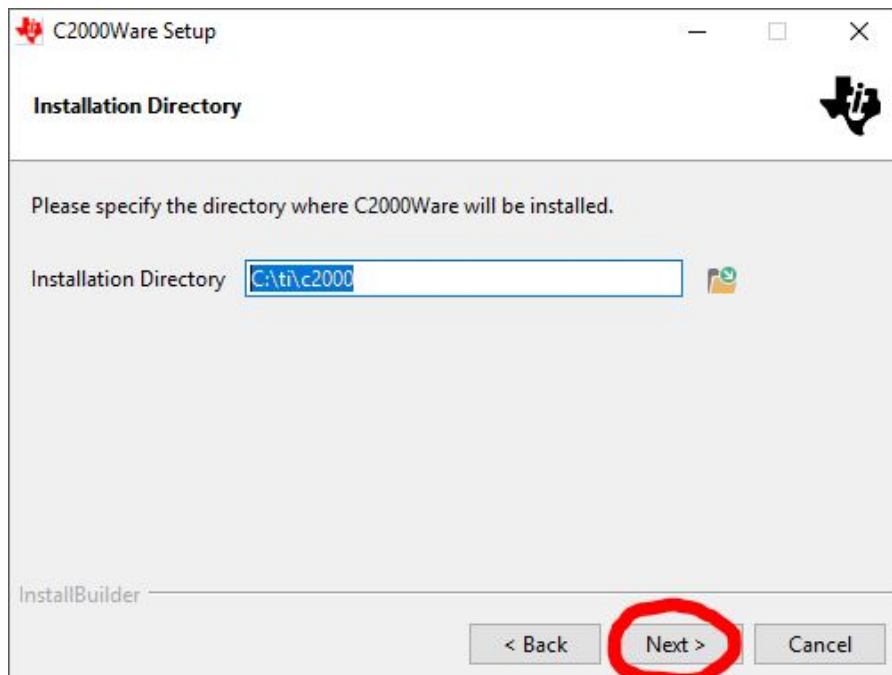


Figure A.30: step 10

- 11. Click "Next".

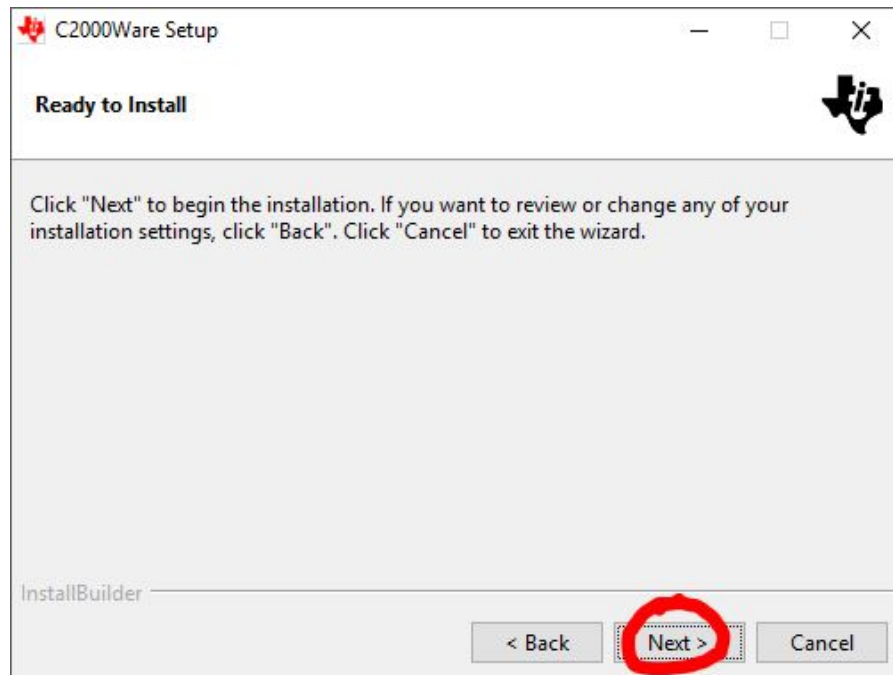


Figure A.31: step 11

12. Wait for the installer to install C2000Ware.
13. If you don't want to view the C2000Ware directory, deselect the box. Click "Finish".

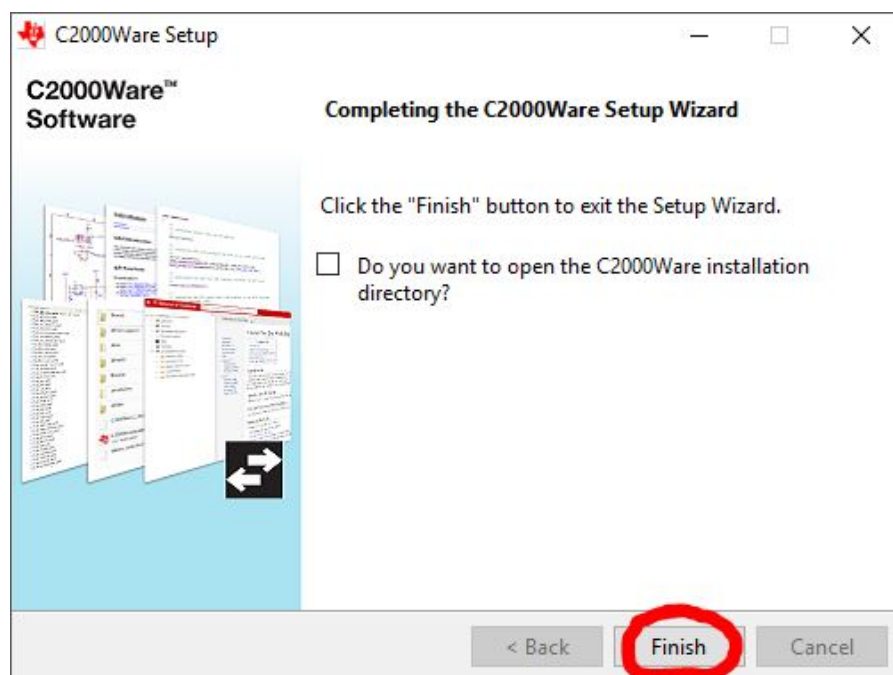


Figure A.32: step 13

#### A.4. Hardware configuration

1. Before connecting the LAUNCHXL-F28069M to anything, the settings of the board need to be changed. For this manual the board should be configured as follows [27]:

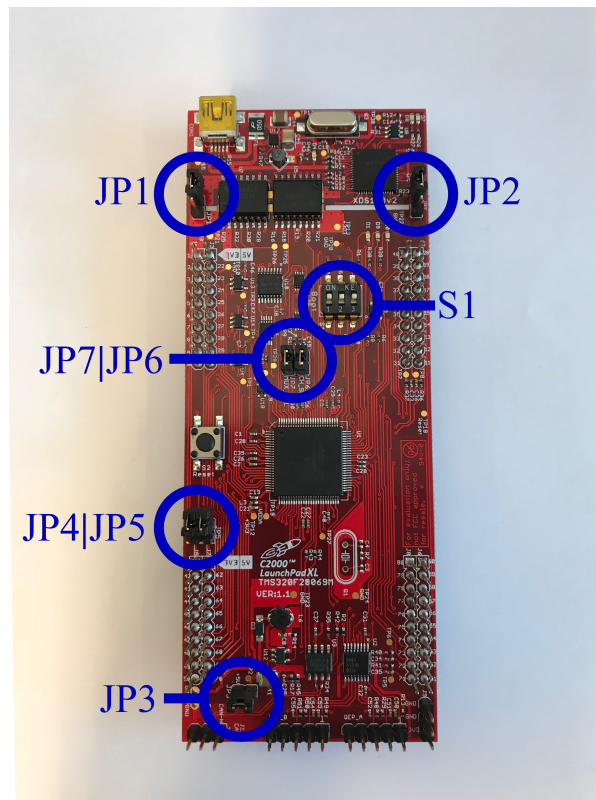


Figure A.33: The location of the jumpers and switches on the LAUNCHXL-F28069M

- Remove the jumpers from JP1 and JP2 to isolate the USB power from the rest of the board. The chip will be powered through the BoosterPack, but can still be programmed using USB.
- Set the switches on S1 to ON–ON–ON.
- Put the jumpers on JP3, JP6 and JP7.
- Jumpers 4 and 5:
  - Put the jumpers on JP4 and JP5, to use only the bottom BoosterPack headers J5-J8.
  - Remove the jumpers on JP4 and JP5, to use only the top BoosterPack headers J1-J4 or using both BoosterPacks J1-J4 and J5-J8.

The BoosterPack will be connected to J1-J4 so remove the jumpers from JP4 and JP5.

2. Connect the BOOSTXL-DRV8301 to the LAUNCHXL-F28069M, with the connections on the same side as the USB-port.

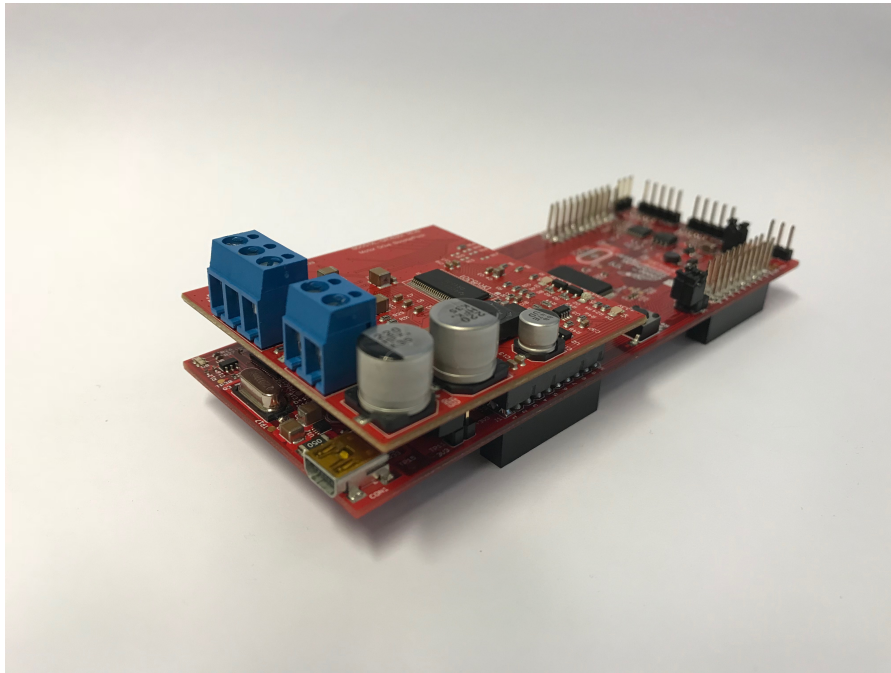


Figure A.34: The BOOSTXL-DRV8301 connected to the LAUNCHXL-F28069M

3. Connect the motor cable to the cable with smaller connections

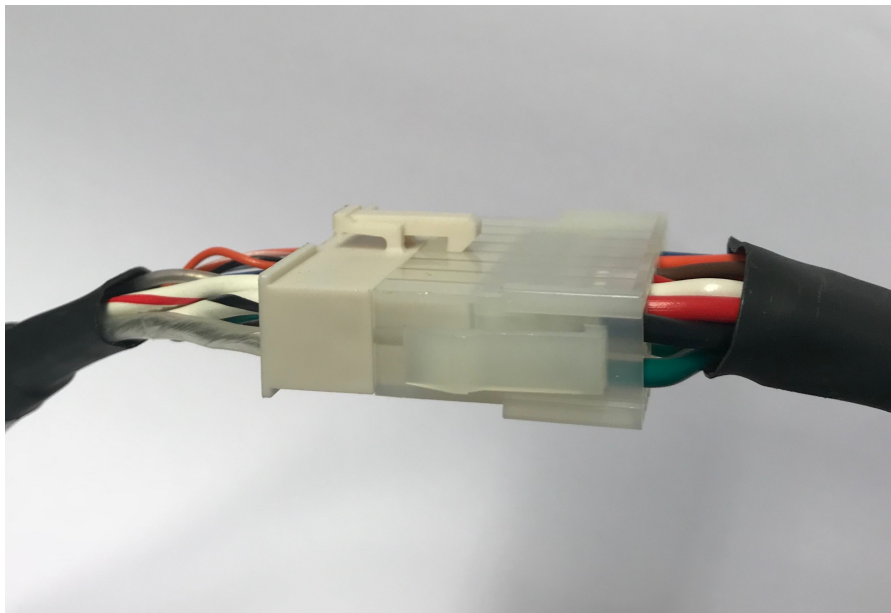


Figure A.35: The cable connection, the small hook clicks in place.

4. Connect the motor phase cables to the BOOSTXL-DRV8301. The green cable does not need to be connected, the other three can be connected in any way.

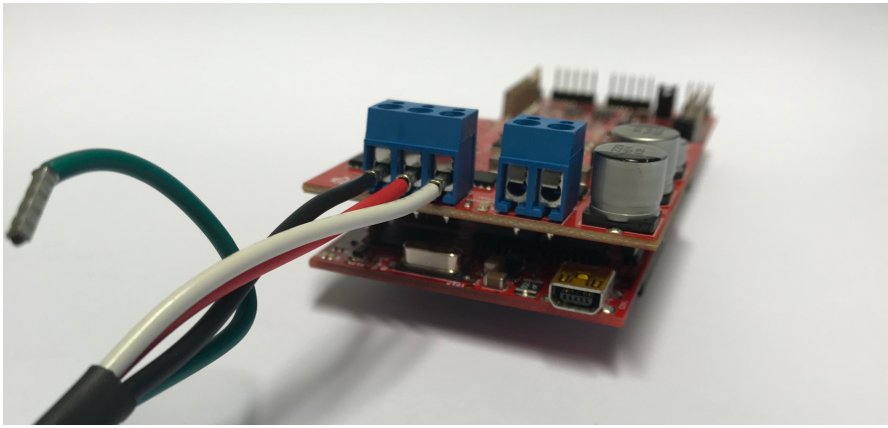


Figure A.36: The phase cables connected to the BOOSTXL-8301. The green cable should not be connected.

5. Connect the DC power cables to the BOOSTXL-8301.

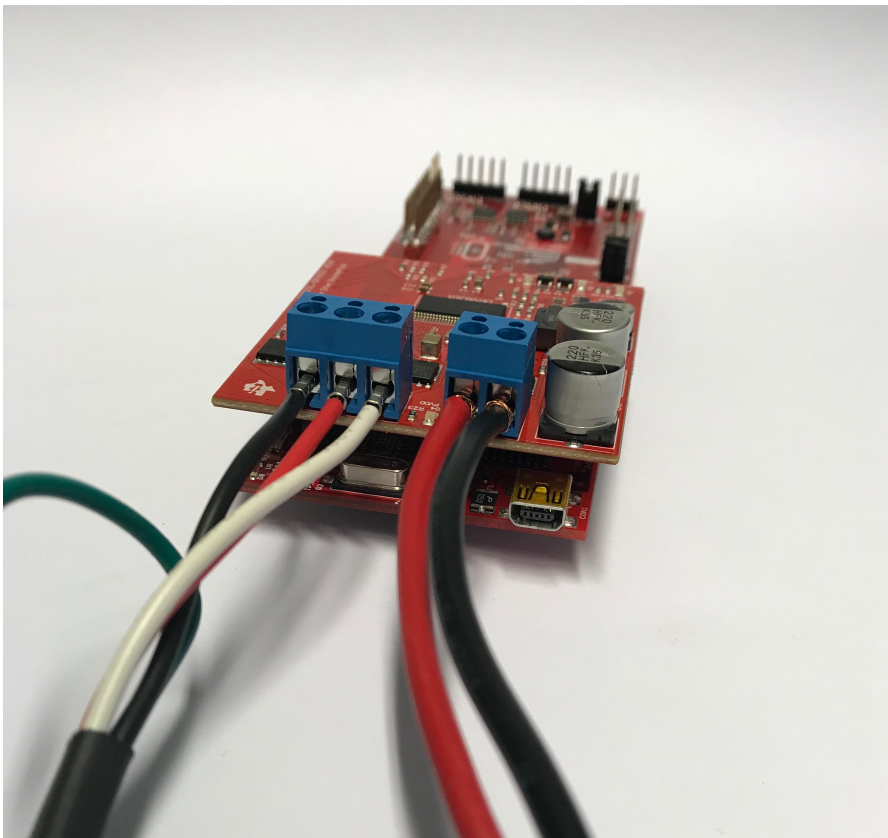


Figure A.37: The DC power cables connected to the BOOSTXL-8301.

6. Connect the DC cables to the power supply, and connect the LAUNCHXL-F28069M to your PC with the USB cable.



Figure A.38: The LaunchPad/BoosterPack combo with everything connected.

**If you want to work with one motor first to get familiar with the hardware and software, continue with step 7 and then appendix A.5. If you wish to get started on the simulation set-up with multiple machines right away, go to step 8.**

7. Fasten the Teknic Hudson M-2310 motor to the table using a clamp. Then continue with appendix A.5 and follow the InstaSPIN manual from there.



Figure A.39: Make sure the motor is clamped to the table firmly.

8. Repeat step 1-6, connecting the BoosterPack to the same power supply as the first one.

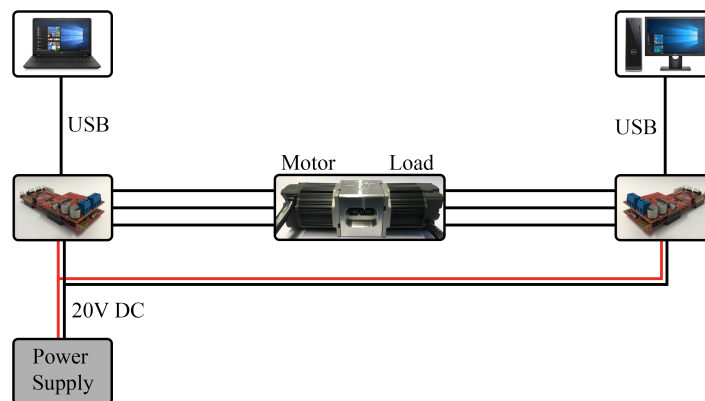


Figure A.40: A schematic representation of the simulation set-up which shows all the connections.

9. Find the Ruland Oldham coupling from the 2MTR-DYNO kit.



Figure A.41: The coupling used to couple the motors

10. Take it apart in two parts, one end, and one end with the middle part attached.



Figure A.42: The coupling in two pieces.

11. Make sure the motors are aligned 90 degrees from each other.



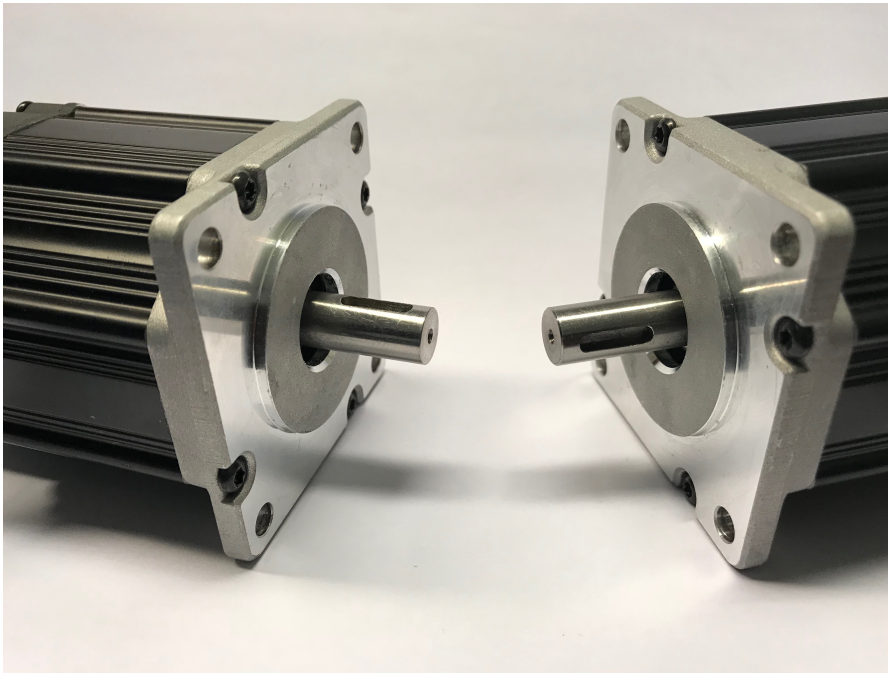


Figure A.43: The motor shafts should have a 90 degree angle.

12. Put the end of the coupling over the motor shafts. Do not shove them to far on the shaft, but rather leave them a bit over the edge.

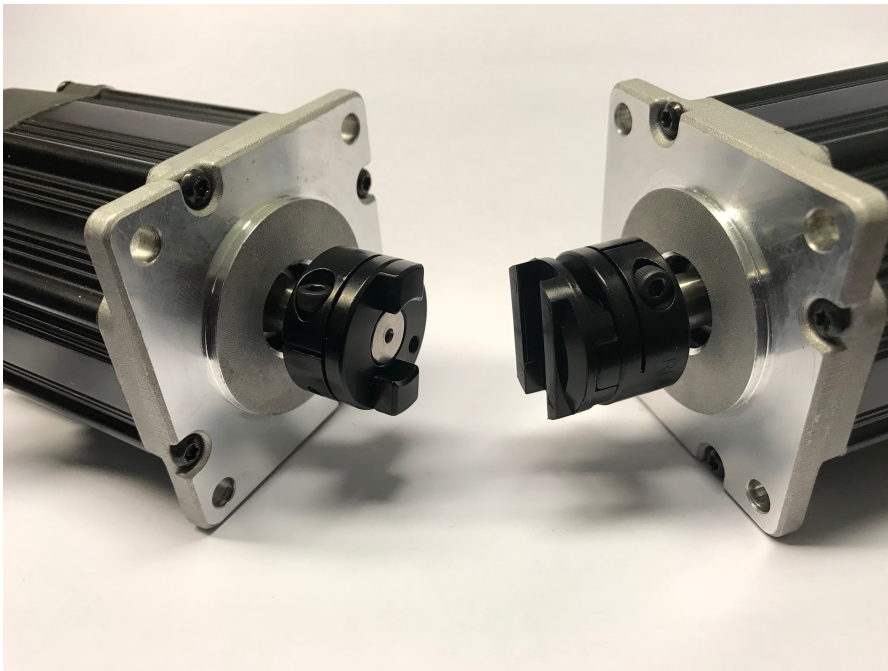


Figure A.44: The motors with the coupling parts over the shaft.

13. Place the two motors in the frame mount, make sure the coupling connects.

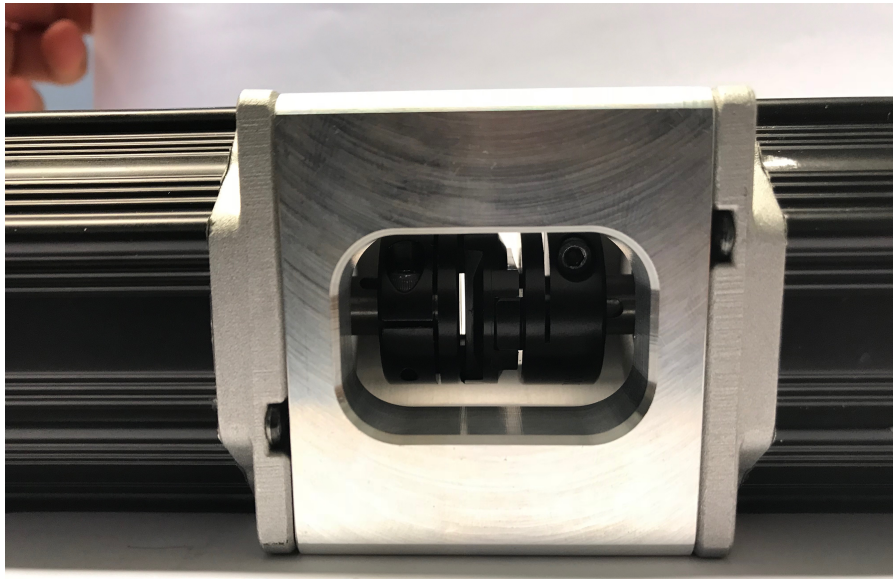


Figure A.45: The coupling is inside the frame mount.

14. Screw the motors to the frame mount with the eight screws.

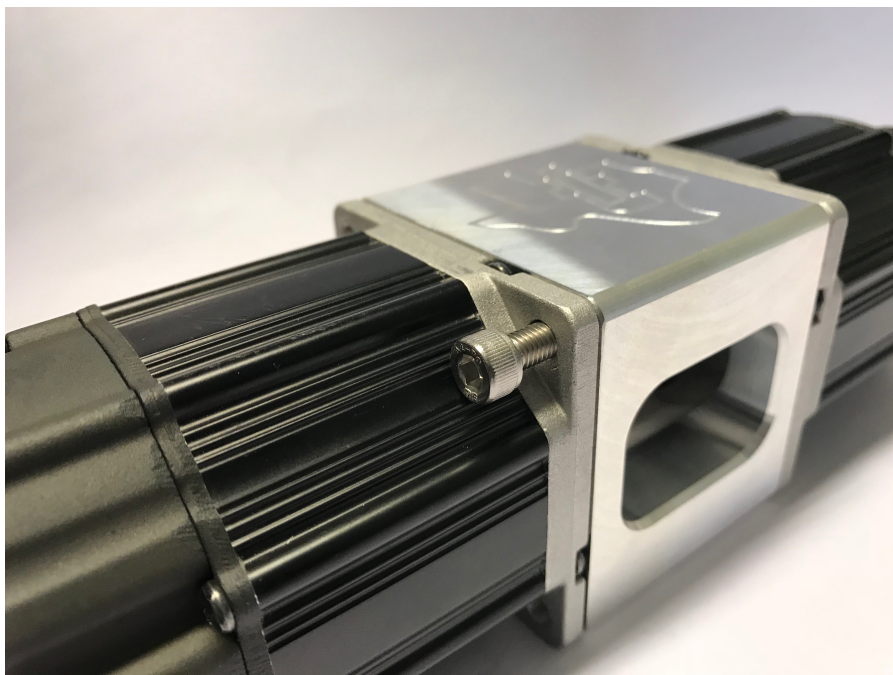


Figure A.46: Fasten the motors to the frame mount.

15. Make sure the coupling is pressed together well, and fasten the screws of the coupling through the hole in the frame mount.

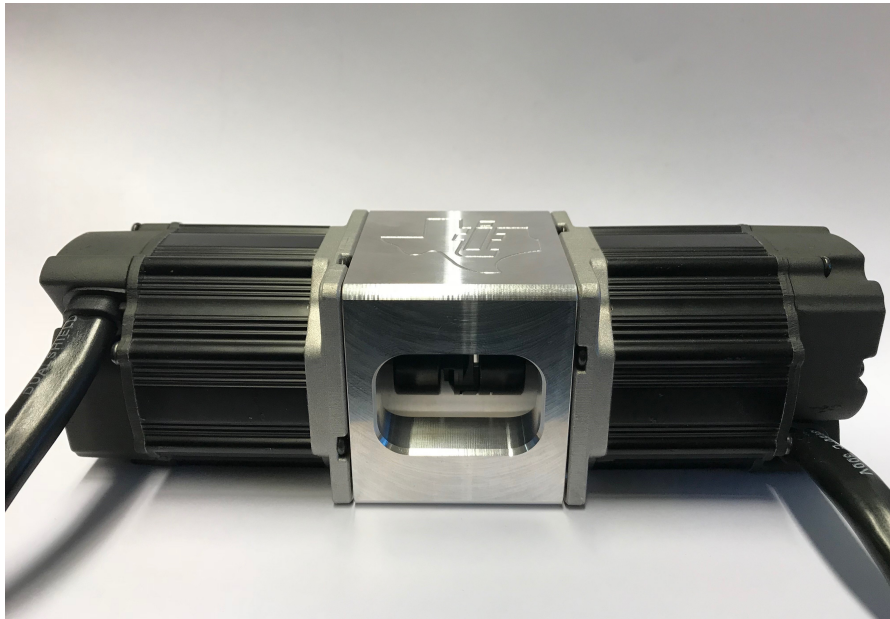


Figure A.47: The motors connected.

## A.5. Getting started

### A.5.1. Checking the drivers

After all the software is installed and the hardware is set up, we can take a look at actually programming the LaunchPad. To make sure it works, check the drivers:

1. Make sure everything is connected and the DC power supply is on.
2. Click the settings icon in the Start menu.
3. Go to Devices.
4. If the drivers are correctly installed, a device will be shown under "Other Devices"

#### Other devices



Texas Instruments Inc.XDS100 Ver 2.0

Figure A.48: If this device shows up the driver has been installed correctly.

5. If this device doesn't show up, something has probably gone wrong during the installation of Code Composer Studio. Try re-installing (appendix A.3.1).

### A.5.2. Starting with MotorWare™

This section will show where to find the lab manual in MotorWare™, as this can be quite difficult when there is no prior experience with it.

1. Run Code Composer Studio (In the Start menu it's in the "motorware" folder).
2. A security warning will pop up. Click "Yes".

3. The MotorWare™ home screen will show.

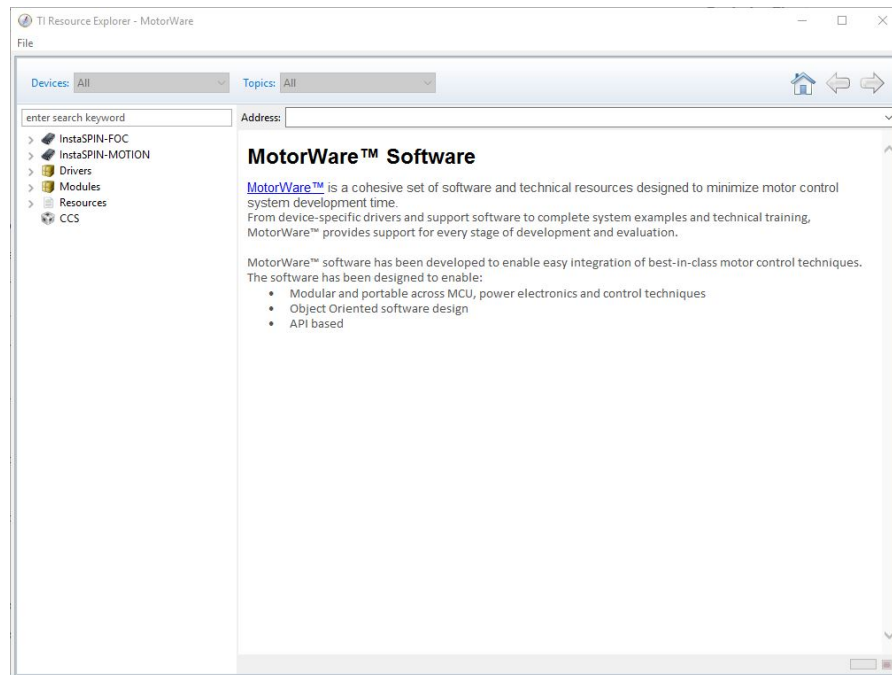


Figure A.49: The MotorWare™ home screen

4. The manual explaining the InstaSPIN™ labs can be found under "Resources" -> "Training: User's Guide, Labs, Tutorials" -> "InstaSPIN Projects and Labs User's Guide".

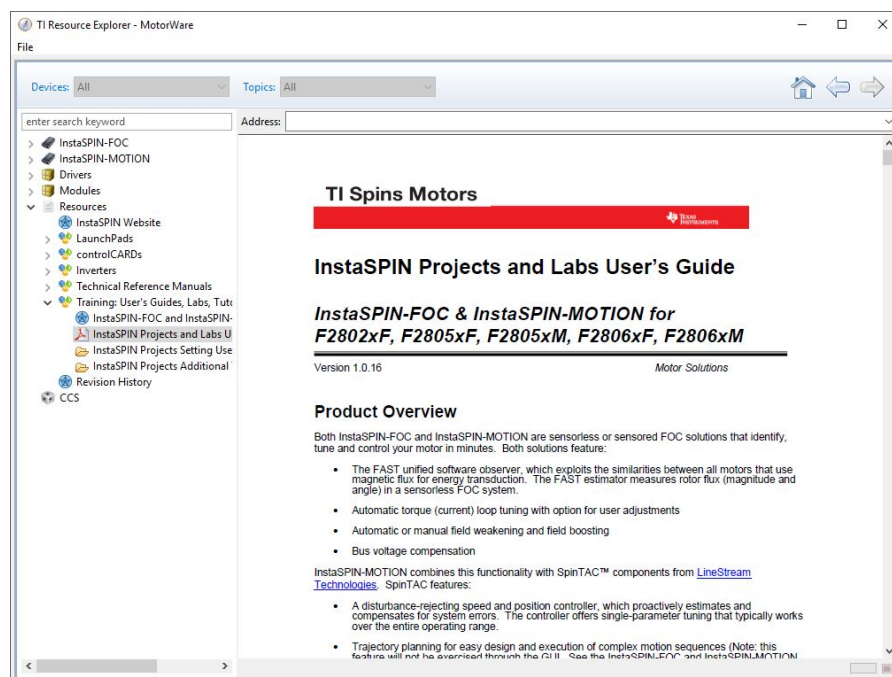


Figure A.50: Here the lab manual for InstaSPIN™ can be found.

### A.5.3. Starting with Code Composer Studio

Now we can start using Code Composer Studio to program our MCU and control the motor.

1. Run Code Composer Studio (In the Start menu it's in the "Texas Instruments" folder).

2. A window will appear asking for the workspace directory.

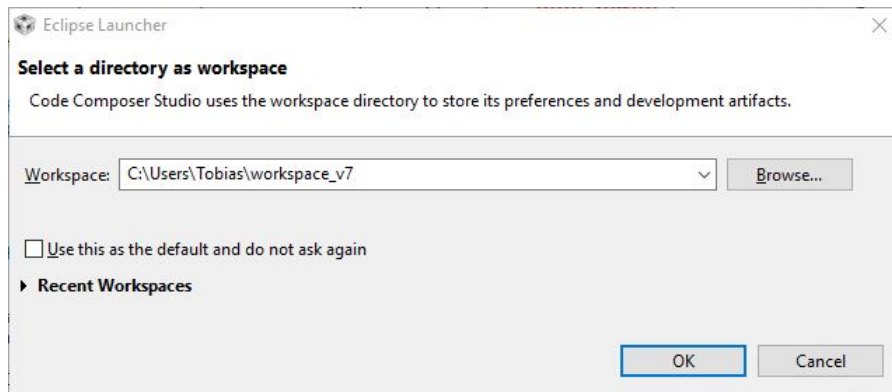


Figure A.51: This window shows after you run Code Composer Studio.

3. Change the directory to the main MotorWare™ direction (if you followed the instructions from appendix A.3 the direction will be C:\ti\motorware\motorware\_[version]). Then click "OK".

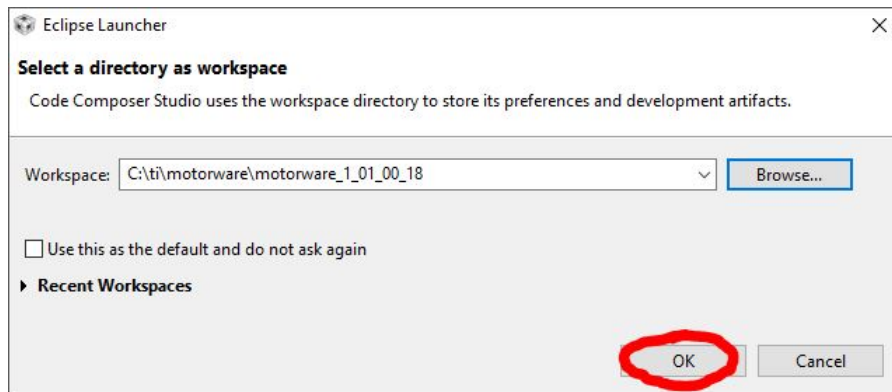


Figure A.52: Change the directory and click "OK".

4. The home screen of Code Composer Studio will show. Here there are several quick start options, such as introduction videos and a link to the wiki.

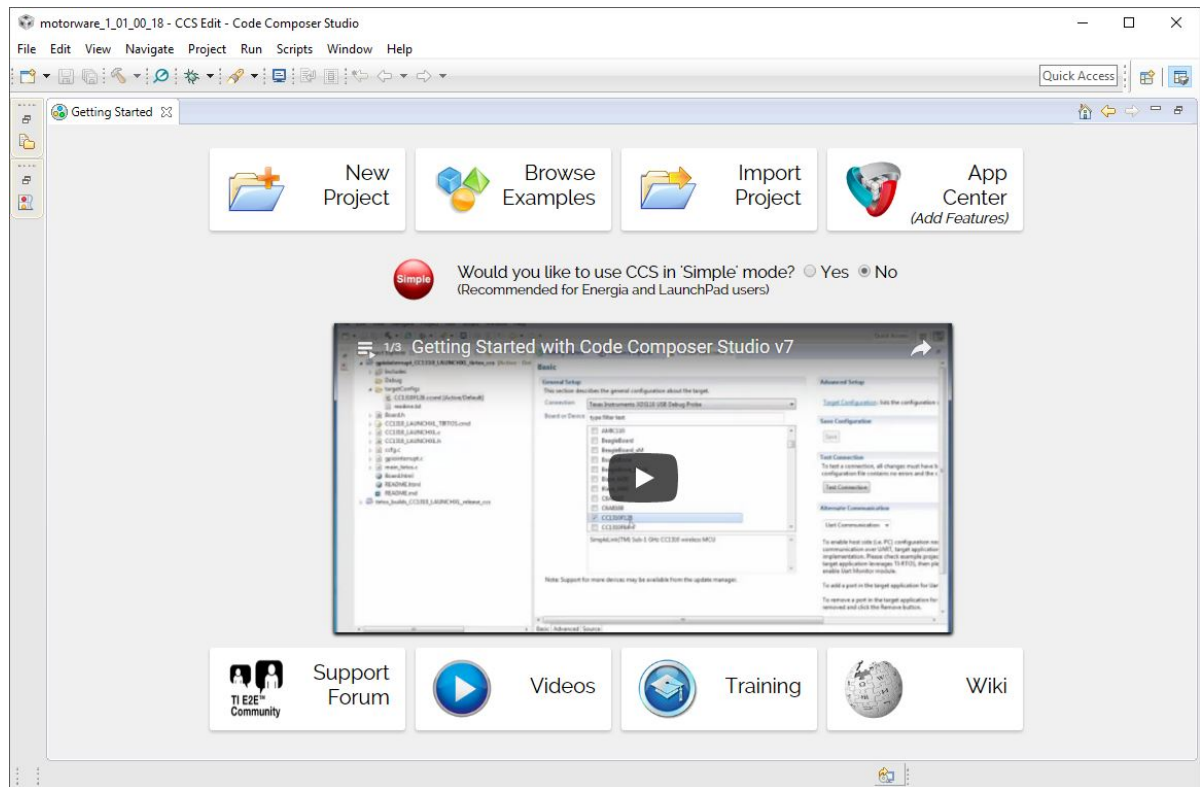


Figure A.53: The screen Code Composer Studio shows when you first run it.

5. To get started on the InstaSPIN labs, click on "Import CCS projects..." in the Project menu.

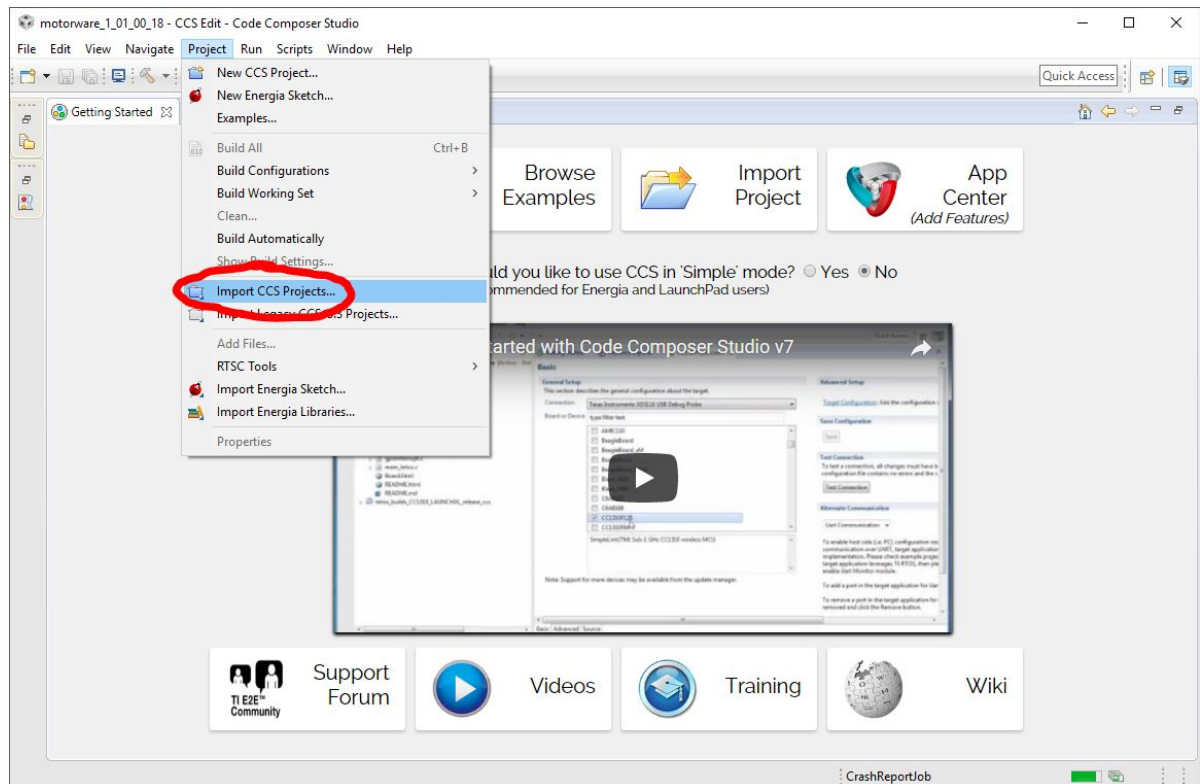


Figure A.54: Click Import CCS projects... in the Project menu.

6. In the window that pops up, click browse.

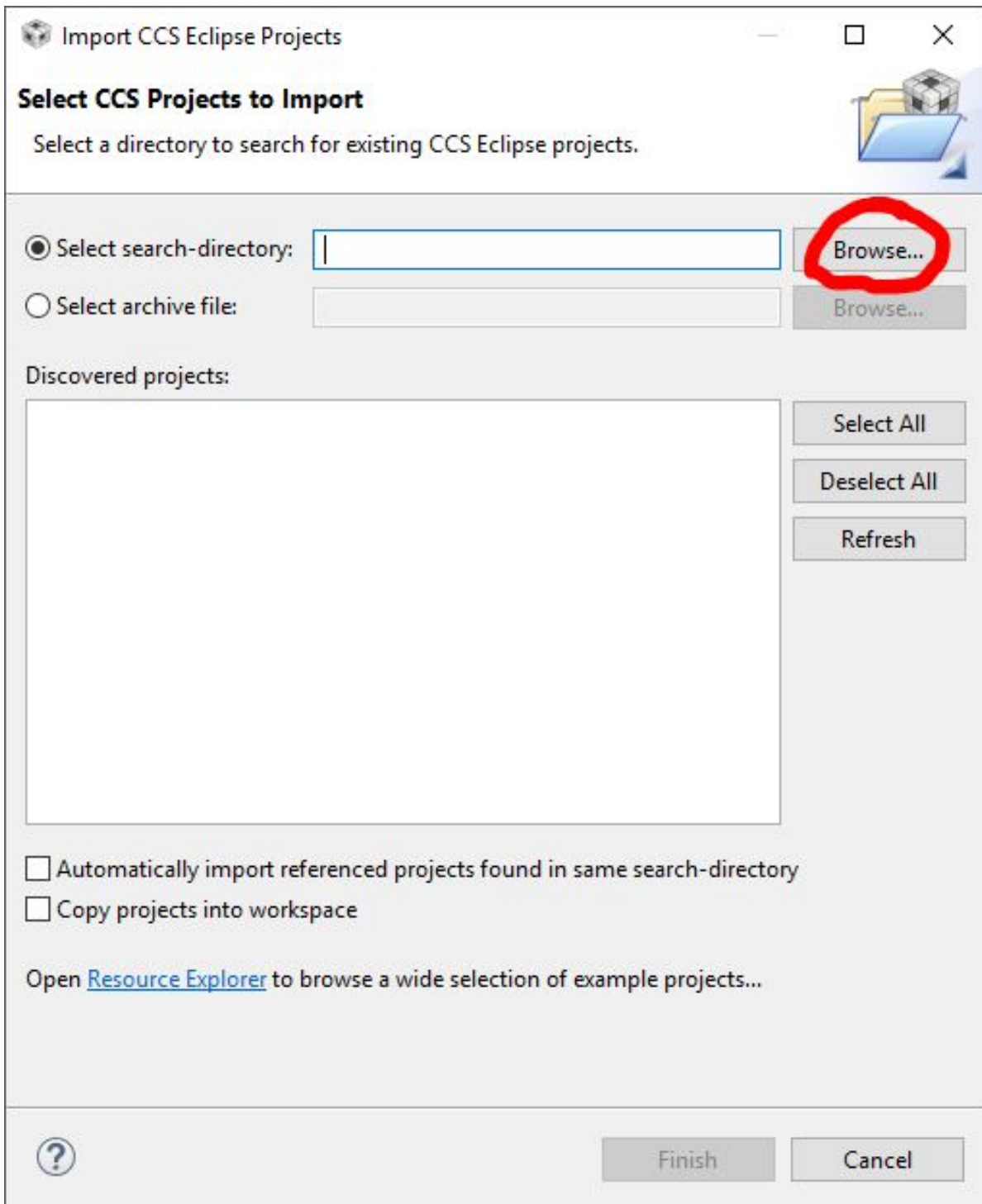


Figure A.55: Browse for a search-directory

7. The location for the labs is `C:\ti\motorware\motorware_[version]\sw\solution\instaspin_foc\boards\boostldrv8301_revB\28x\2806xF\project\ccs`. Select it and click "OK".

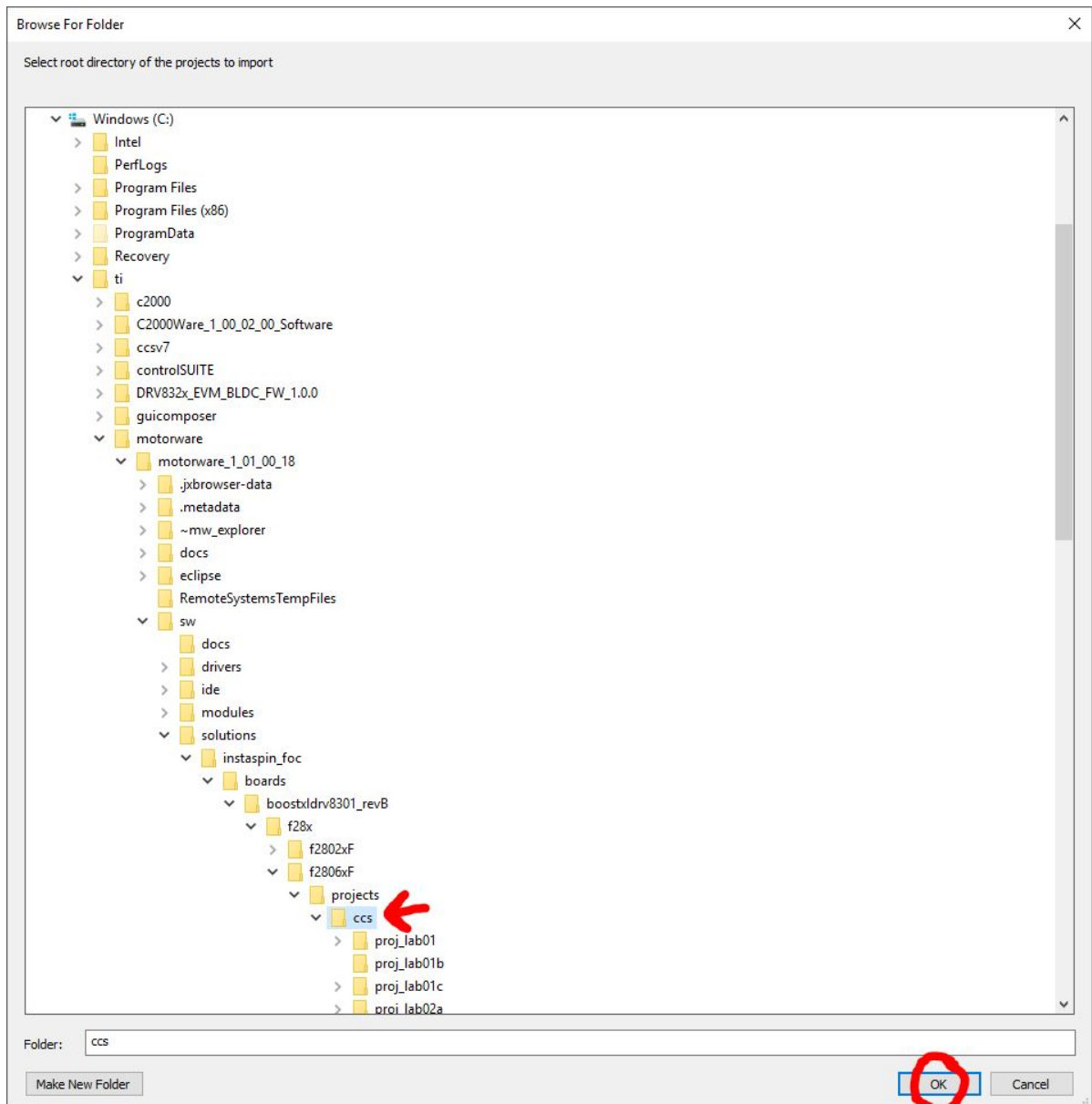


Figure A.56: Find the ccs folder, select it and click "OK"

8. The projects will show up in the previous window. Click "Select All".



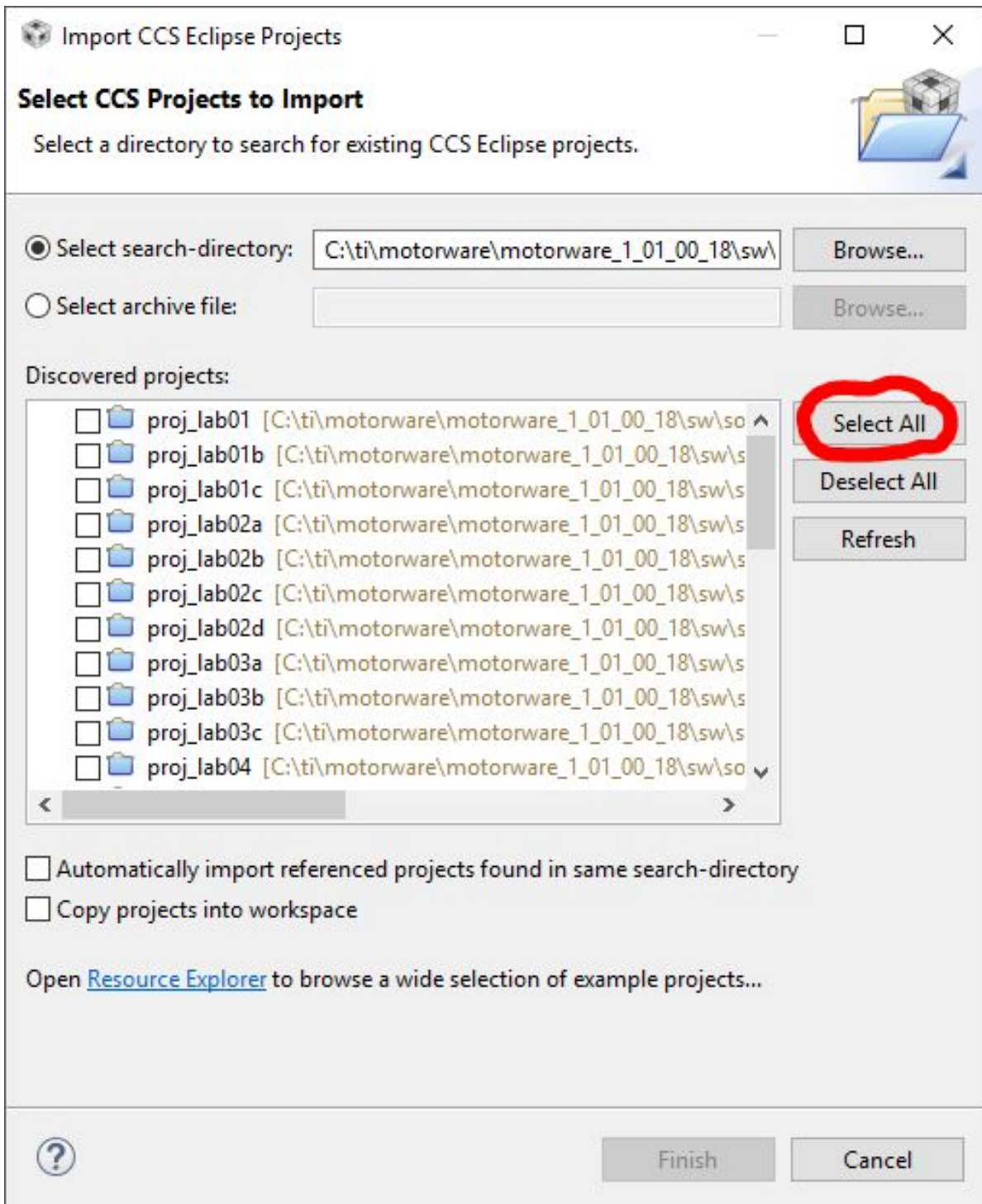


Figure A.57: The projects are found. Click "Select All".

9. Click "Finish" to load the projects into Code Composer Studio. Make sure "Copy projects into workspace" is NOT selected.

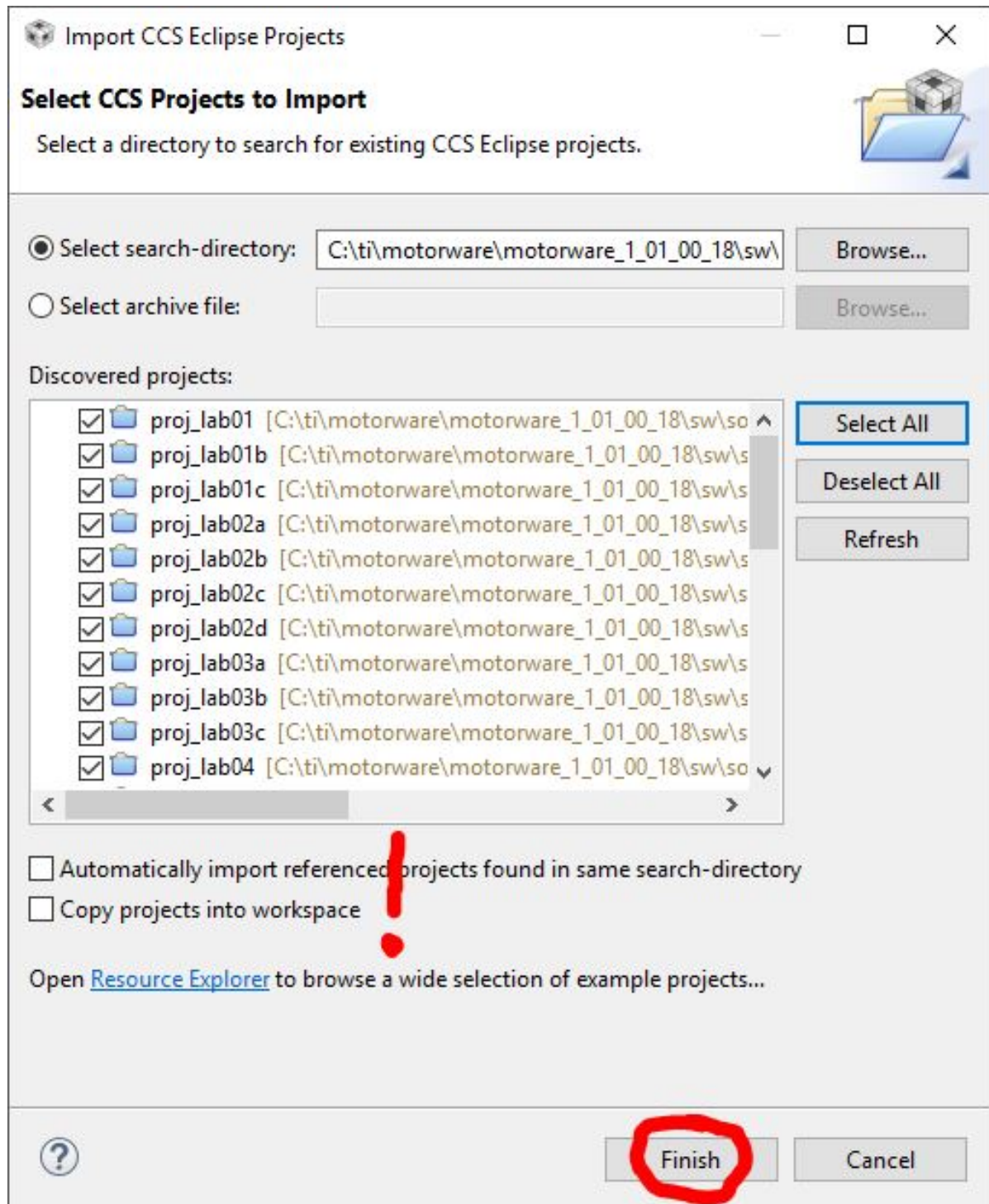


Figure A.58: Click "Finish" to load the projects into Code Composer Studio.

10. All the projects will be loaded, and the home window will look like this.

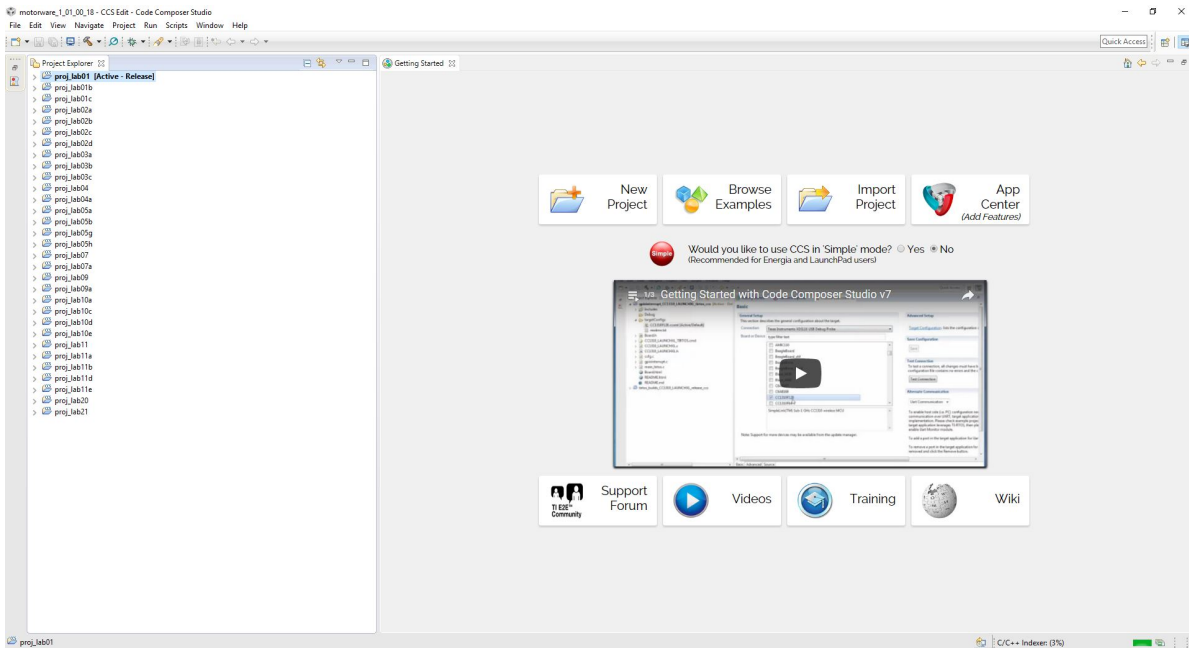


Figure A.59: The CCS home window with all the projects from the InstaSPIN labs loaded.

**At this point the InstaSPIN manual found in step A.5.2 ([14]) can be followed to go through all the labs. If you are only interested in using the simulation set-up as quick as possible, keep following this manual. If anything is still unclear about any of the labs, check [14].**

## A.6. Using the InstaSPIN labs

### A.6.1. Using lab 2 for estimating motor parameters

1. Doubleclick on `proj\_lab02a`, then find the `user\_j1.h` file, located in `includes -> "C:\ti\motorware\motorware_1_01_00_18\sw\solutions\instaspin_foc\boards\boostxldr8301_revB\28x\2806x\src"` and double click on that. This will open the file in a windows to the right.

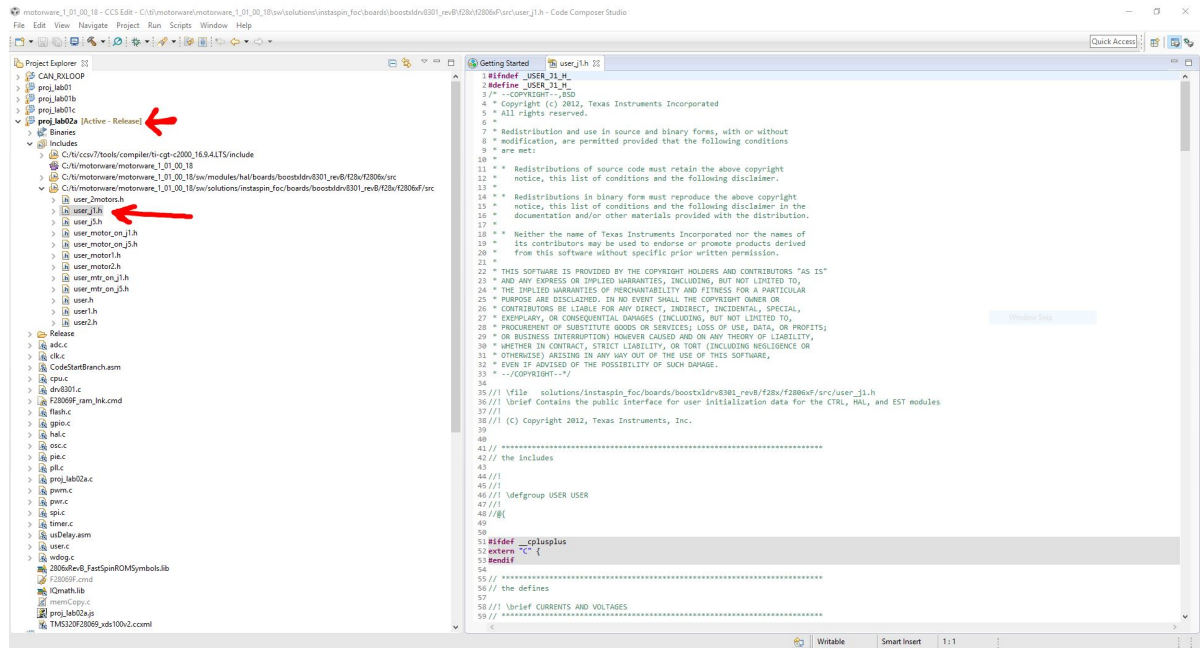


Figure A.60: Double click on proj\_lab2a and user\_j1.h

- Find the motor selection section (around line 219) and comment everything except `#define USER_MOTOR Teknic_M2310PLN04K`

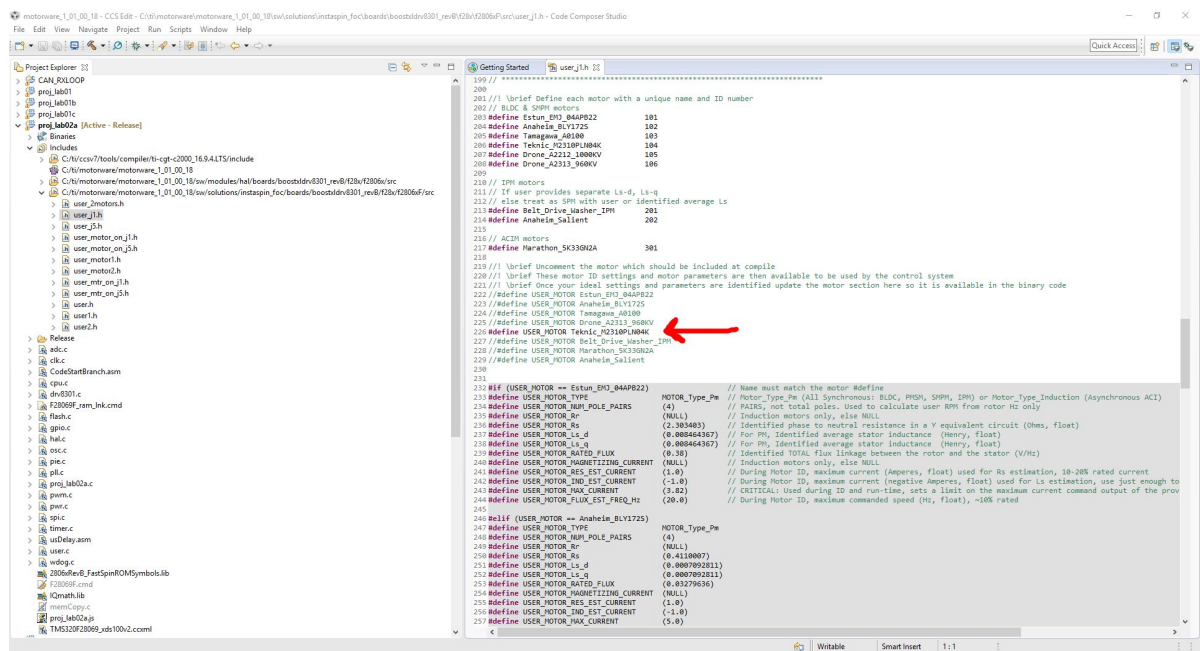


Figure A.61: Uncomment the Teknic motor and comment the other ones

- In the sections where the motors are defined, make sure the Teknic motor is defined as in fig. A.62.

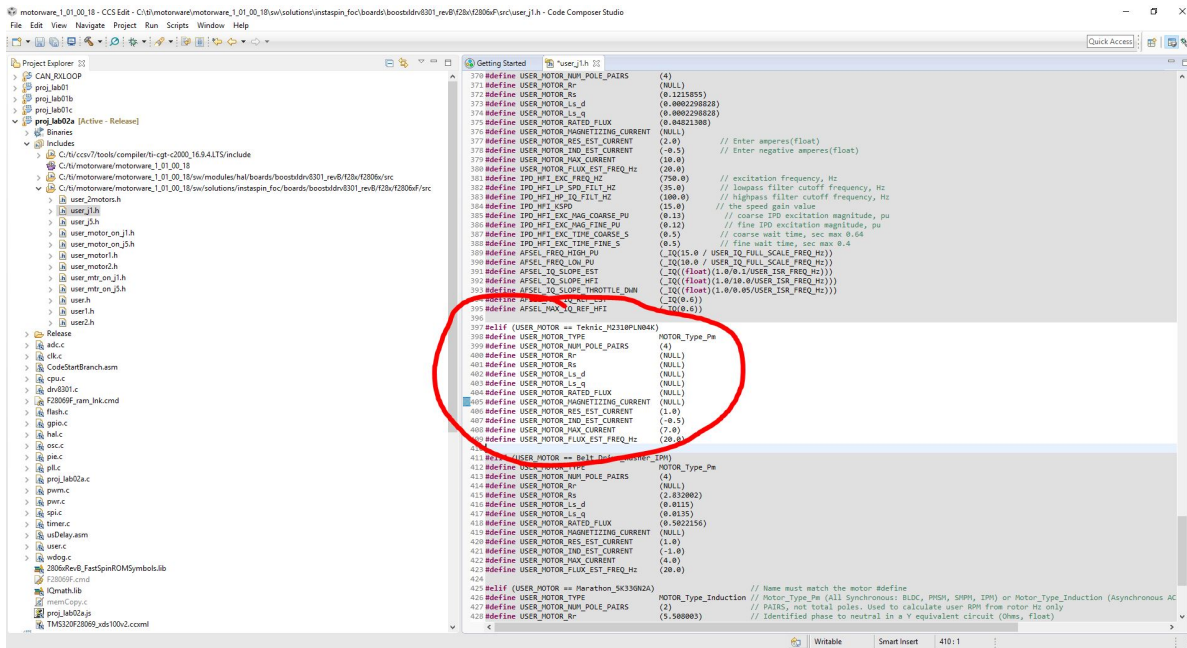


Figure A.62: Click "Finish" to load the projects into Code Composer Studio.

### 4. Open the Scripting Console from the view menu

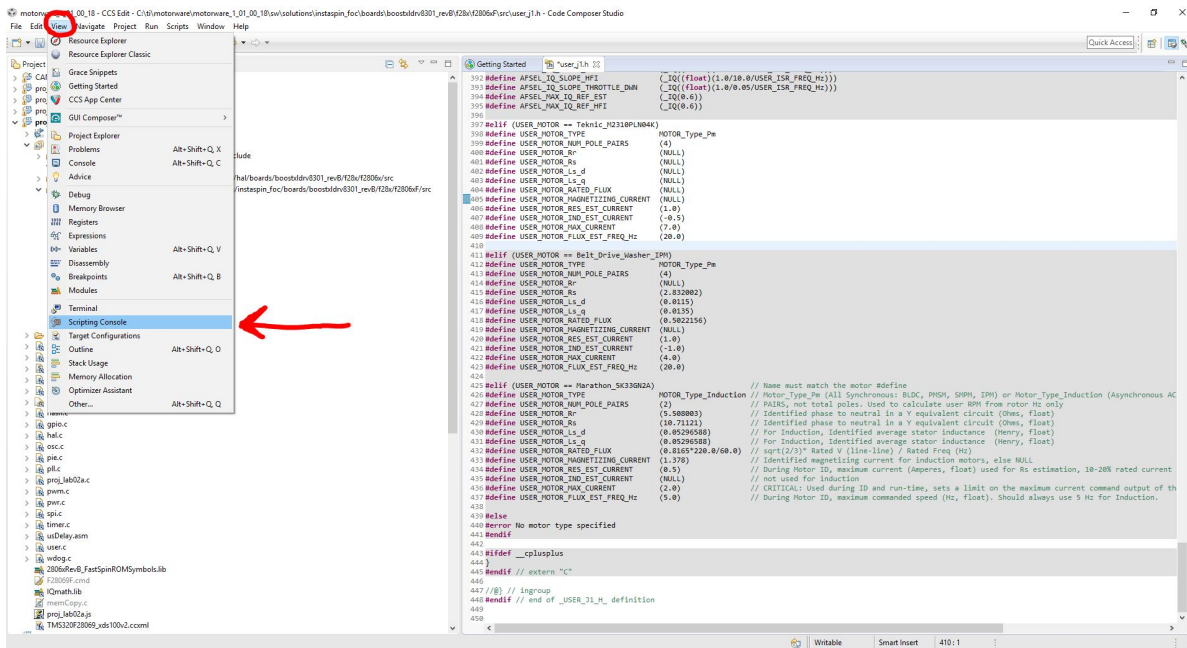


Figure A.63: Step 4

### 5. From the scripting console, click on the folder icon to open a file.

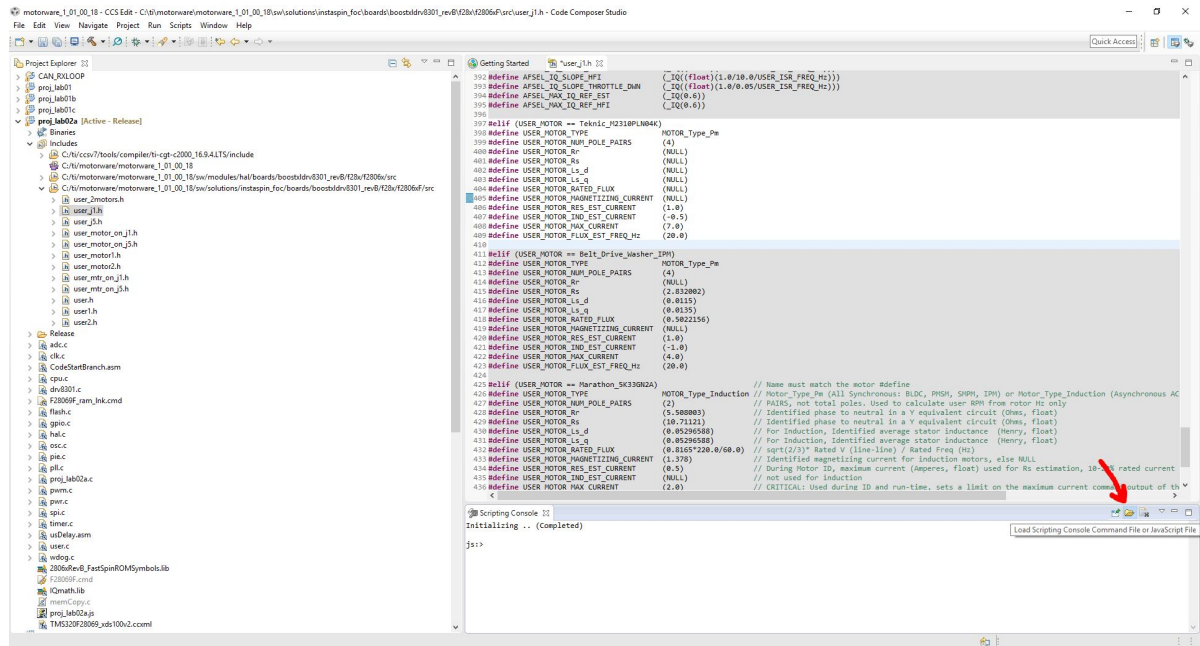


Figure A.64: Step 5

- Go to the file location `C:\ti\motorware\motorware_1_01_00_18\sw\solutions\instaspin_foc\src`

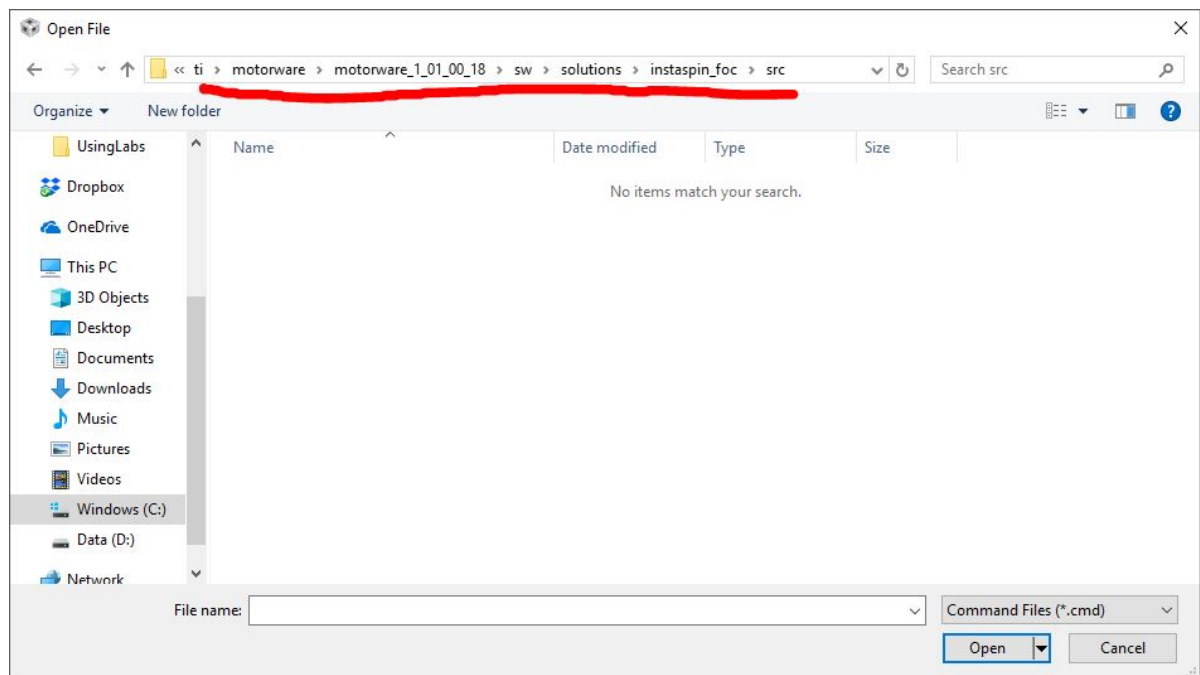


Figure A.65: Step 6

- Check for JavaScript files, and open `proj_lab02a`.

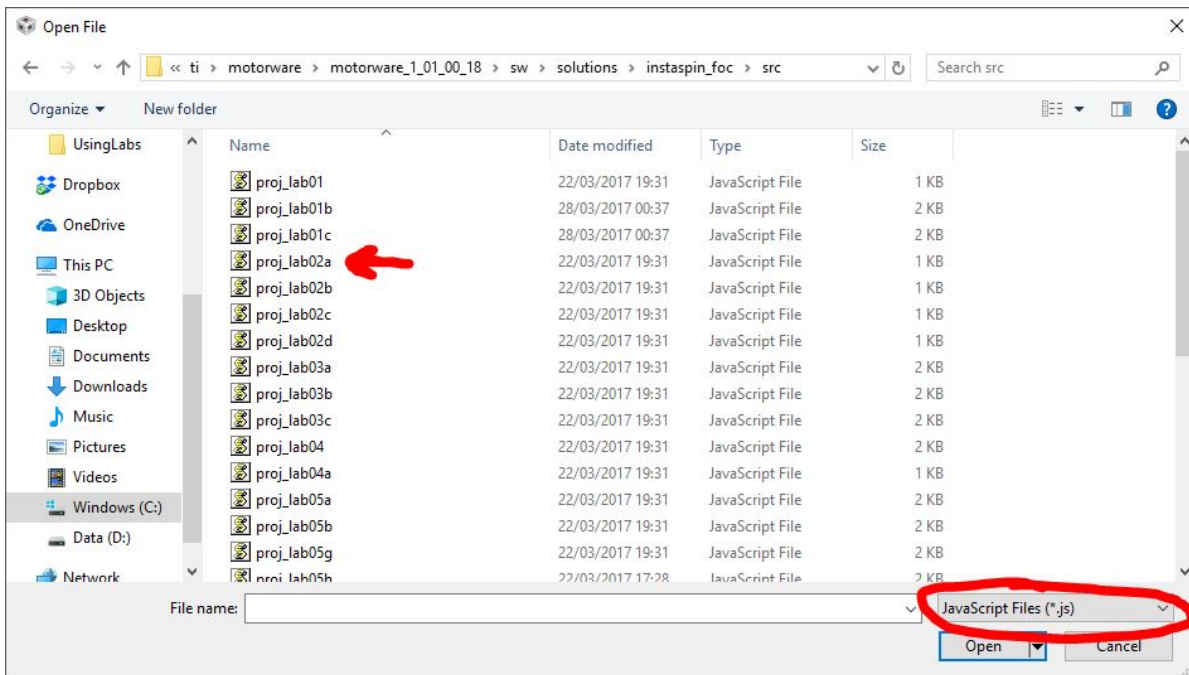


Figure A.66: Step 7

8. The watch window will open in the top right. Here you will be able to monitor and change values while running the motor.

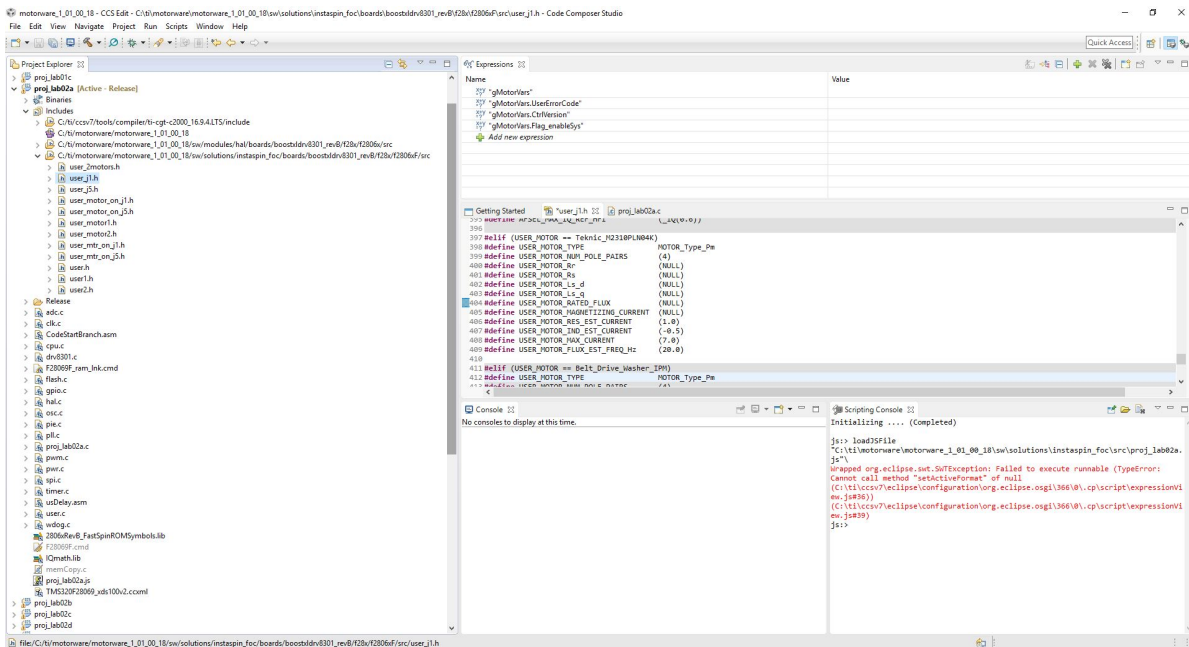


Figure A.67: Step 8

9. Click the debug button

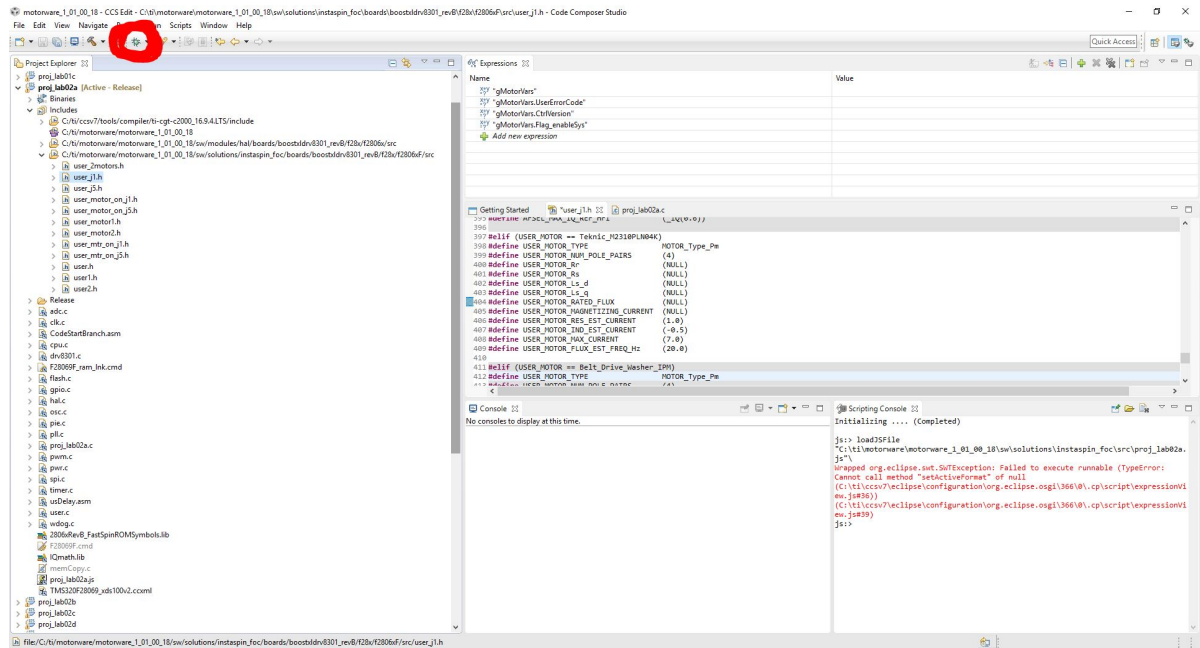


Figure A.68: The debug button is located in the top to the left

10. Enable real time (1), run the program (2) and allow continuous refresh in the watch window (3). Expand the gMotorVars folder in the watch window.

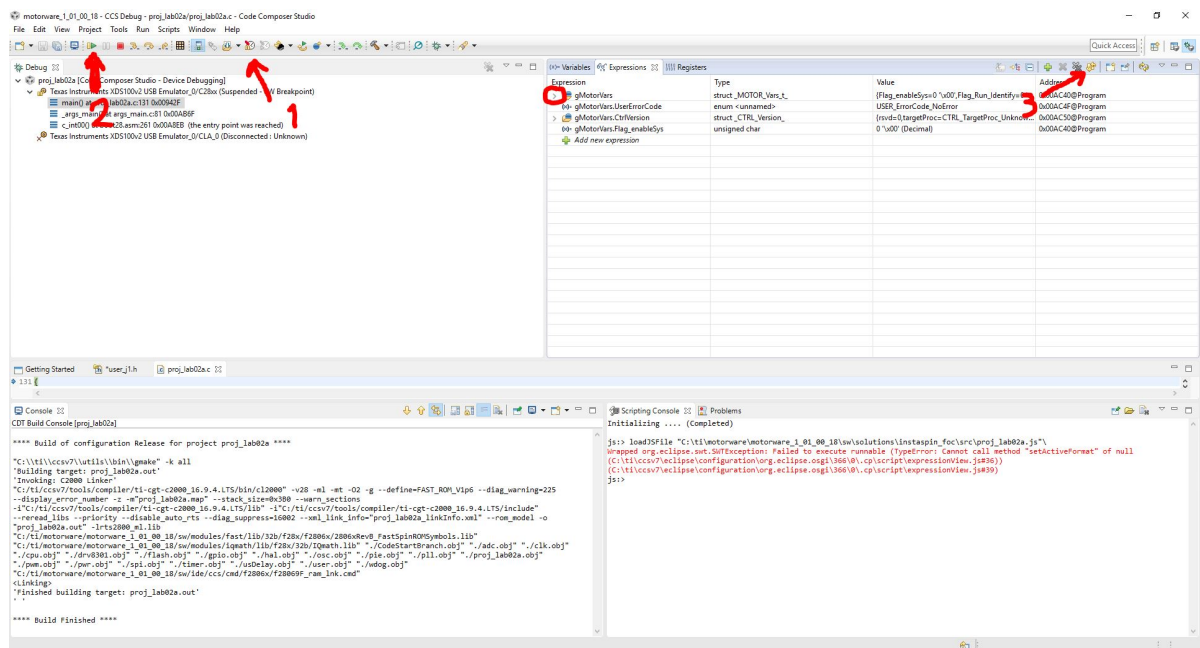


Figure A.69: Step 10

11. Check if the value show what you expect. For example, SpeedRef\_krpm should show a decimal number. Right-click the value and change the Q-value to 24.



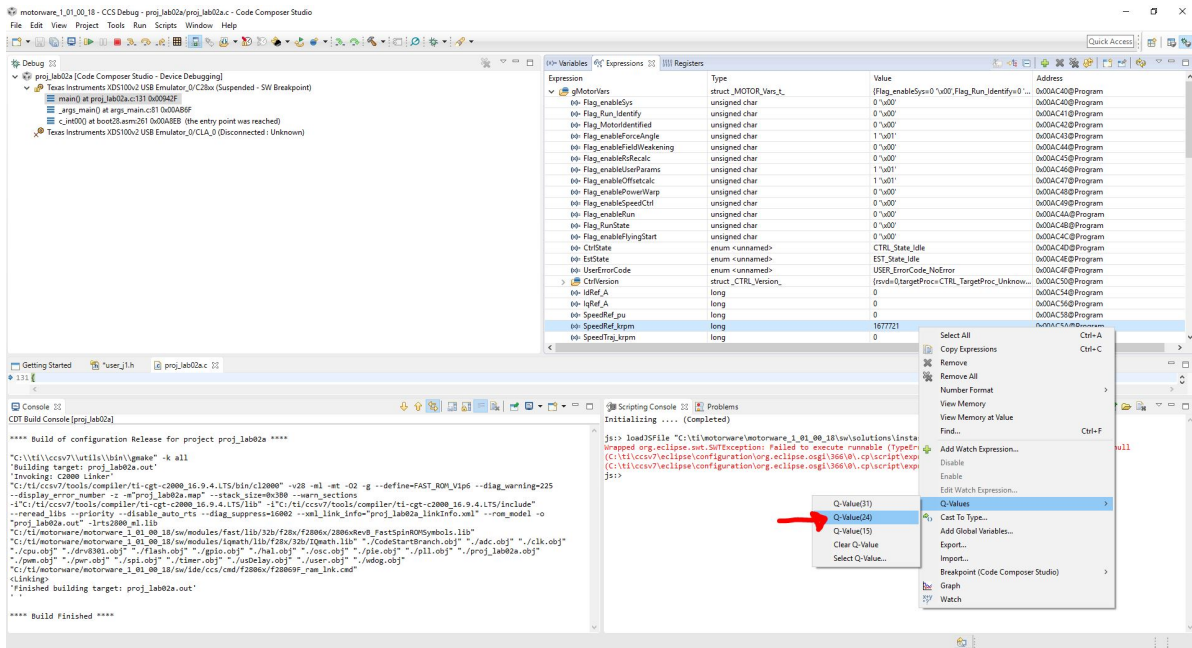


Figure A.70: Step 11

12. First set Flag\_enableSys to 1, then set Flag\_Run\_Identify to 1. This will run the motor identification. After the identification is done, the motor will start spinning normally.

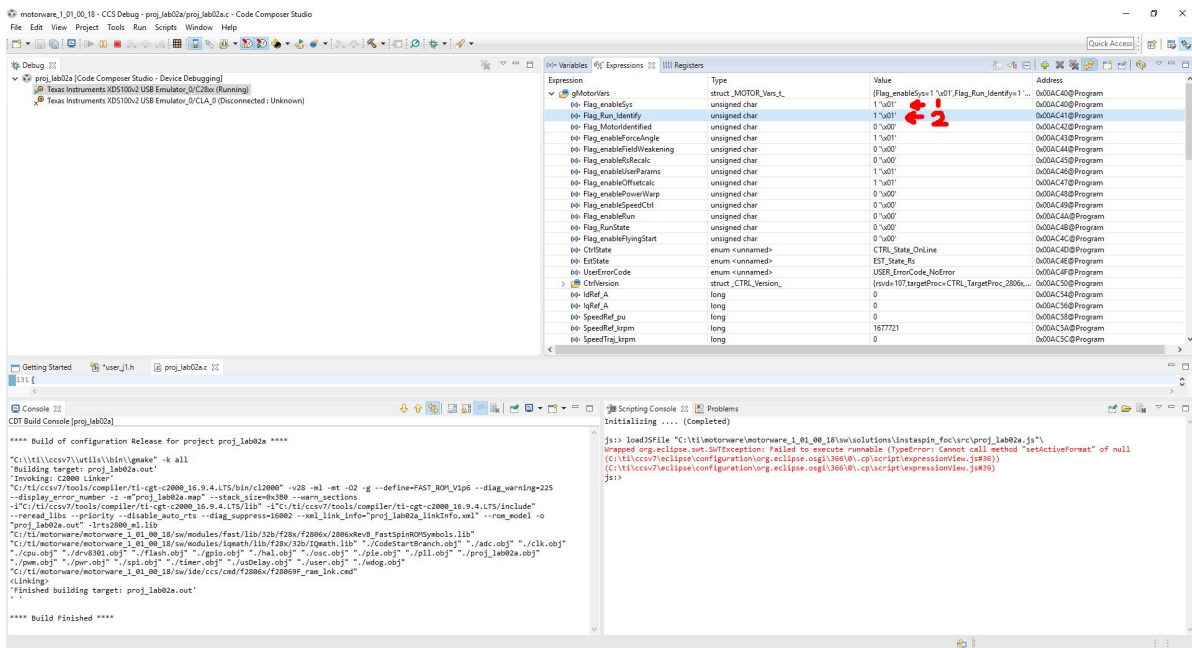


Figure A.71: Step 12

13. After the motor identification is done, copy the following values in the watch window to the user\_j1.h file: Rs, Ls\_d, Ls\_q and Flux\_VpHz (the last one in RATED\_FLUX).

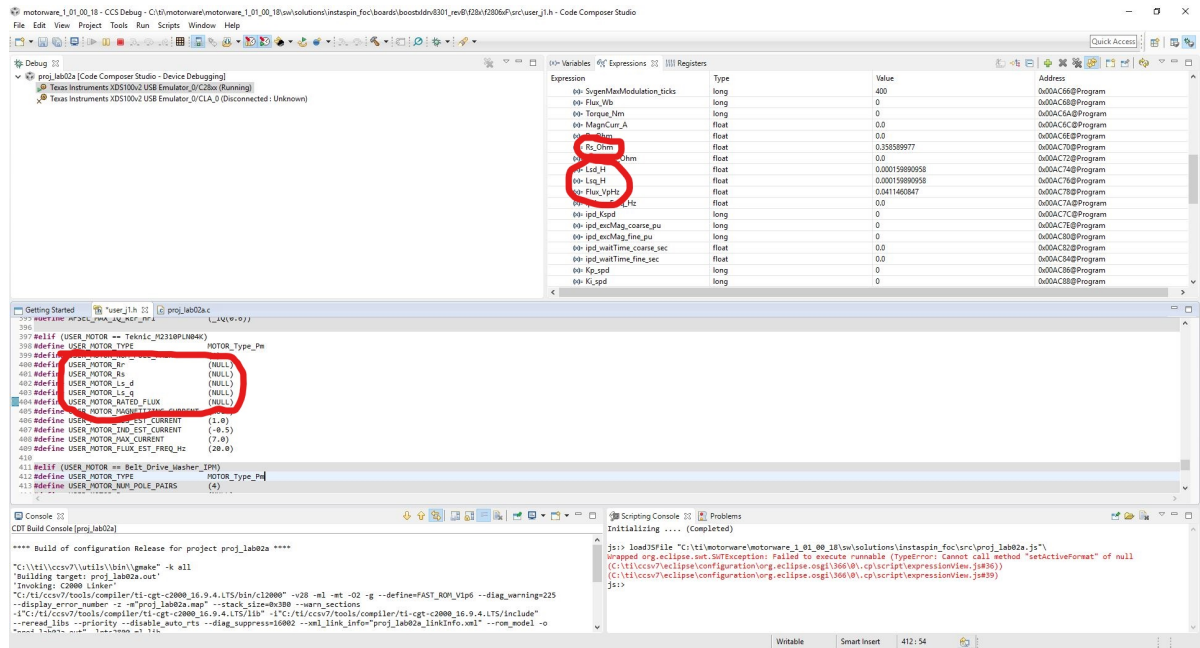


Figure A.72: Step 13

- When the motor identification is done and the values are copied to `user\_j1.h` the program can be stopped and the next part of this manual can be followed.

### A.6.2. Using lab 4 for the torque load

Running lab 4 works essentially the same as running lab 2, so only a few differences will be explained here. It is assumed the motor parameters determined lab 2a are stored in `user_j1.h`.

- Double click on `proj_lab04`. This will set lab 4 as the active project.

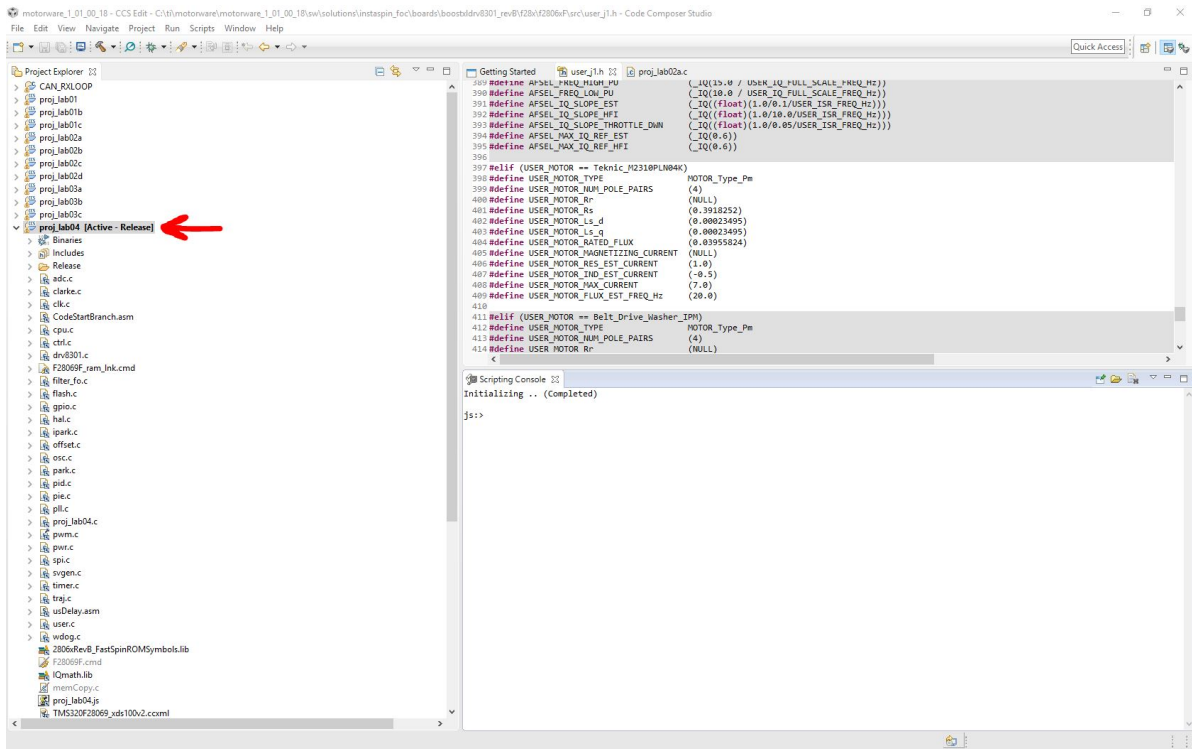


Figure A.73: Step 1

2. Open a different JavaScript file from the scripting console: proj\_lab04.

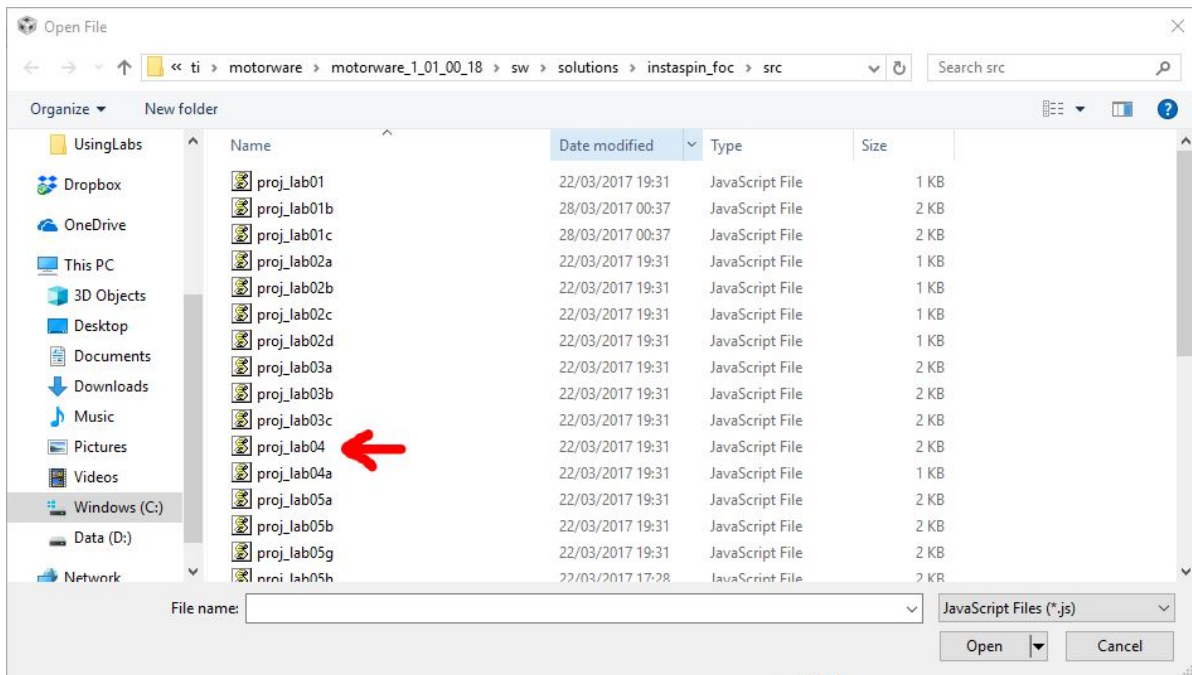


Figure A.74: Open a different config file.

3. The torque of the motor can be changed in the expressions window using IqRef\_A (make sure the variable is set to Q-value(24)).

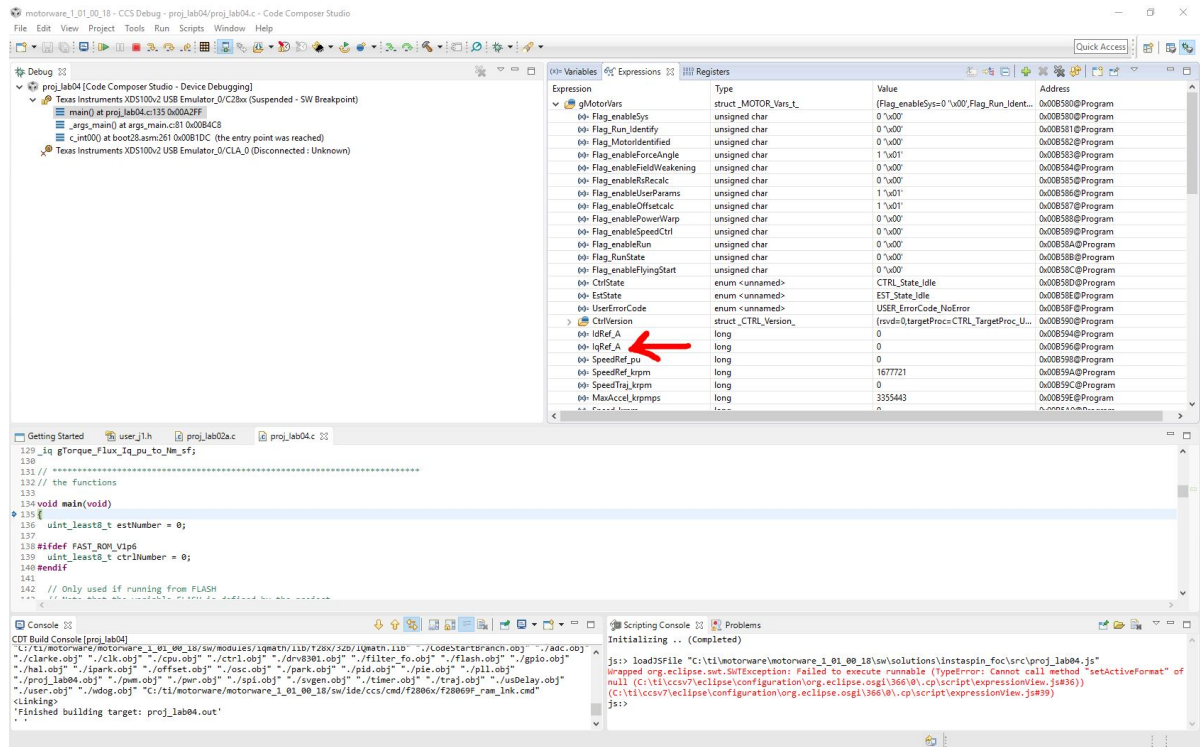


Figure A.75: Here the torque load can be changed.

4. Make sure the motor is identified and the values are stored in `user_j1.h`. If this is not the case, go back to appendix A.6.1.
5. When the motor is identified, right click on `Torque_Nm` in the expressions window and click on graph. This opens the graph window to see the torque.

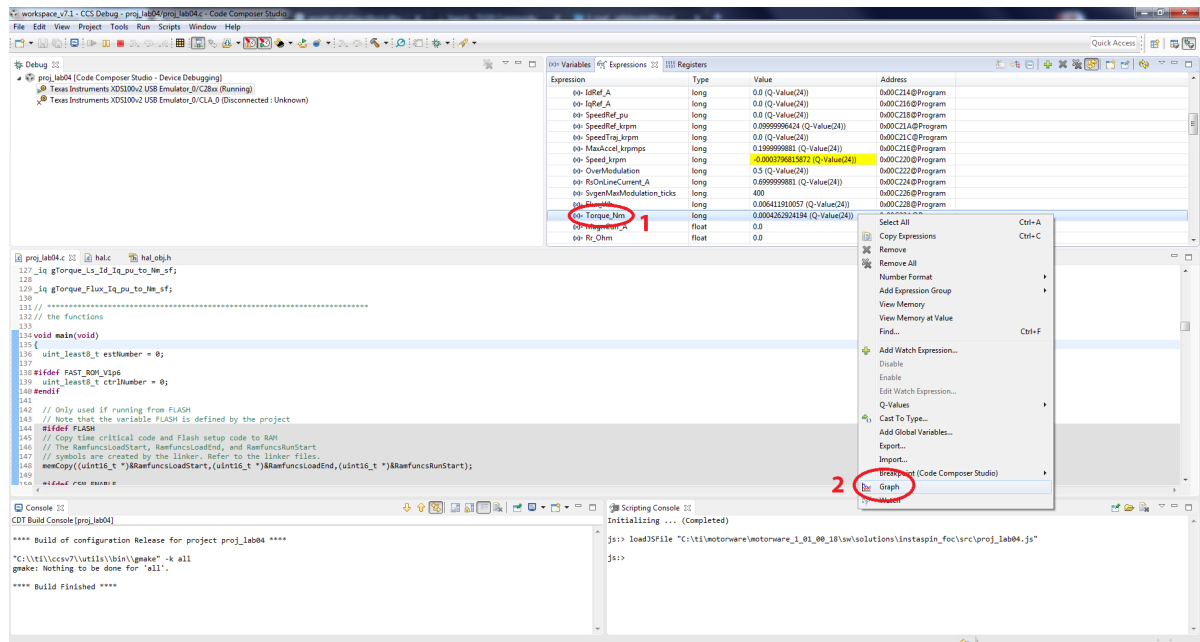


Figure A.76: Click here to show Torque\_Nm in a graph.

6. Enable continuous refreshing in the graph window.

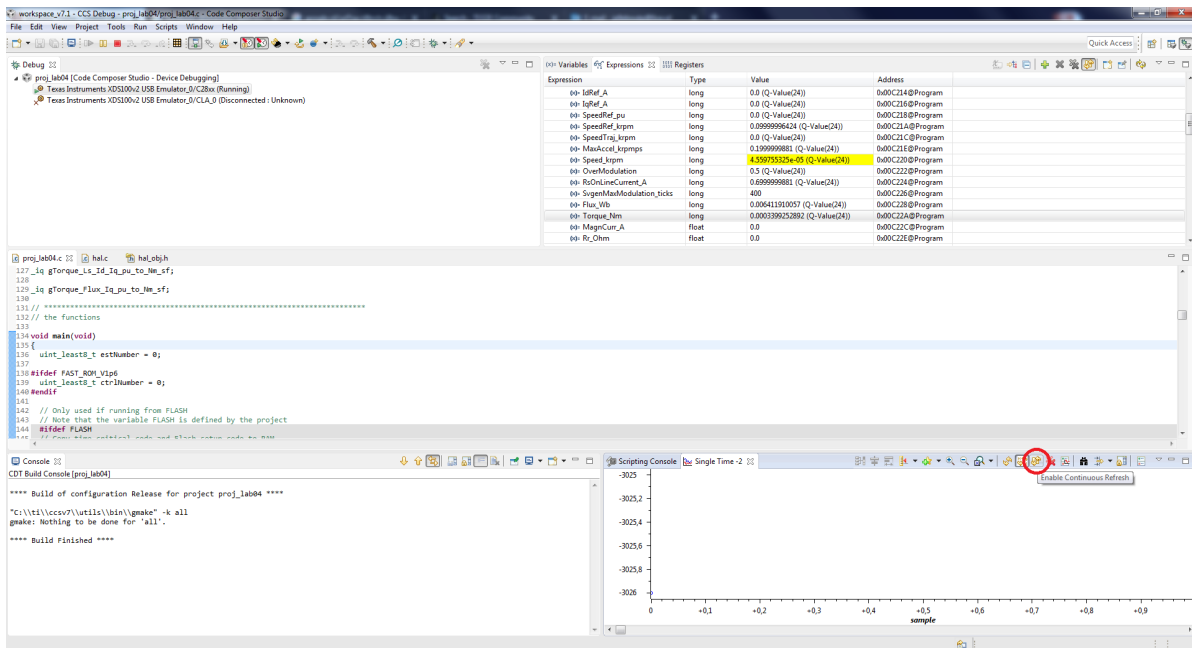


Figure A.77: Enable continuous refresh

7. When changing IqRef\_A (1) to a different value, the speed change can be seen (2), Torque\_Nm will change (3) and this change can be seen in the graph window (4)

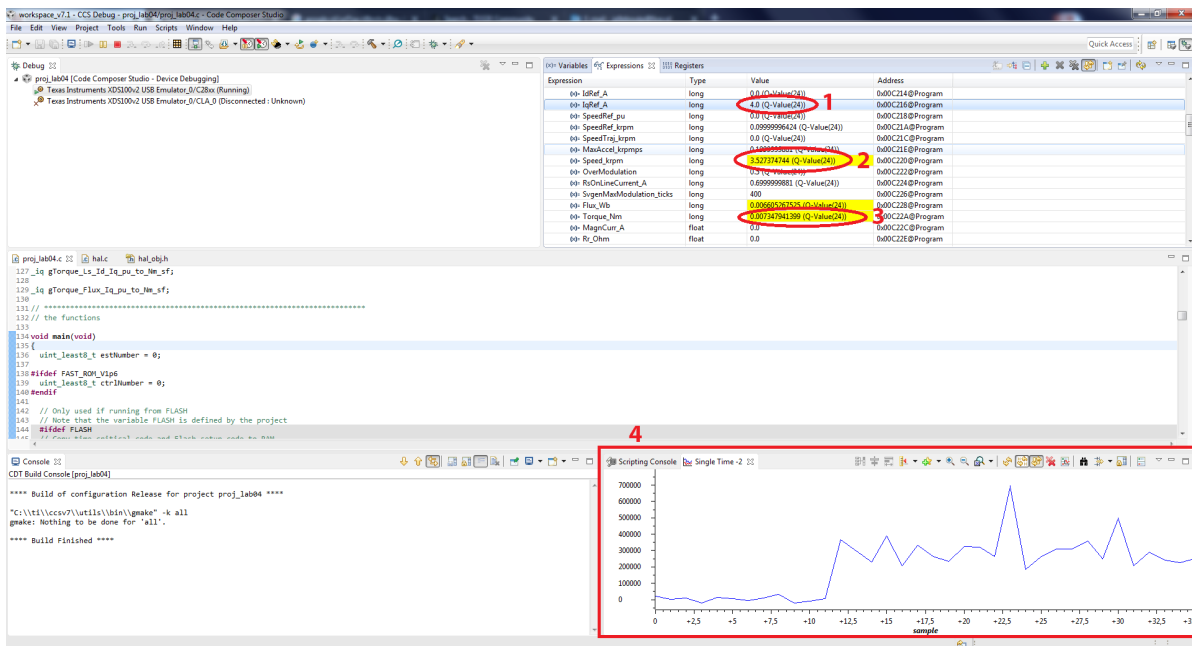


Figure A.78: Changing IqRef\_A (done here at sample +11) will influence the torque and speed of the motor. The change in torque is seen in the graph window.

8. Changing the IqRef\_A back to zero, the motor will stop spinning as the torque will also become zero again.

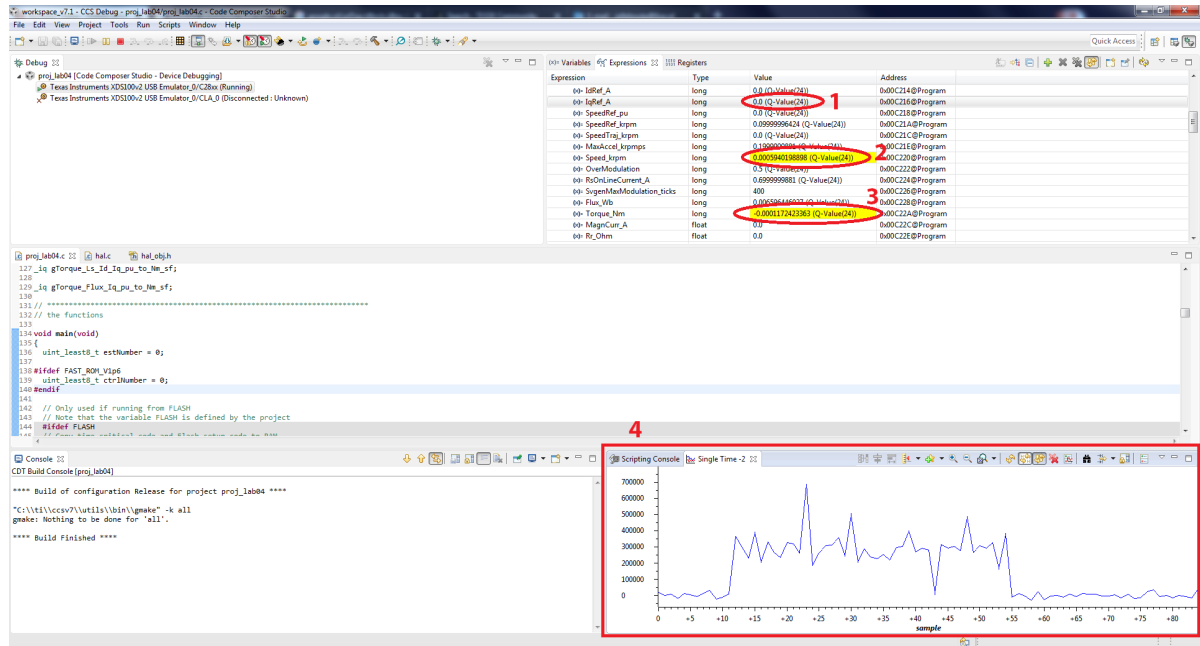


Figure A.79: IqRef\_A is set back to zero at sample +54

### A.6.3. Using lab 11a for the motor controller

1. Running lab 11a works the same as lab 2 and 4, with again selecting the appropriate project (proj\_lab11a) and the appropriate JavaScript file (proj\_11a.js).
2. Before running the motor, first set the enableOffsetCalc flag to 1. This will recalculate the voltage and current offsets for the measurements. After that is done, set the enableRsRecalc flag to one. This will update the stator resistance value for a more accurate control.

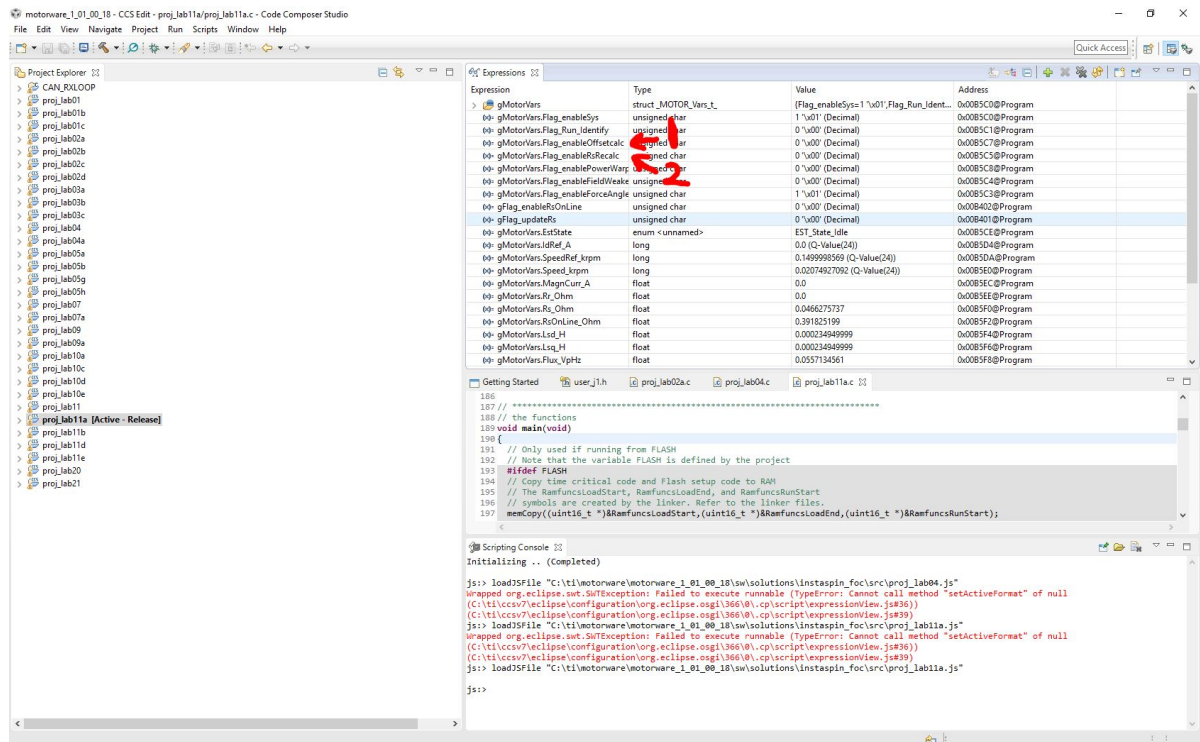


Figure A.80: Step 1

- While running the motor, the enableRsOnLine flag can be set to 1 to monitor the value of Rs. This is useful for calculating the temperature of the motor. With the updateRs flag, the most recent value of Rs will constantly be updated in the estimator, so the control will be more accurate.

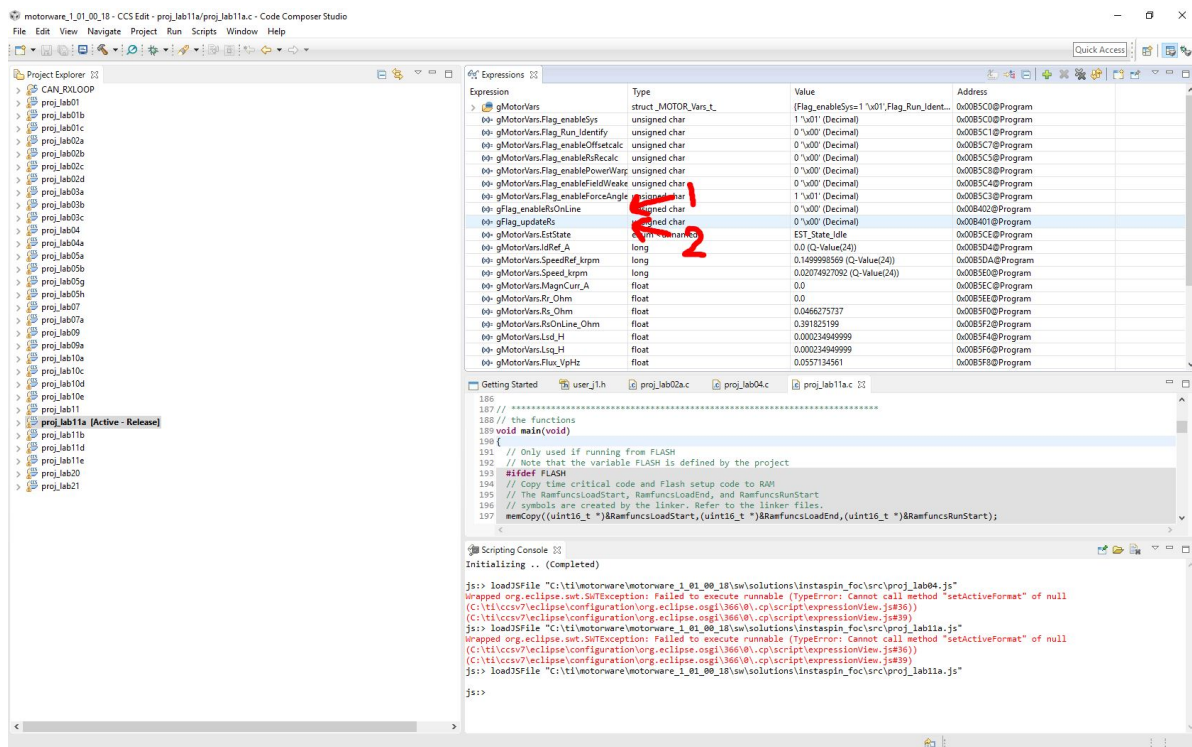


Figure A.81: Enable the online recalculation of the stator resistance.

- From the watch window, all PID controllers can also be tuned. The controllers are: the speed controller, the Iq controller and the Id controller. To tune the controllers change the Kp and Ki values. (for more information on tuning the controllers, see lab 5a and 5b in [14].

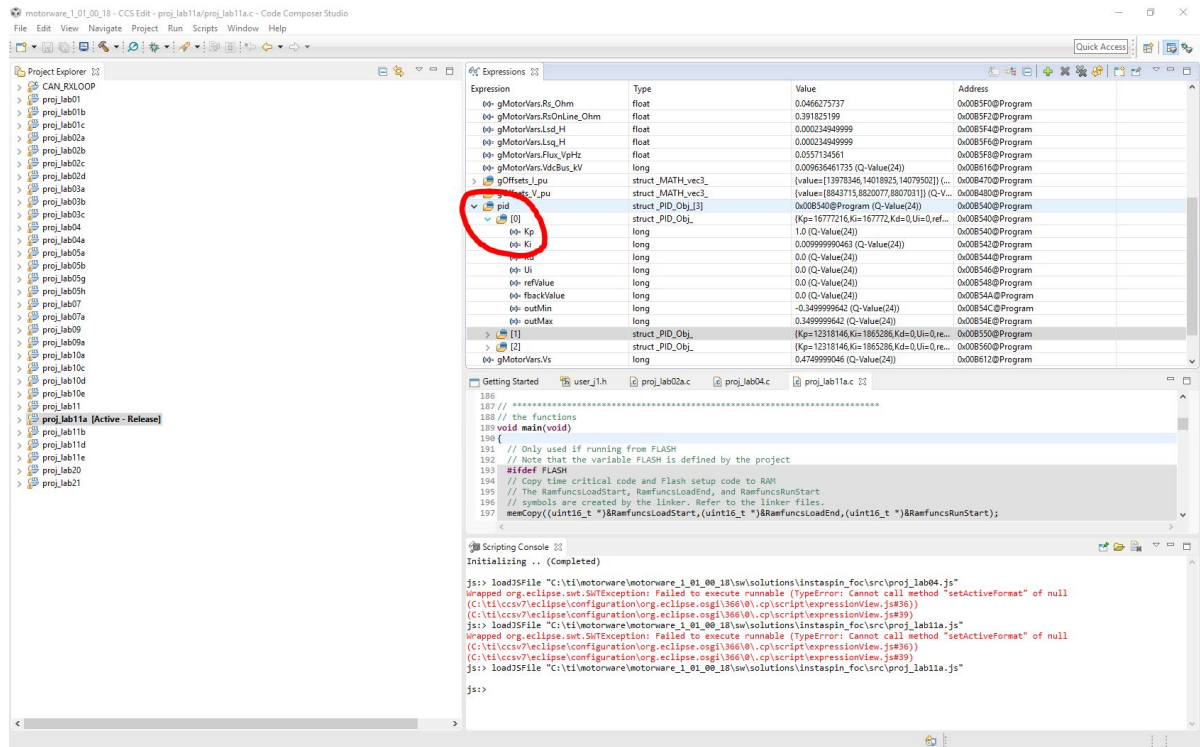


Figure A.82: The controllers can be independently tuned.

## 5. Field weakening can also be enabled in this lab. To do that, change the value of the enableFieldWeakening flag to 1 in the watch window.

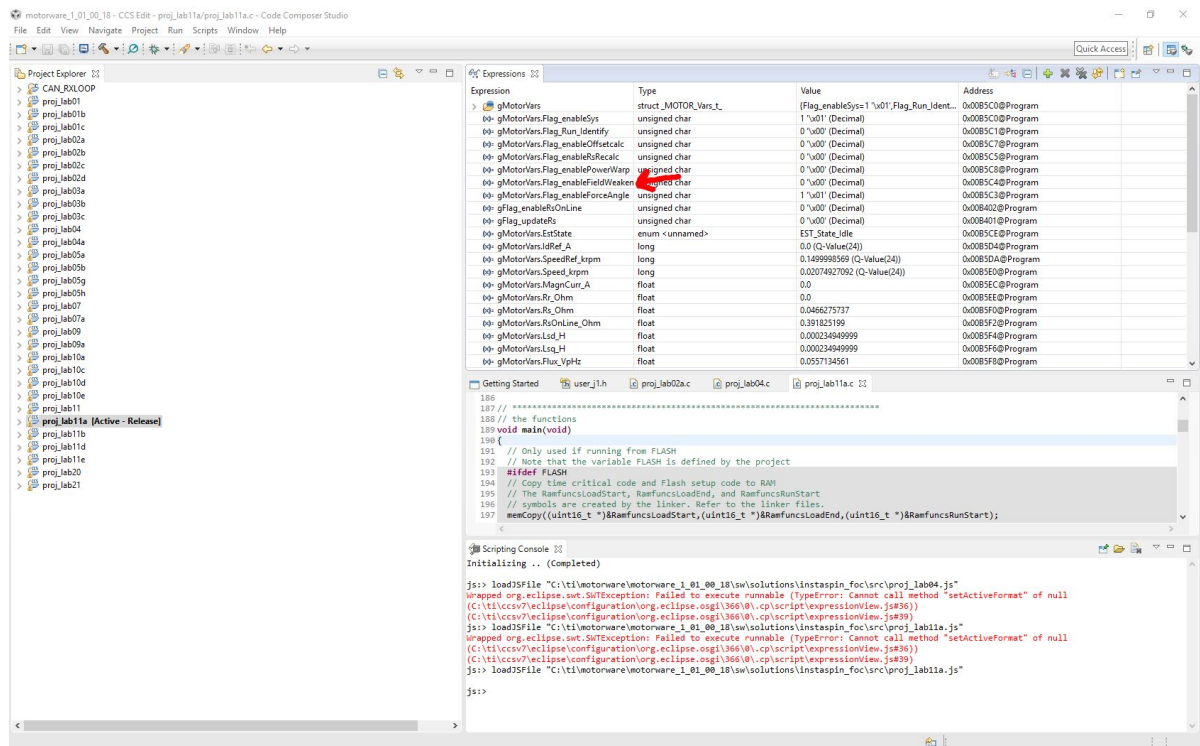


Figure A.83: Field weakening can be enabled by setting this flag to 1.

## 6. To open the graph to observe the actual speed of the motor. Right-click on the variable (in this



case: Speed\_krpm) and click on graph.

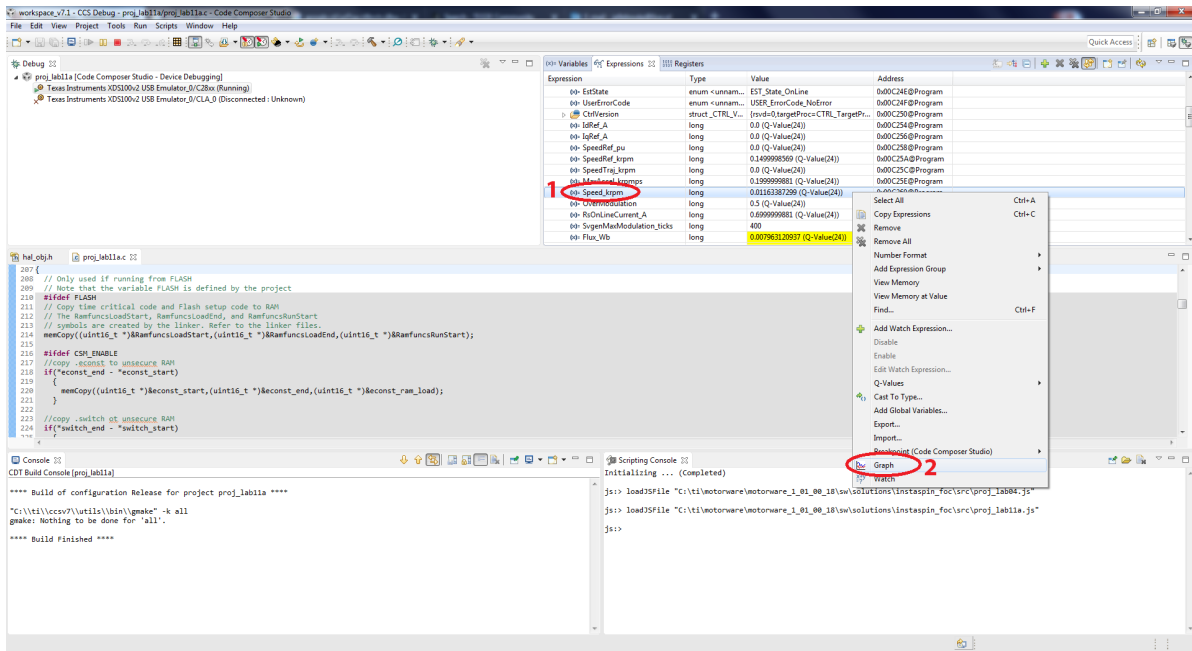


Figure A.84: To open the graph of the actual speed, right click on speed\_krpm and click on graph.

7. Enable the continuous refreshing, otherwise refreshing the graph needs to be done by hand.

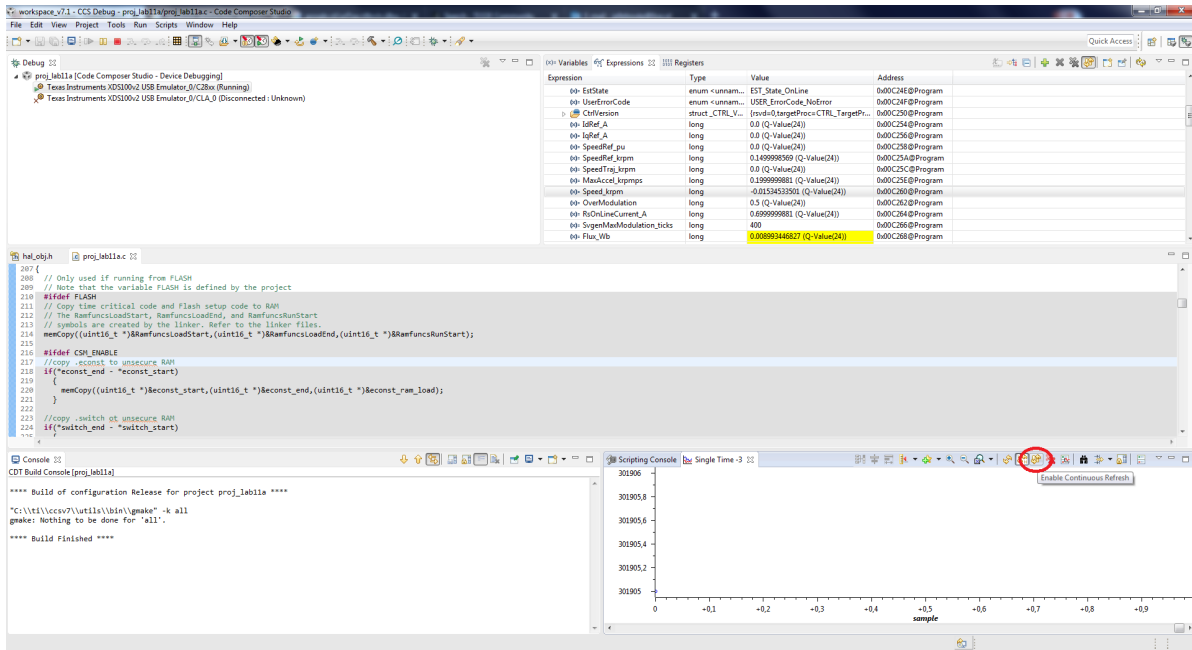


Figure A.85: Enable continuous refreshing.

8. While changing the reference speed at SpeedRef\_krpm. The actual speed will change by the maximum acceleration set. This can be observed in the graphs of fig. A.86 and fig. A.87.

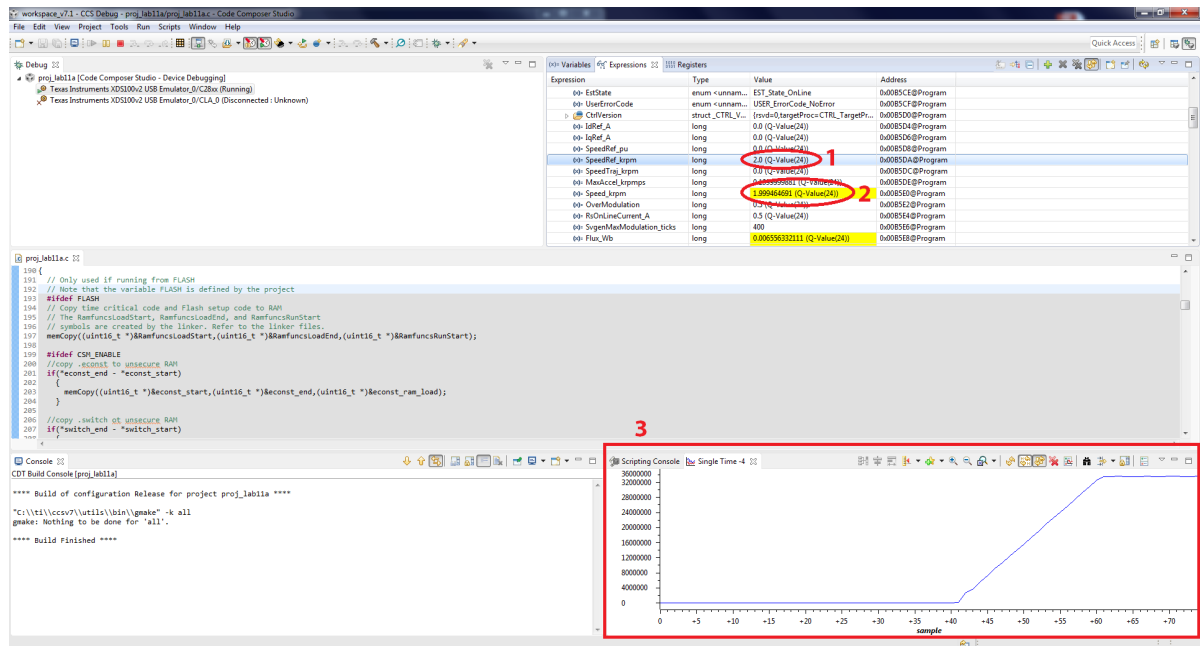


Figure A.86: 1. Change the speed, 2. The actual speed changes and 3. Graph shows how the speed changed.

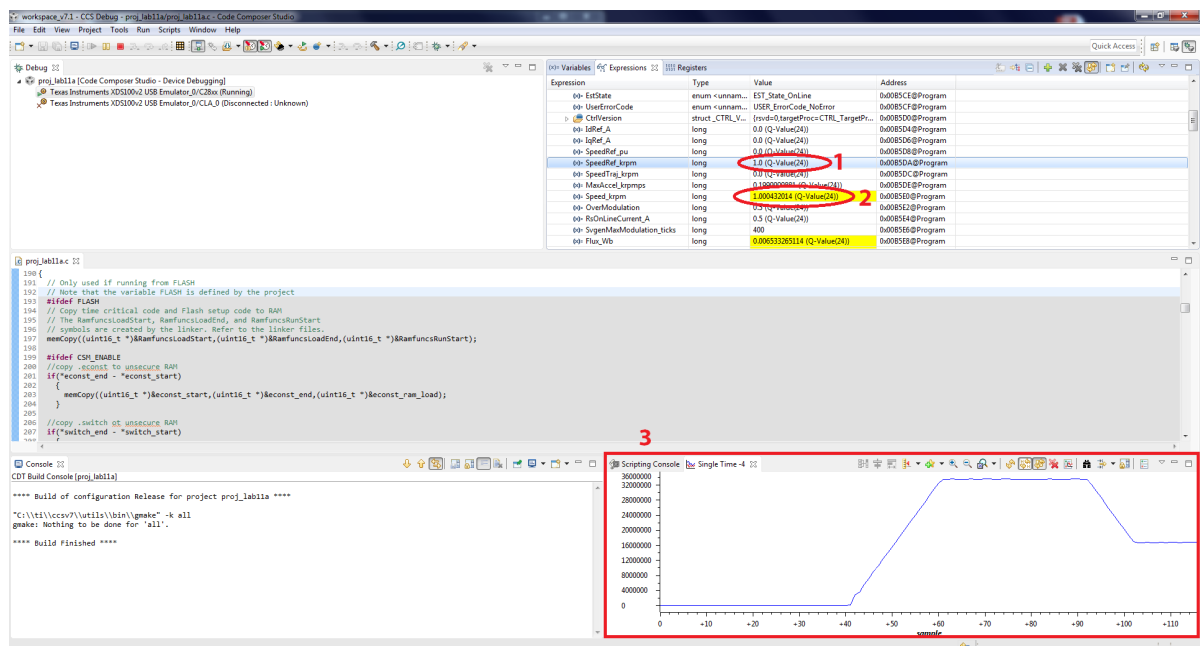


Figure A.87: Another example like fig. A.86.

More information on the use of this lab can be found in [14].

## A.7. Adding the eCAN module

For integrating the CAN module of the Launchpad first some files need to be downloaded from the archive. This is all done with help from the work of Andrew Buckin [26].

1. Download the zip file: "CAN\_interface-ti-F28069M-master" from the archive.
2. Save it in the folder "C:\ti\motorware\motorware\_1\_01\_00\_18\sw\solutions\"

instaspin\_foc\boards\boostxldr8301\_revB\f28x\f2806xF\src" And extract all the files.

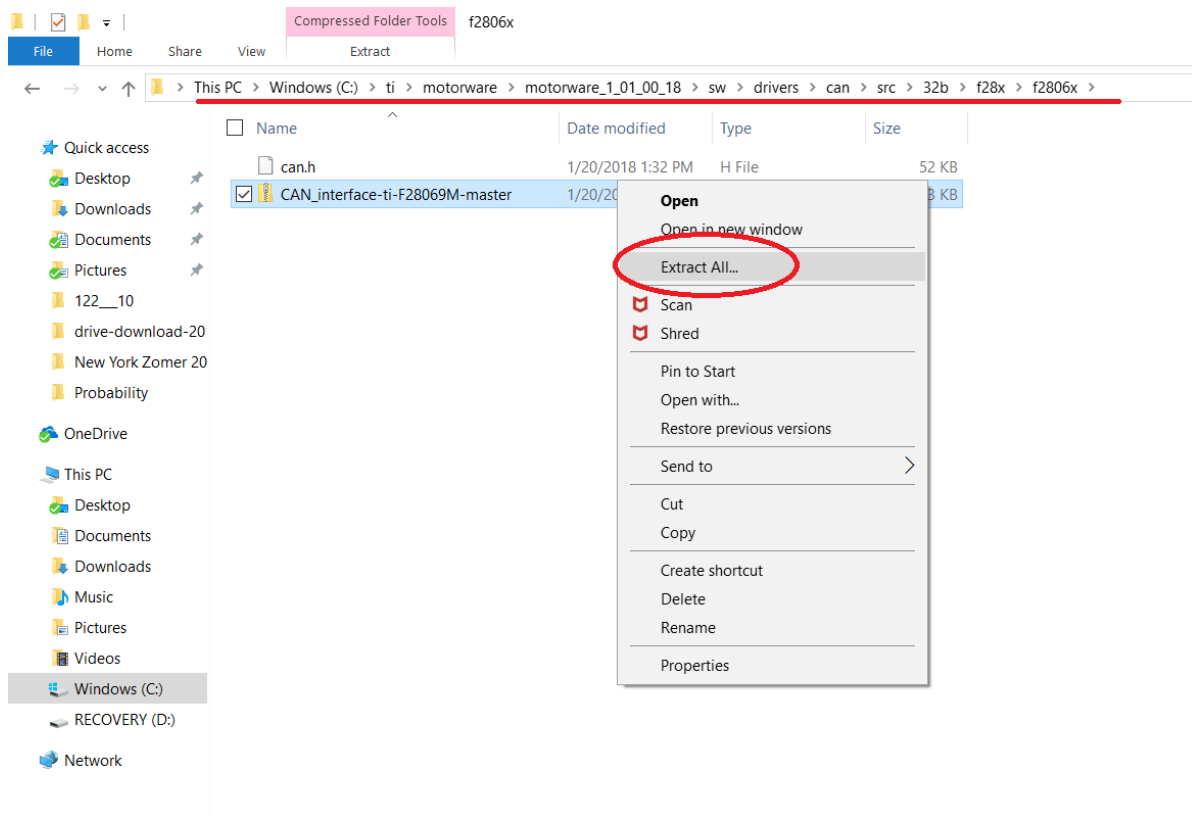


Figure A.88: Step 2: Extract all the files.

3. Copy the can.c and can.h file from "C:\ti\motorware\motorware\_1\_01\_00\_18\sw\drivers\can\src\32b\f28x\f2806x\CAN\_interface-ti-F28069M-master"

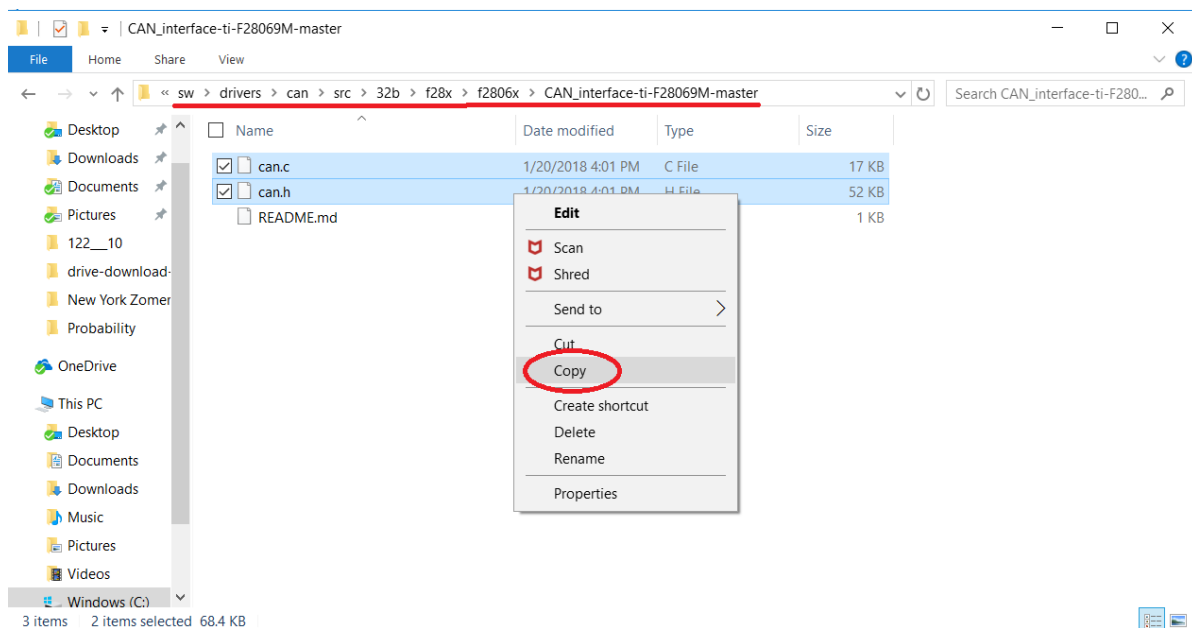


Figure A.89: Step 3: Copy the files from the underlined folder.

- Paste the can.c and can.h files in "C:\ti\motorware\motorware\_1\_01\_00\_18\sw\drivers\can\src\32b\f28x\f2806x"

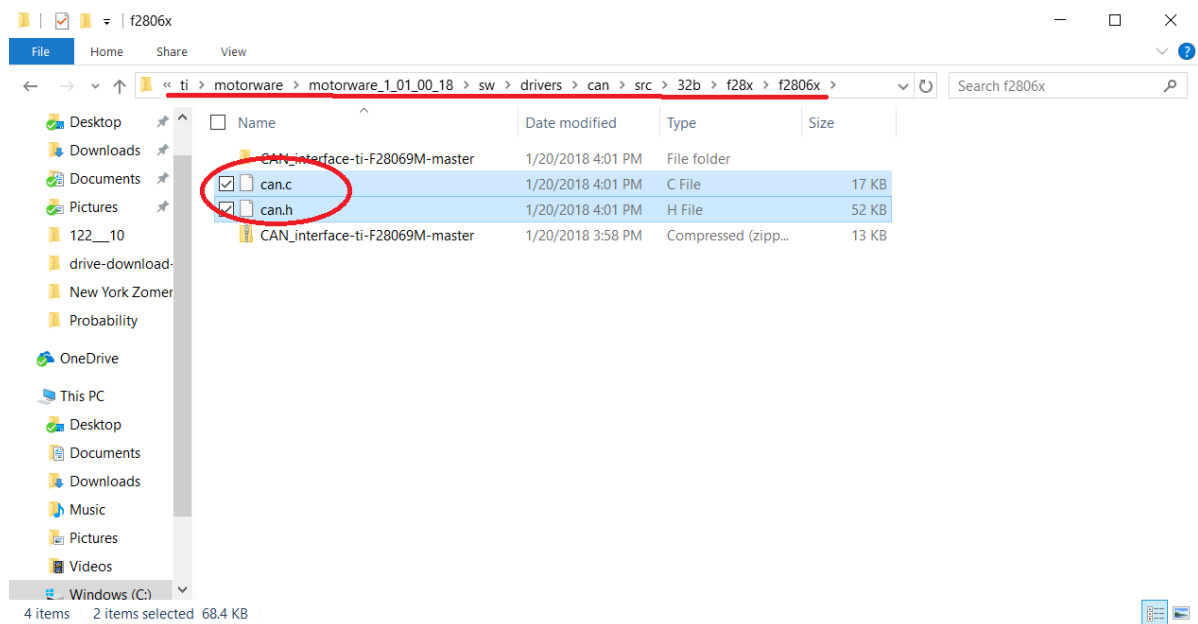


Figure A.90: Step 4: Paste the files from the underlined folder.

- In Code Composer Studio open a project according to the instructions of appendix A.5.3.
- Right-click on the project where the CAN interface needs to be integrated and click "Add Files.."

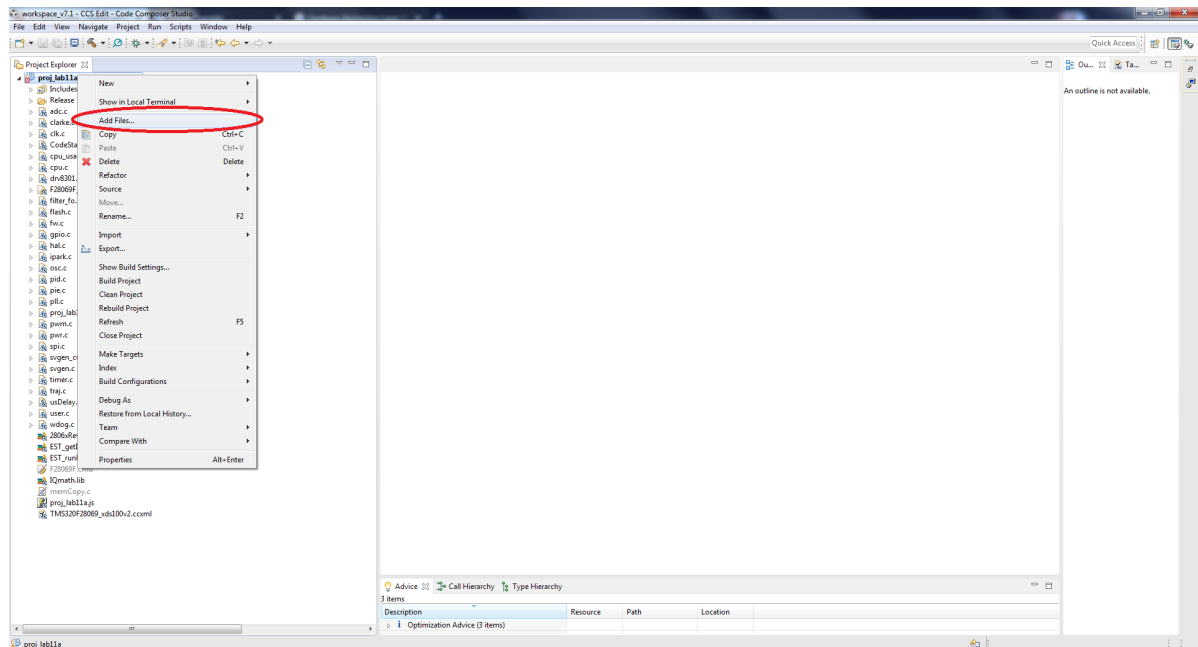


Figure A.91: Step 6: Right-click on the project and click on "Add Files..".

- Go to "C:\ti\motorware\motorware\_1\_01\_00\_18\sw\drivers\can\src\32b\f28x\f2806x" and select can.c.

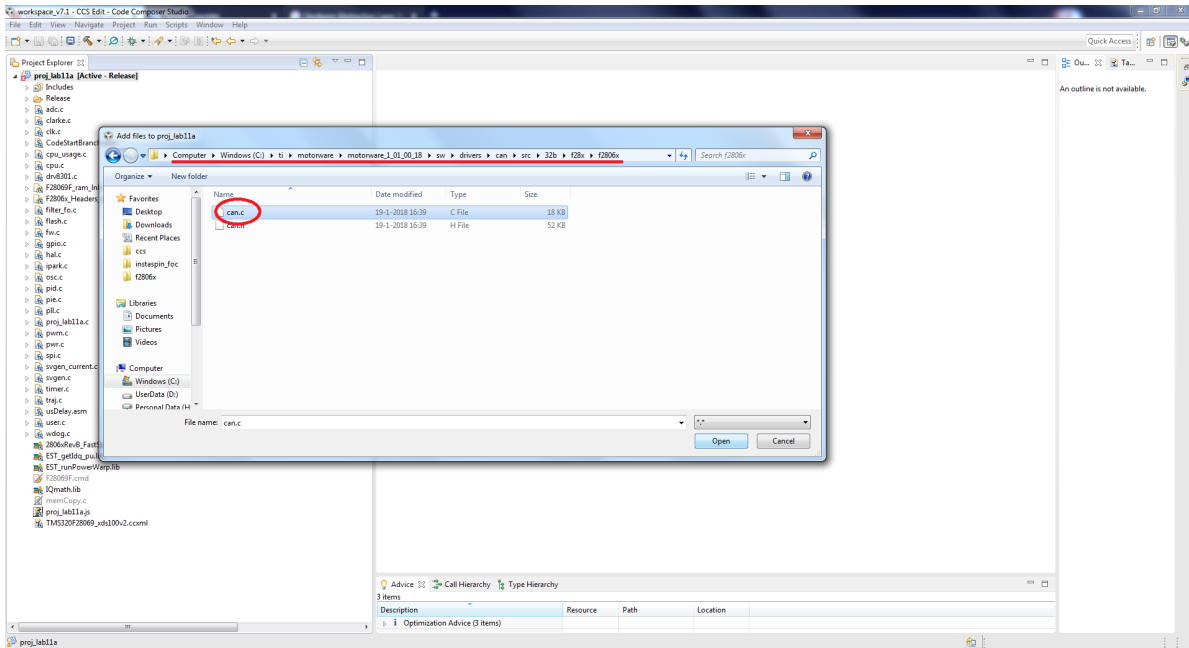


Figure A.92: Step 7: Go to the underlined folder and select can.c.

8. Select link files and set the "Create link locations relative to:" drop-down menu to "MW\_INSTALL\_DIR". Then click OK.

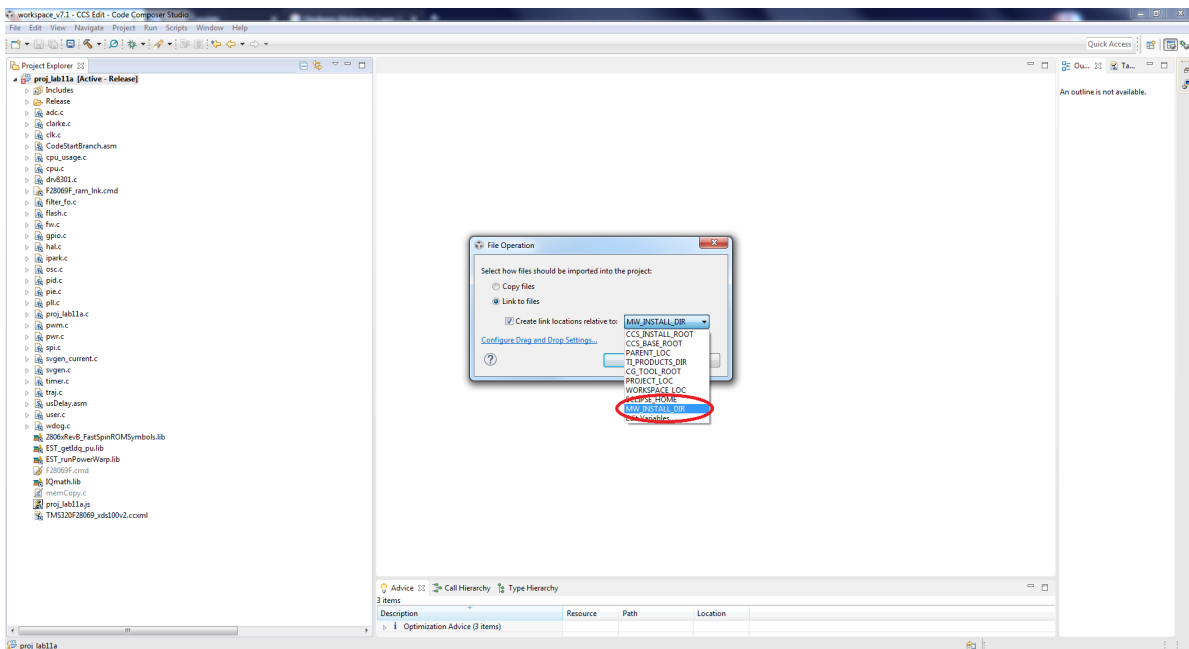


Figure A.93: Step 8: Select Link files and select MW\_INSTALL\_DIR and click Ok.

9. Right-click on the project where the CAN interface needs to be integrated and click "Add Files..."

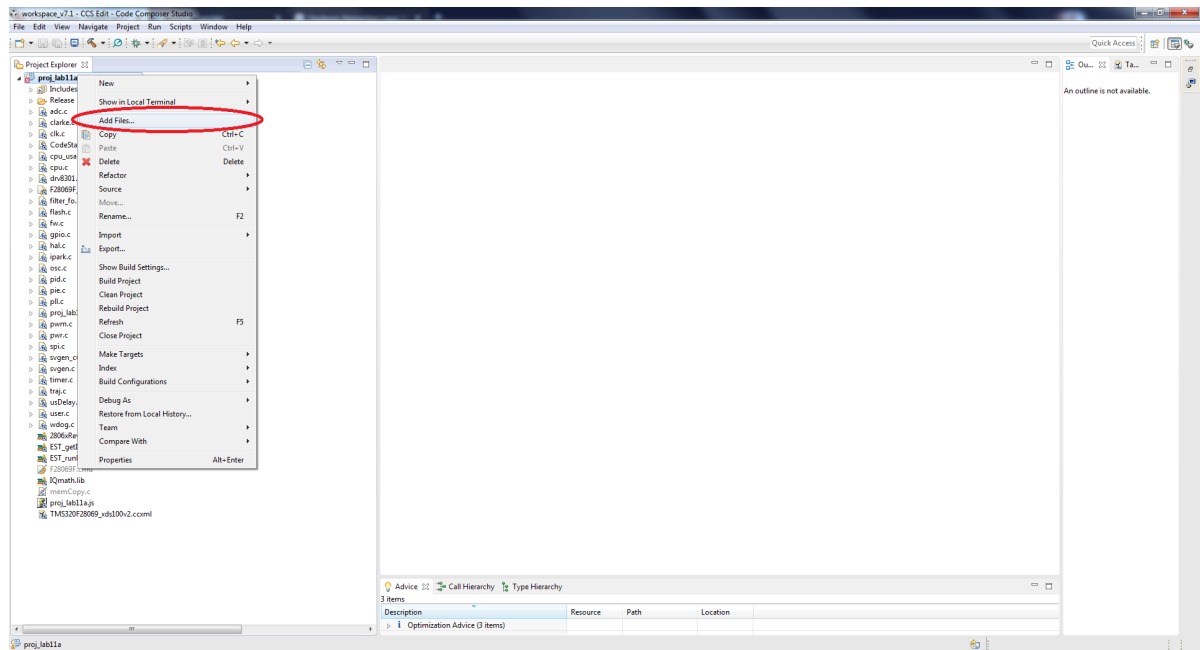


Figure A.94: Step 9: Right-click on the project and click on “Add Files...”

10. Go to “C:\ti\motorware\motorware\_1\_01\_00\_18\sw\ide\ccs\cmd\f2806x” and select F2806x\_Headers\_nonBIOS.

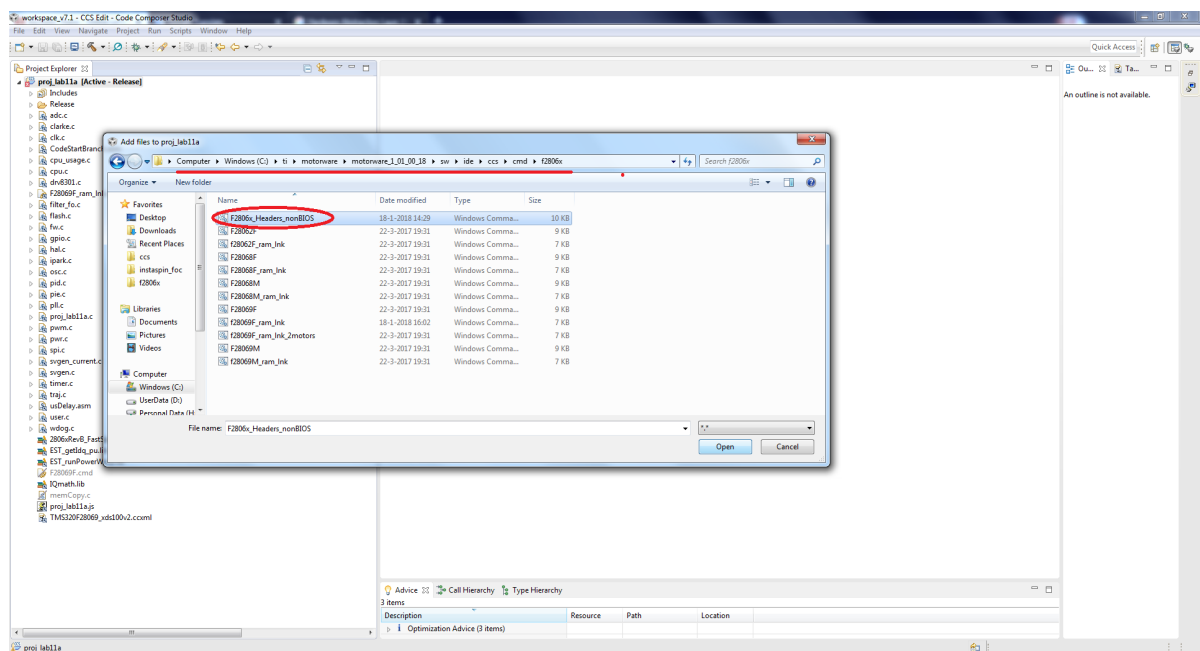


Figure A.95: Step 10: Go to the underlined folder and select F2806x\_Headers\_nonBIOS.

11. Select link files and set the “Create link locations relative to:” drop-down menu to “MW\_INSTALL\_DIR”. Then click OK.

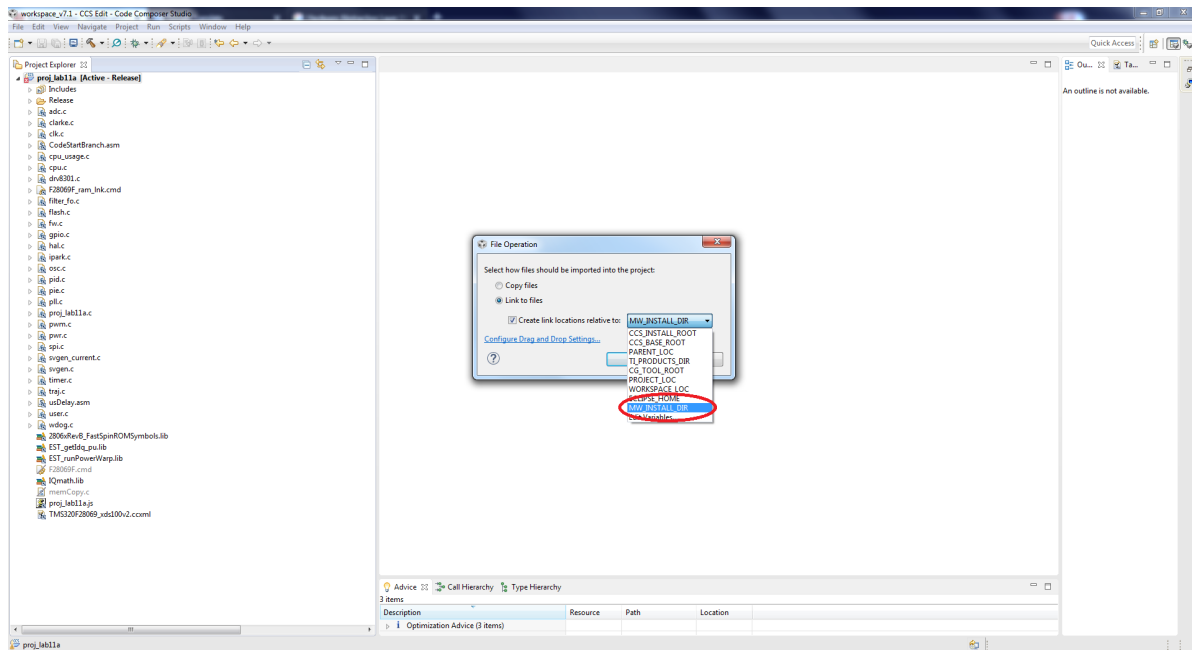


Figure A.96: Step 11: Select Link files and select MW\_INSTALL\_DIR and click Ok.

After adding the files, the codes of hal.c, hal.h and hal\_obj.h need to be modified to integrate and initialize the CAN module.

12. Open hal.c, select hal\_obj.h. Then right-click and click on "Open Declaration" or press F3.

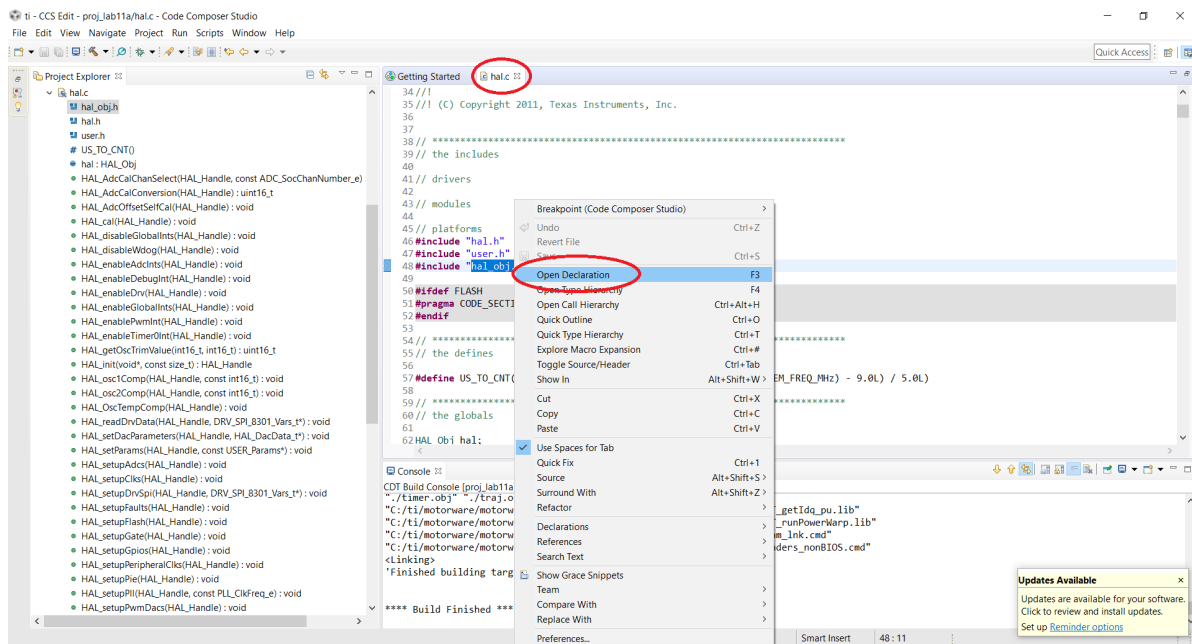


Figure A.97: Step 12: Open the file hal\_obj.h.

13. Then hal\_obj.h opens. Add the following line of code beneath the rest of the drivers:

```
#include "sw/drivers/can/src/32b/f28x/f2806x/can.h"
```

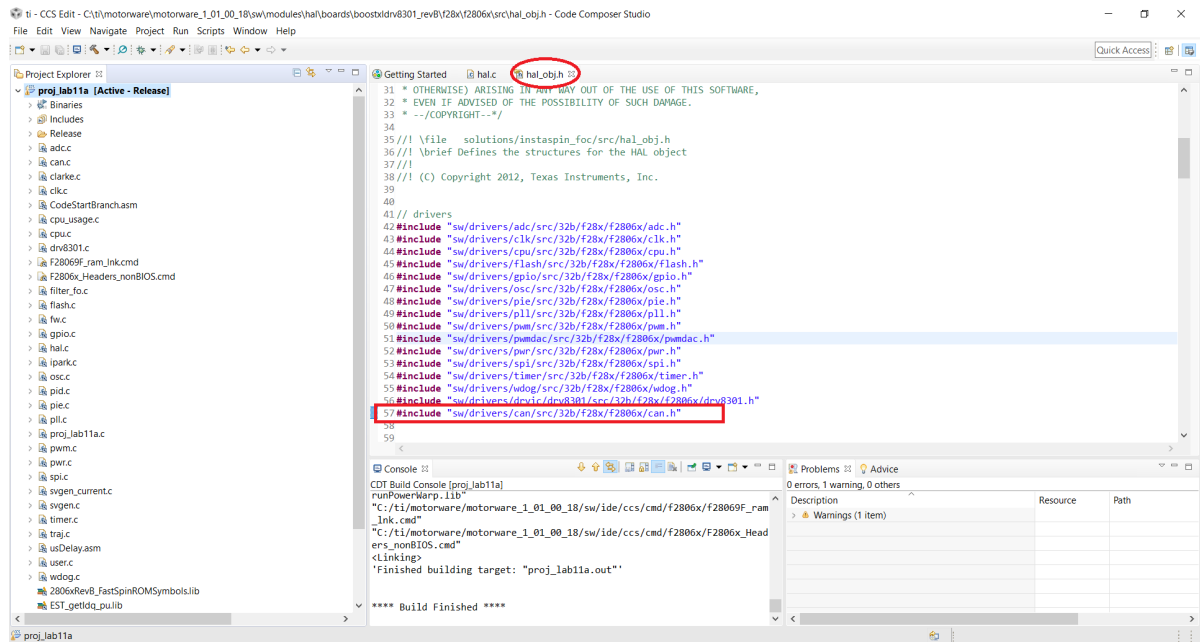


Figure A.98: Step 13: Add the line of code to hal\_obj.h.

#### 14. Add the following line of code at the end of the HAL\_Obj function:

```
ECAN_Handle      ecanHandle;          //!< The eCAN handle
```

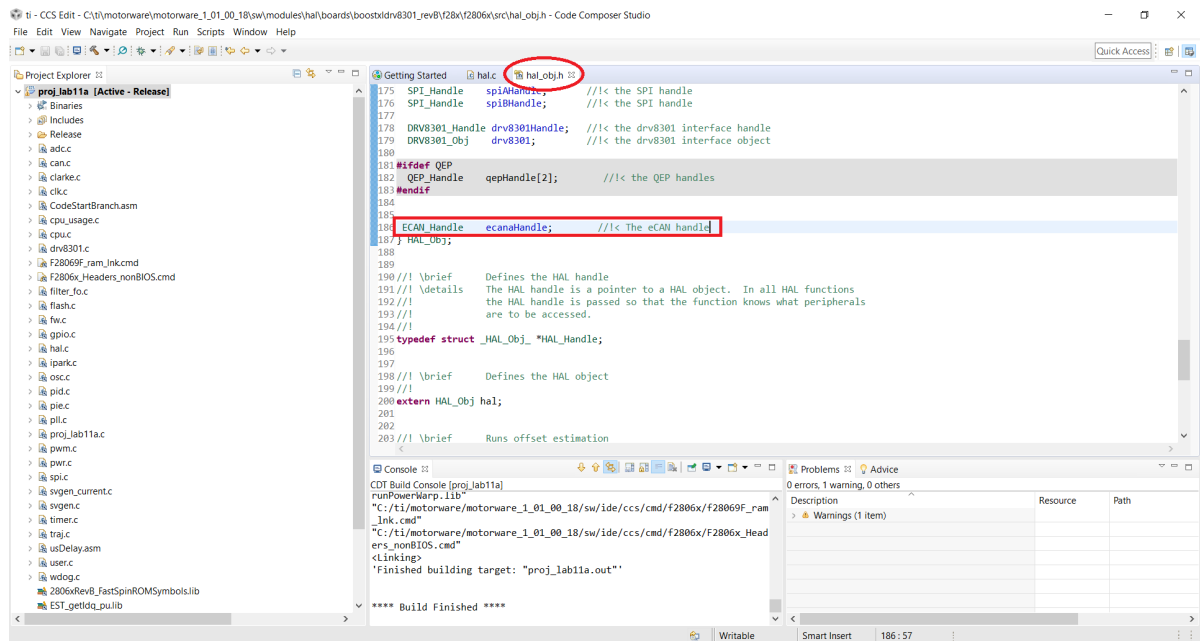


Figure A.99: Step 14: Add the line of code to hal\_obj.h.

#### 15. Close hal\_obj.h, open the hal.c code and select hal.h. Right-click and click on "Open Declaration" or press F3.



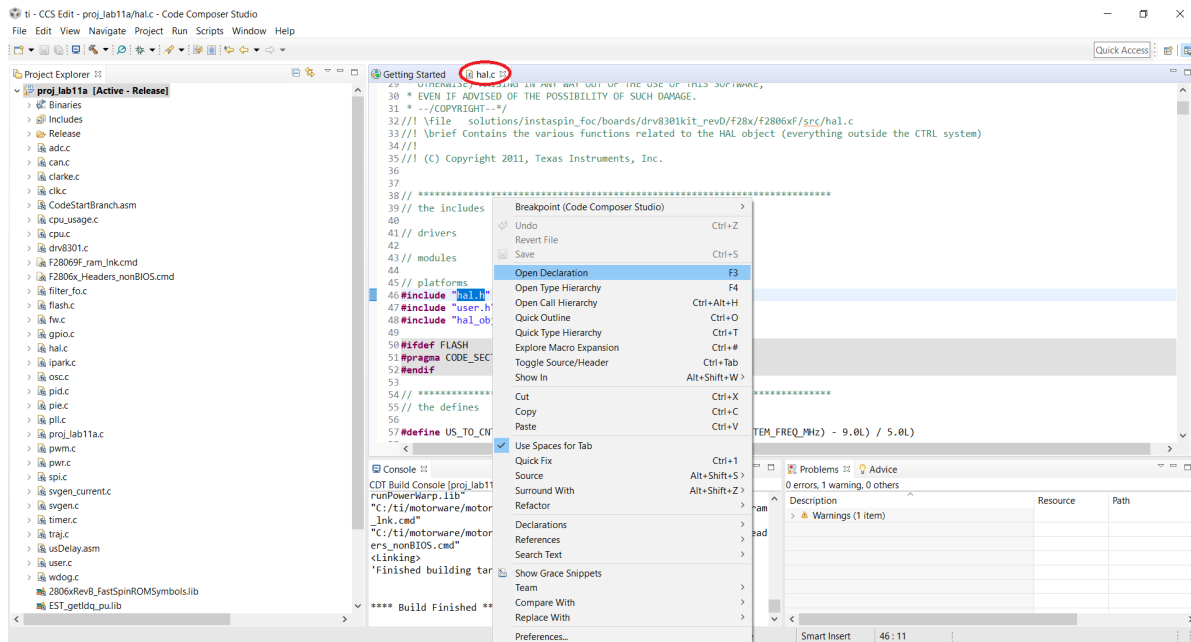


Figure A.100: Step 15: Open the file hal.h.

16. Go to the end of the headerfile hal.h and add the following lines of code:

```

!!! \brief      Sets up the ECAN module.
!!! \param[in] handle The hardware abstraction layer (HAL) handle
extern void HAL_setupECAN(HAL_Handle handle);

```

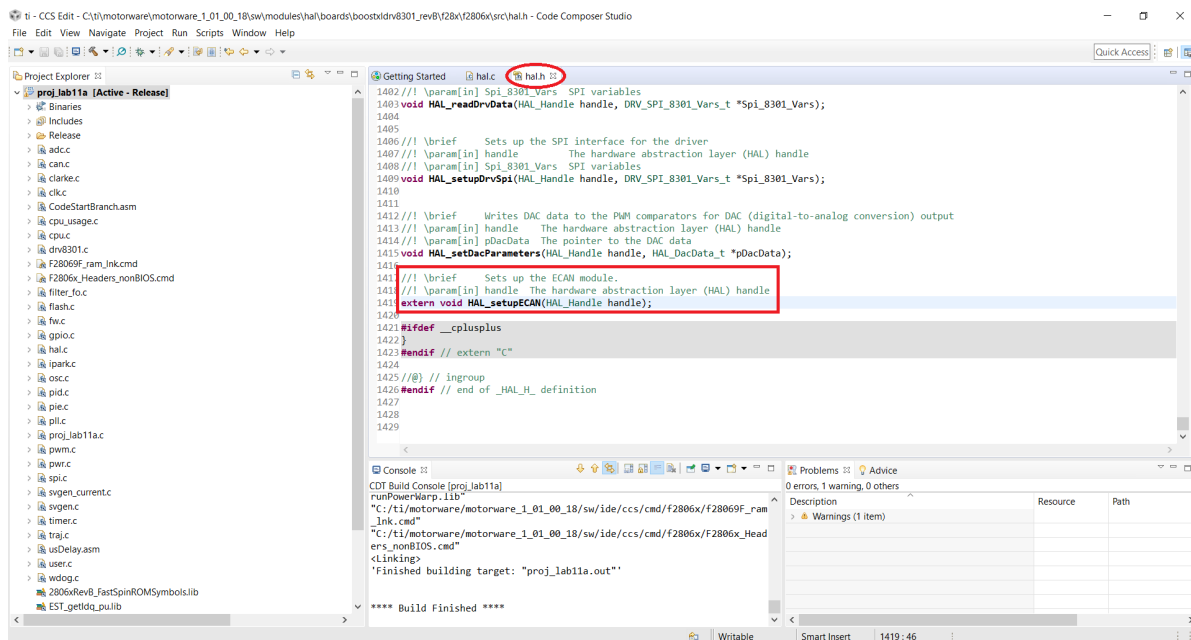


Figure A.101: Step 16: Add the lines of code to hal.h.

17. Close hal.h and open hal.c. At the end of the HAL\_init() function, add the following line of code:

```
obj->ecanaHandle = ECAN_init(); //Initialize the CAN handle
```

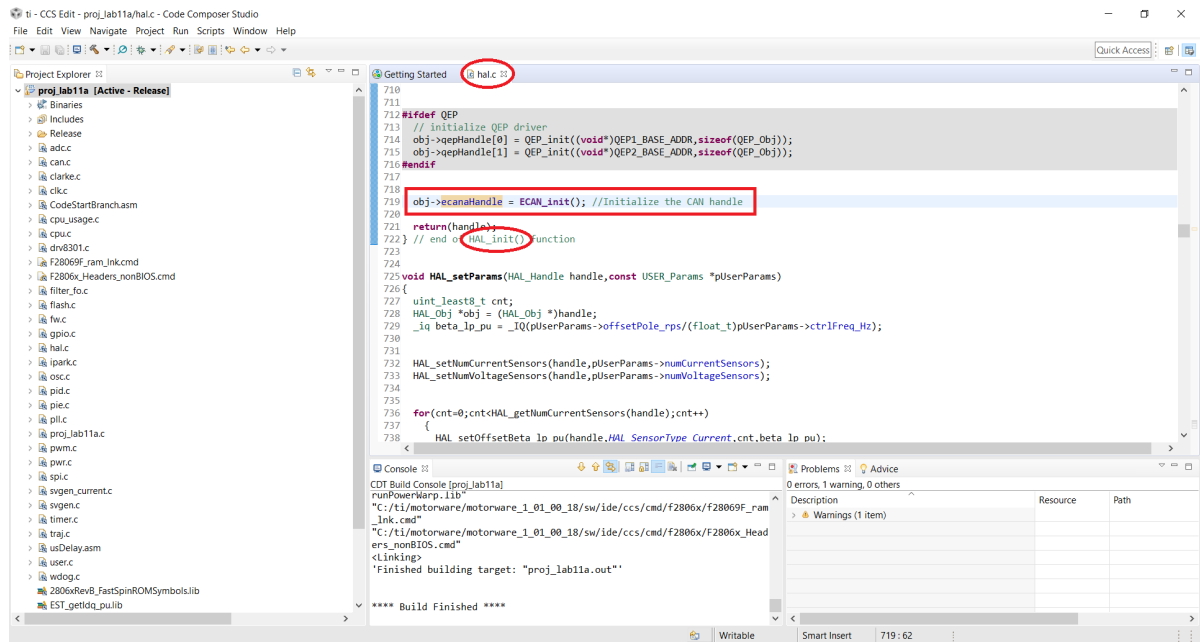


Figure A.102: Step 17: Add the line of code to hal.c.

18. Then call the function HAL\_setupCAN by adding the following lines of code:

```
// setup the eCAN
HAL_setupECAN(handle);
```

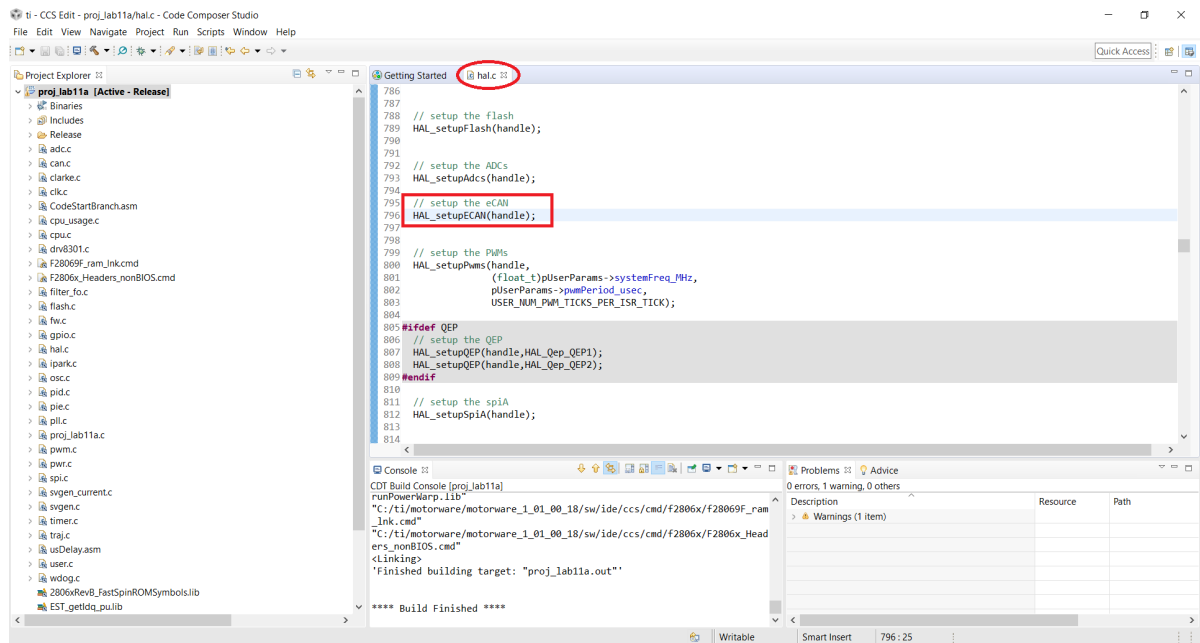


Figure A.103: Step 18: Add the lines of code to hal.c.

19. Check if the GPIO's are declared right. GPIO30 is for receiving CAN messages (CANRXA) and GPIO31 is for transmitting CAN messages (CANTXA).

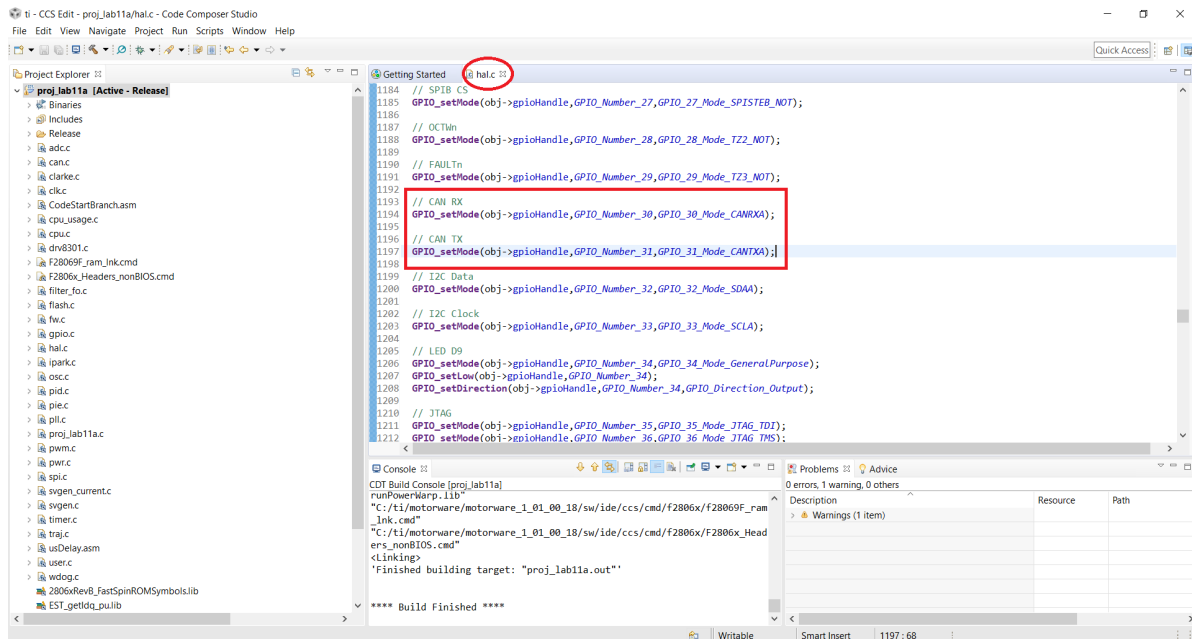


Figure A.104: Step 19: Check the GPIO 30 and 31 functions in hal.c.

20. Check if the eCAN clock is enabled in hal.c. If not change

```
CLK_disableEcanaClock(obj->clkHandle);
```

in

```
CLK_enableEcanaClock(obj->clkHandle);
```

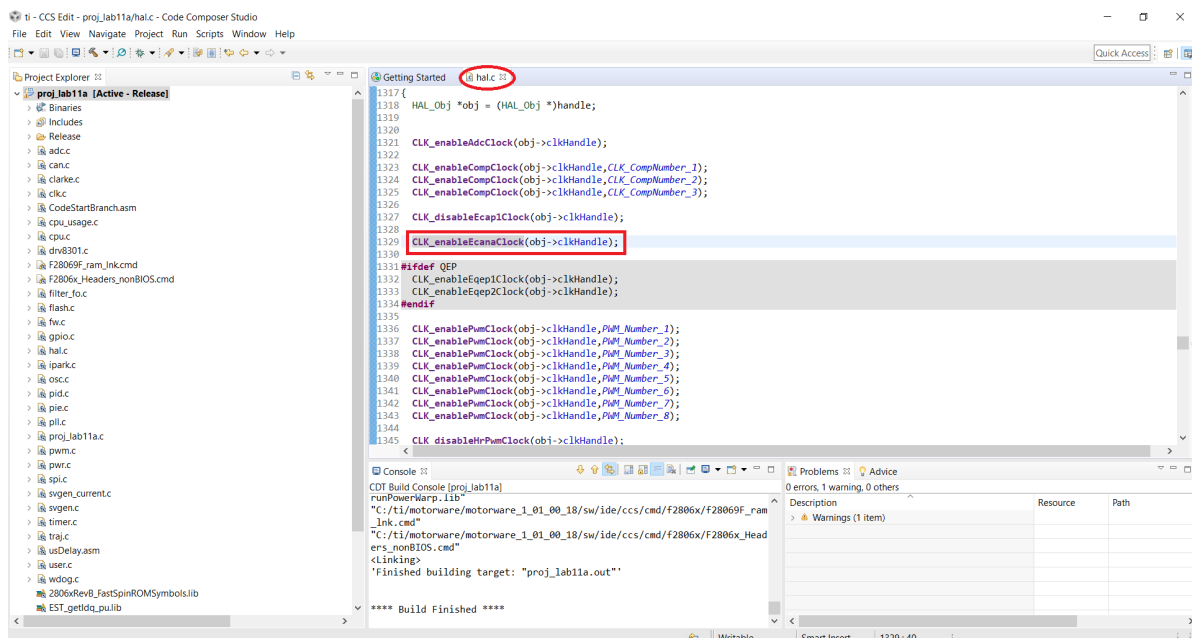


Figure A.105: Step 20: Check if the eCAN clock is enabled in hal.c.

21. Add the following function at the end of hal.c:

```

void HAL_setupECAN(HAL_Handle handle){
    HAL_Obj *obj = (HAL_Obj *)handle;

    ECAN_setTXIO(obj->ecanaHandle);
    ECAN_setRXIO(obj->ecanaHandle);
    // ECAN_setSCCmode(obj->ecanaHandle);
    ECAN_Mode(obj->ecanaHandle, eCANmode);

    ECAN_disableAllMailbox(obj->ecanaHandle);
    ECAN_clearMSGCTRL(obj->ecanaHandle);
    ECAN_clearMSGID(obj->ecanaHandle);
    // ECAN_clearMDL(obj->ecanaHandle);
    // ECAN_clearMDH(obj->ecanaHandle);

    ECAN_clearCANTA(obj->ecanaHandle);
    ECAN_clearCANRMP(obj->ecanaHandle);
    ECAN_clearCANGIF0(obj->ecanaHandle);
    ECAN_clearCANGIF1(obj->ecanaHandle);

    ECAN_disableAllInt(obj->ecanaHandle);
    ECAN_configMasterReg(obj->ecanaHandle, Normal_operation,
        Power_normal, MSB, PDR_activity, Requests_normal,
        ABO_0, No_effect, Mailbox_N0);
    ECAN_setBitrate(obj->ecanaHandle, Bitrate_500K);
    // 90 MHz SYSCLKOUT. 45 MHz CAN module clock Bit rate = 500 Kbps

    // ECAN_setBTCreg(obj->ecanaHandle, 0x000503BD); // sprac35
    // ECAN_enableAllInt(obj->ecanaHandle);
    // ECAN_enableAllMailbox(obj->ecanaHandle);
    // ECAN_setMailboxDir(obj->ecanaHandle, 0xFFFF0000);
    //Configure Mailboxes 0-15 as Tx, 16-31 as Rx

    ECAN_setMailboxIntMask(obj->ecanaHandle, 0x00000000);
        //Mailbox interrupt is disabled.

    //MailBoxID                Mask
    ECAN_configMailbox(obj->ecanaHandle, MailBox0, 6, Enable_Mbox,
        Tx_Dir, Standard_ID, DLC_8, LAMI_0,
        Mask_is_used, 0x0000FF80);
    ECAN_configMailbox(obj->ecanaHandle, MailBox16, 6, Enable_Mbox,
        Rx_Dir, Standard_ID, DLC_8, LAMI_0,
        Mask_is_used, 0x0000FF80);
    ECAN_SelfTest(obj->ecanaHandle, Normal_mode);
}

```

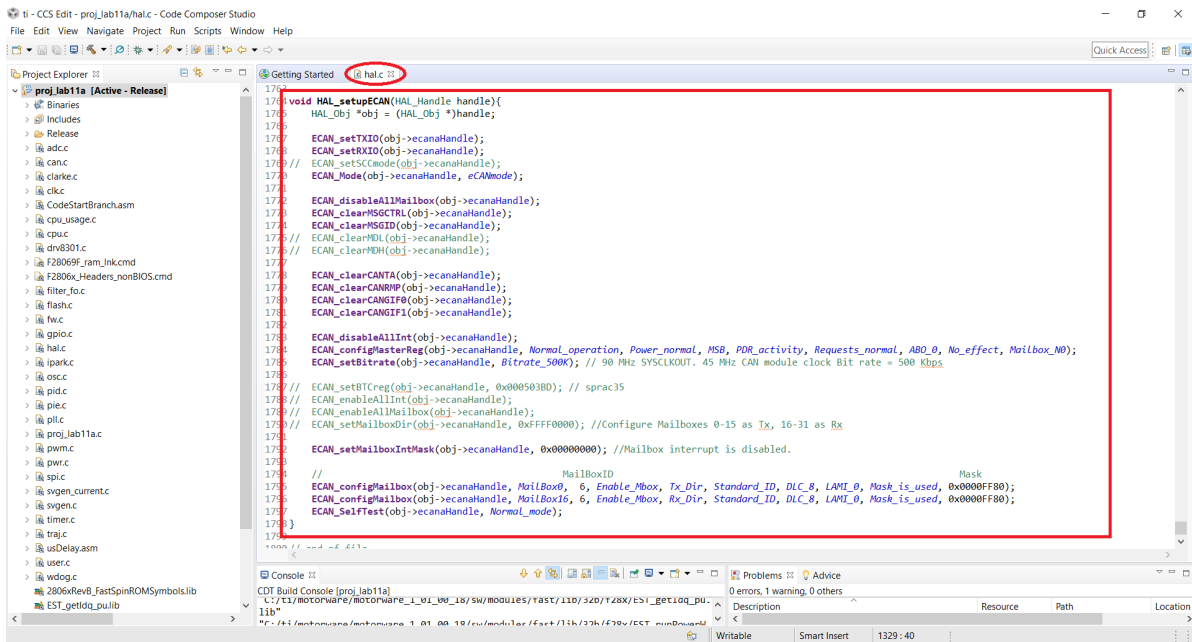


Figure A.106: Step 21: Add the following lines of code to hal.c.

Now the CAN interface is fully integrated in the project and ready to use. However the mailboxes still need to be configured in the proj\_labx.c code, where x is the lab in which the CAN module is integrated.

### A.7.1. .esysmem warning after building

It is possible that after building the project the following warning appears:

warning #10210-D: creating ".esysmem" section with default size of 0x400; use the -heap option to change the default size

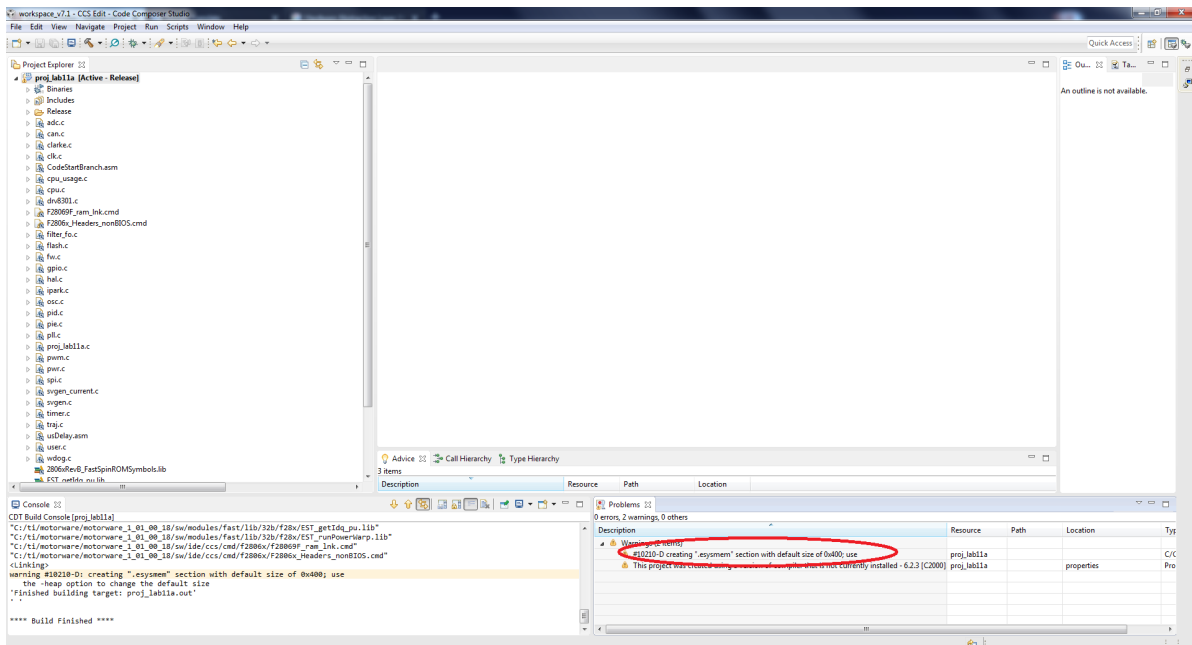


Figure A.107: The .esysmem warning.

This can be resolved by doing the following:

1. Go to Project and click on "Show Build Settings...".

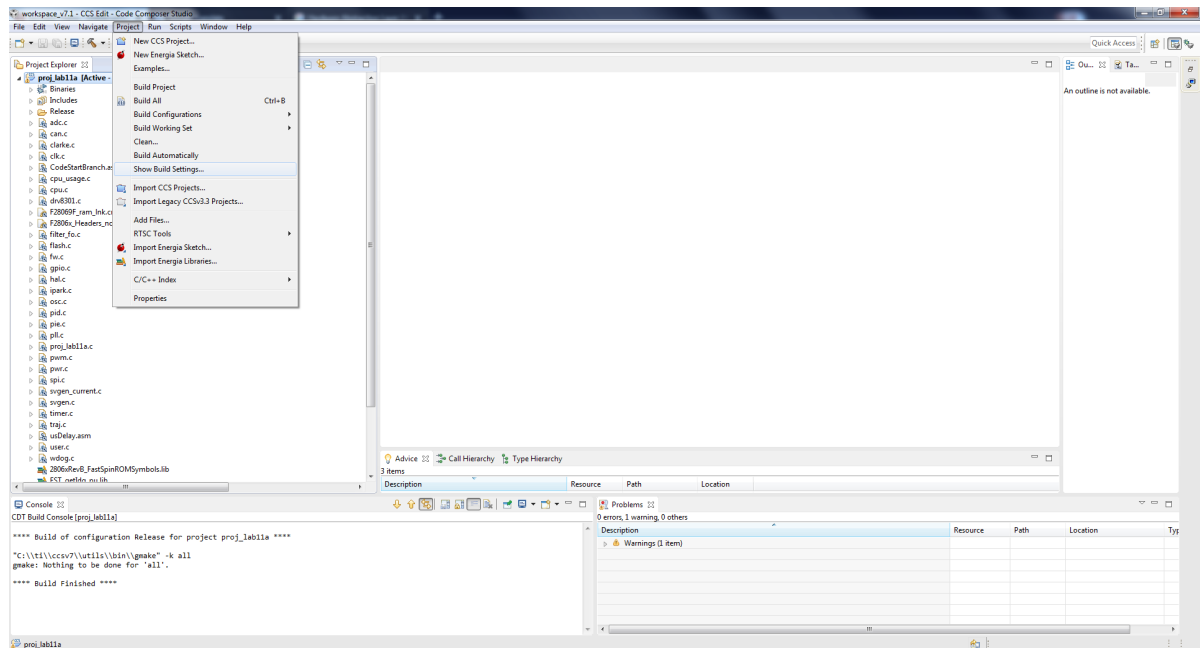


Figure A.108: Step 1: Go to build settings.

2. In the build settings, open the "C2000 Linker" drop-down menu. In this menu select "Basic Options". At that moment the Heap Size is left empty. Fill in a hexadecimal number of at least 0x400, but preferably 0x800 or larger. Then click OK and the issue is resolved.

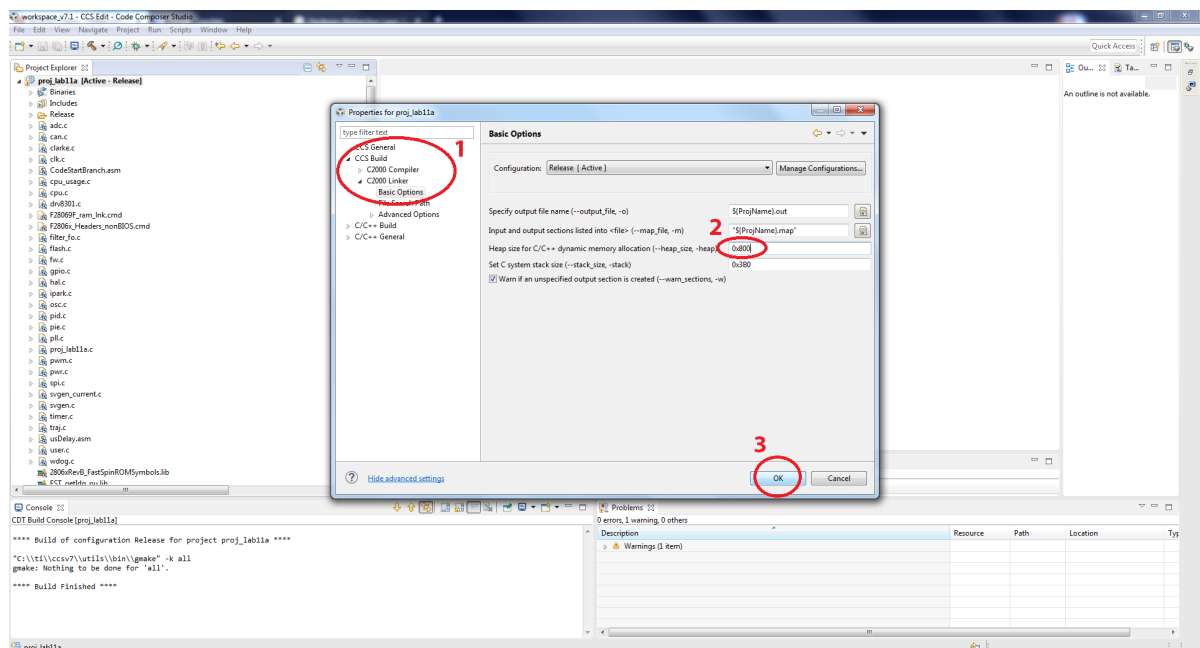


Figure A.109: Step 2: Change the Heap Size in the build settings.

# B

## user.h & user\_j1.h code

### B.1. user.h

```
1 #ifndef _USER_H_
2 #define _USER_H_
3 /* ---COPYRIGHT---,BSD
4 * Copyright (c) 2012, Texas Instruments Incorporated
5 * All rights reserved.
6 *
7 * Redistribution and use in source and binary forms, with or without
8 * modification, are permitted provided that the following conditions
9 * are met:
10 *
11 * * Redistributions of source code must retain the above copyright
12 * * notice, this list of conditions and the following disclaimer.
13 * *
14 * * Redistributions in binary form must reproduce the above copyright
15 * * notice, this list of conditions and the following disclaimer in the
16 * * documentation and/or other materials provided with the distribution.
17 * *
18 * * Neither the name of Texas Instruments Incorporated nor the names of
19 * * its contributors may be used to endorse or promote products derived
20 * * from this software without specific prior written permission.
21 *
22 * THIS SOFTWARE IS PROVIDED BY THE COPYRIGHT HOLDERS AND CONTRIBUTORS "AS IS"
23 * AND ANY EXPRESS OR IMPLIED WARRANTIES, INCLUDING, BUT NOT LIMITED TO,
24 * THE IMPLIED WARRANTIES OF MERCHANTABILITY AND FITNESS FOR A PARTICULAR
25 * PURPOSE ARE DISCLAIMED. IN NO EVENT SHALL THE COPYRIGHT OWNER OR
26 * CONTRIBUTORS BE LIABLE FOR ANY DIRECT, INDIRECT, INCIDENTAL, SPECIAL,
27 * EXEMPLARY, OR CONSEQUENTIAL DAMAGES (INCLUDING, BUT NOT LIMITED TO,
28 * PROCUREMENT OF SUBSTITUTE GOODS OR SERVICES; LOSS OF USE, DATA, OR PROFITS;
29 * OR BUSINESS INTERRUPTION) HOWEVER CAUSED AND ON ANY THEORY OF LIABILITY,
30 * WHETHER IN CONTRACT, STRICT LIABILITY, OR TORT (INCLUDING NEGLIGENCE OR
31 * OTHERWISE) ARISING IN ANY WAY OUT OF THE USE OF THIS SOFTWARE,
32 * EVEN IF ADVISED OF THE POSSIBILITY OF SUCH DAMAGE.
33 * ---/COPYRIGHT---*/
34
35 /*! \file solutions/instaspin_foc/boards/boostxldrv8301_revB/f28x/f2806xF/src/user.h
36  * \brief Contains the public interface for user initialization data for the CTRL, HAL, and EST modules
37  * \!
38  * \! (C) Copyright 2012, Texas Instruments, Inc.
39  * \!
40  * \!
41  * \! *****
42  * \! the includes
43  * \!
44  * \! modules
45  * \! #include "sw/modules/types/src/types.h"
46  * \! #include "sw/modules/motor/src/32b/motor.h"
47  * \! #include "sw/modules/est/src/32b/est.h"
48  * \! #include "sw/modules/est/src/est_states.h"
49  * \! #include "sw/modules/est/src/est_Flux_states.h"
50  * \! #include "sw/modules/est/src/est_Ls_states.h"
51  * \! #include "sw/modules/est/src/est_Rs_states.h"
52  * \! #include "sw/modules/ctrl/src/32b/ctrl_obj.h"
53
54
55 // select whether to use the inverter on connector J1 or J5 of the LaunchPad
56 #define J1
```

```

// platforms
#include "sw/modules/fast/src/32b/userParams.h"
61 #ifdef J5
#include "user_j5.h"
#else
#include "user_j1.h"
#endif
66
//!
//!
//! \defgroup USER USER
//!
71 //@{

#ifdef __cplusplus
extern "C" {
76 #endif

// *****
// the defines

81
//! \brief CURRENTS AND VOLTAGES
// *****
//! \brief Defines the voltage scale factor for the system
//! \brief Compile time calculation for scale factor (ratio) used throughout the system
86 #define USER_VOLTAGE_SF ((float_t)((USER_ADC_FULL_SCALE_VOLTAGE_V)/(
USER_IQ_FULL_SCALE_VOLTAGE_V))

//! \brief Defines the current scale factor for the system
//! \brief Compile time calculation for scale factor (ratio) used throughout the system
#define USER_CURRENT_SF ((float_t)((USER_ADC_FULL_SCALE_CURRENT_A)/(
USER_IQ_FULL_SCALE_CURRENT_A))
91

//! \brief CLOCKS & TIMERS
// *****
//! \brief Defines the system clock frequency, MHz
96 #define USER_SYSTEM_FREQ_MHz (90.0)

//! \brief Defines the address of controller handle
//!
#define USER_CTRL_HANDLE_ADDRESS (0x13C40)
101 #define USER_CTRL_HANDLE_ADDRESS_1 (0x13D36)

//! \brief Defines the address of estimator handle
//!
#define USER_EST_HANDLE_ADDRESS (0x13840)
106 #define USER_EST_HANDLE_ADDRESS_1 (0x13A3E)

//! \brief Defines the direct voltage (Vd) scale factor
//!
#define USER_VD_SF (0.95)
111

//! \brief Defines the Pulse Width Modulation (PWM) period, usec
//! \brief Compile time calculation
#define USER_PWM_PERIOD_usec (1000.0/USER_PWM_FREQ_kHz)

116 //! \brief Defines the Interrupt Service Routine (ISR) frequency, Hz
//!
#define USER_ISR_FREQ_Hz ((float_t)USER_PWM_FREQ_kHz * 1000.0 / (float_t)
USER_NUM_PWM_TICKS_PER_ISR_TICK)

//! \brief Defines the Interrupt Service Routine (ISR) period, usec
//!
121 #define USER_ISR_PERIOD_usec (USER_PWM_PERIOD_usec * (float_t)USER_NUM_PWM_TICKS_PER_ISR_TICK)

//! \brief DECIMATION
126 // *****
//! \brief Defines the controller frequency, Hz
//! \brief Compile time calculation
#define USER_CTRL_FREQ_Hz (uint_least32_t)(USER_ISR_FREQ_Hz/USER_NUM_ISR_TICKS_PER_CTRL_TICK)

131 //! \brief Defines the estimator frequency, Hz
//! \brief Compile time calculation
#define USER_EST_FREQ_Hz (uint_least32_t)(USER_CTRL_FREQ_Hz/USER_NUM_CTRL_TICKS_PER_EST_TICK)

//! \brief Defines the trajectory frequency, Hz
//! \brief Compile time calculation
136 #define USER_TRAJ_FREQ_Hz (uint_least32_t)(USER_CTRL_FREQ_Hz/USER_NUM_CTRL_TICKS_PER_TRAJ_TICK)

```



```

141  /// \brief Defines the controller execution period, usec
/// \brief Compile time calculation
#define USER_CTRL_PERIOD_usec      (USER_ISR_PERIOD_usec * USER_NUM_ISR_TICKS_PER_CTRL_TICK)

/// \brief Defines the controller execution period, sec
/// \brief Compile time calculation
#define USER_CTRL_PERIOD_sec      ((float_t)USER_CTRL_PERIOD_usec/(float_t)1000000.0)
146

/// \brief LIMITS
// *****
/// \brief Defines the maximum current slope for Id trajectory during PowerWarp
151 /// \brief For Induction motors only, controls how fast Id input can change under PowerWarp control
#define USER_MAX_CURRENT_SLOPE_POWERWARP (0.3*USER_MOTOR_RES_EST_CURRENT/USER_IQ_FULL_SCALE_CURRENT_A/
USER_TRAJ_FREQ_Hz) // 0.3*RES_EST_CURRENT / IQ_FULL_SCALE_CURRENT / TRAJ_FREQ Typical to produce 1-
sec rampup/down

/// \brief Defines the starting maximum acceleration AND deceleration for the speed profiles, Hz/s
/// \brief Updated in run-time through user functions
156 /// \brief Inverter, motor, inertia, and load will limit actual acceleration capability
#define USER_MAX_ACCEL_Hzps        (20.0) // 20.0 Default

/// \brief Defines maximum acceleration for the estimation speed profiles, Hz/s
/// \brief Only used during Motor ID (commission)
161 #define USER_MAX_ACCEL_EST_Hzps   (5.0) // 5.0 Default, don't change

/// \brief Defines the maximum current slope for Id trajectory during estimation
#define USER_MAX_CURRENT_SLOPE     (USER_MOTOR_RES_EST_CURRENT/USER_IQ_FULL_SCALE_CURRENT_A/
USER_TRAJ_FREQ_Hz) // USER_MOTOR_RES_EST_CURRENT/USER_IQ_FULL_SCALE_CURRENT_A/USER_TRAJ_FREQ_Hz
Default, don't change

166 /// \brief Defines the fraction of IdRated to use during rated flux estimation
///
#define USER_IDRATED_FRACTION_FOR_RATED_FLUX (1.0) // 1.0 Default, don't change

/// \brief Defines the fraction of IdRated to use during inductance estimation
171 ///
#define USER_IDRATED_FRACTION_FOR_L_IDENT (1.0) // 1.0 Default, don't change

/// \brief Defines the IdRated delta to use during estimation
///
176 #define USER_IDRATED_DELTA        (0.00002)

/// \brief Defines the fraction of SpeedMax to use during inductance estimation
///
#define USER_SPEEDMAX_FRACTION_FOR_L_IDENT (1.0) // 1.0 Default, don't change
181

/// \brief Defines flux fraction to use during inductance identification
///
#define USER_FLUX_FRACTION        (1.0) // 1.0 Default, don't change

186 /// \brief Defines the PowerWarp gain for computing Id reference
/// \brief Induction motors only
#define USER_POWERWARP_GAIN        (1.0) // 1.0 Default, don't change

191 /// \brief POLES
// *****
/// \brief Defines the analog voltage filter pole location, rad/s
/// \brief Compile time calculation from Hz to rad/s
#define USER_VOLTAGE_FILTER_POLE_rps (2.0 * MATH_PI * USER_VOLTAGE_FILTER_POLE_Hz)
196

/// \brief Defines the software pole location for the voltage and current offset estimation, rad/s
/// \brief Should not be changed from default of (20.0)
#define USER_OFFSET_POLE_rps       (20.0) // 20.0 Default, do not change

201 /// \brief Defines the software pole location for the flux estimation, rad/s
/// \brief Should not be changed from default of (100.0)
#define USER_FLUX_POLE_rps        (100.0) // 100.0 Default, do not change

/// \brief Defines the software pole location for the direction filter, rad/s
206 #define USER_DIRECTION_POLE_rps   (6.0) // 6.0 Default, do not change

/// \brief Defines the software pole location for the speed control filter, rad/s
#define USER_SPEED_POLE_rps       (100.0) // 100.0 Default, do not change

211 /// \brief Defines the software pole location for the DC bus filter, rad/s
#define USER_DCBUS_POLE_rps       (100.0) // 100.0 Default, do not change

/// \brief Defines the convergence factor for the estimator
/// \brief Do not change from default for FAST
216 #define USER_EST_KAPPAQ          (1.5) // 1.5 Default, do not change

// *****

```

```

// end the defines

221
///brief USER MOTOR & ID SETTINGS
///*****
///this section defined in user_j1.h or user_j5.h

226 #ifndef USER_MOTOR
#error Motor is not defined in user.h
#endif

#ifndef USER_MOTOR_TYPE
231 #error The motor type is not defined in user.h
#endif

#ifndef USER_MOTOR_NUM_POLE_PAIRS
#error Number of motor pole pairs is not defined in user.h
236 #endif

#ifndef USER_MOTOR_Rr
#error The rotor resistance is not defined in user.h
#endif

241 #ifndef USER_MOTOR_Rs
#error The stator resistance is not defined in user.h
#endif

246 #ifndef USER_MOTOR_Ls_d
#error The direct stator inductance is not defined in user.h
#endif

#ifndef USER_MOTOR_Ls_q
251 #error The quadrature stator inductance is not defined in user.h
#endif

#ifndef USER_MOTOR_RATED_FLUX
#error The rated flux of motor is not defined in user.h
256 #endif

#ifndef USER_MOTOR_MAGNETIZING_CURRENT
#error The magnetizing current is not defined in user.h
#endif

261 #ifndef USER_MOTOR_RES_EST_CURRENT
#error The resistance estimation current is not defined in user.h
#endif

266 #ifndef USER_MOTOR_IND_EST_CURRENT
#error The inductance estimation current is not defined in user.h
#endif

#ifndef USER_MOTOR_MAX_CURRENT
271 #error The maximum current is not defined in user.h
#endif

#ifndef USER_MOTOR_FLUX_EST_FREQ_Hz
276 #error The flux estimation frequency is not defined in user.h
#endif

// *****
// the functions

281

///brief Sets the user parameter values
///param[in] pUserParams The pointer to the user param structure
extern void USER_setParams(USER_Params *pUserParams);

286

///brief Checks for errors in the user parameter values
///param[in] pUserParams The pointer to the user param structure
extern void USER_checkForErrors(USER_Params *pUserParams);

291

///brief Gets the error code in the user parameters
///param[in] pUserParams The pointer to the user param structure
///return The error code
296 extern USER_ErrorCode_e USER_getErrorCode(USER_Params *pUserParams);

///brief Sets the error code in the user parameters
///param[in] pUserParams The pointer to the user param structure
301 ///param[in] errorCode The error code
extern void USER_setErrorCode(USER_Params *pUserParams, const USER_ErrorCode_e errorCode);

```

```

306 ///! \brief Recalculates Inductances with the correct Q Format
///! \param[in] handle The controller (CTRL) handle
extern void USER_softwareUpdate1p6(CTRL_Handle handle);

311 ///! \brief Updates Id and Iq PI gains
///! \param[in] handle The controller (CTRL) handle
extern void USER_calcPIgains(CTRL_Handle handle);

316 ///! \brief Computes the scale factor needed to convert from torque created by Ld, Lq, Id and Iq, from
per unit to Nm
///! \return The scale factor to convert torque from (Ld - Lq) * Id * Iq from per unit to Nm, in IQ24
format
extern _iq USER_computeTorque_Ls_Id_Iq_pu_to_Nm_sf(void);

321 ///! \brief Computes the scale factor needed to convert from torque created by flux and Iq, from per
unit to Nm
///! \return The scale factor to convert torque from Flux * Iq from per unit to Nm, in IQ24 format
extern _iq USER_computeTorque_Flux_Iq_pu_to_Nm_sf(void);

326 ///! \brief Computes the scale factor needed to convert from per unit to Wb
///! \return The scale factor to convert from flux per unit to flux in Wb, in IQ24 format
extern _iq USER_computeFlux_pu_to_Wb_sf(void);

331 ///! \brief Computes the scale factor needed to convert from per unit to V/Hz
///! \return The scale factor to convert from flux per unit to flux in V/Hz, in IQ24 format
extern _iq USER_computeFlux_pu_to_VpHz_sf(void);

336 ///! \brief Computes Flux in Wb or V/Hz depending on the scale factor sent as parameter
///! \param[in] handle The controller (CTRL) handle
///! \param[in] sf The scale factor to convert flux from per unit to Wb or V/Hz
///! \return The flux in Wb or V/Hz depending on the scale factor sent as parameter, in IQ24 format
extern _iq USER_computeFlux(CTRL_Handle handle, const _iq sf);

341 ///! \brief Computes Torque in Nm
///! \param[in] handle The controller (CTRL) handle
///! \param[in] torque_Flux_sf The scale factor to convert torque from (Ld - Lq) * Id * Iq from per unit
to Nm
///! \param[in] torque_Ls_sf The scale factor to convert torque from Flux * Iq from per unit to Nm
346 ///! \return The torque in Nm, in IQ24 format
extern _iq USER_computeTorque_Nm(CTRL_Handle handle, const _iq torque_Flux_sf, const _iq torque_Ls_sf);

351 ///! \brief Computes Torque in lbin
///! \param[in] handle The controller (CTRL) handle
///! \param[in] torque_Flux_sf The scale factor to convert torque from (Ld - Lq) * Id * Iq from per unit
to lbin
///! \param[in] torque_Ls_sf The scale factor to convert torque from Flux * Iq from per unit to lbin
356 ///! \return The torque in lbin, in IQ24 format
extern _iq USER_computeTorque_lbin(CTRL_Handle handle, const _iq torque_Flux_sf, const _iq torque_Ls_sf);

#ifdef __cplusplus
}
#endif // extern "C"

361 //@} // ingroup
#endif // end of _USER_H_ definition

```

## B.2. user\_j1.h

```

1 #ifndef _USER_J1_H_
# define _USER_J1_H_
/* ---COPYRIGHT---,BSD
 * Copyright (c) 2012, Texas Instruments Incorporated
 * All rights reserved.
6 *
 * Redistribution and use in source and binary forms, with or without
 * modification, are permitted provided that the following conditions
 * are met:
 *
11 * * Redistributions of source code must retain the above copyright
 * notice, this list of conditions and the following disclaimer.
 *
 * * Redistributions in binary form must reproduce the above copyright
 * notice, this list of conditions and the following disclaimer in the
16 * documentation and/or other materials provided with the distribution.
 *
 * * Neither the name of Texas Instruments Incorporated nor the names of
 * its contributors may be used to endorse or promote products derived
 * from this software without specific prior written permission.
21 *
 * THIS SOFTWARE IS PROVIDED BY THE COPYRIGHT HOLDERS AND CONTRIBUTORS "AS IS"
 * AND ANY EXPRESS OR IMPLIED WARRANTIES, INCLUDING, BUT NOT LIMITED TO,
 * THE IMPLIED WARRANTIES OF MERCHANTABILITY AND FITNESS FOR A PARTICULAR
 * PURPOSE ARE DISCLAIMED. IN NO EVENT SHALL THE COPYRIGHT OWNER OR
26 * CONTRIBUTORS BE LIABLE FOR ANY DIRECT, INDIRECT, INCIDENTAL, SPECIAL,
 * EXEMPLARY, OR CONSEQUENTIAL DAMAGES (INCLUDING, BUT NOT LIMITED TO,
 * PROCUREMENT OF SUBSTITUTE GOODS OR SERVICES; LOSS OF USE, DATA, OR PROFITS;
 * OR BUSINESS INTERRUPTION) HOWEVER CAUSED AND ON ANY THEORY OF LIABILITY,
 * WHETHER IN CONTRACT, STRICT LIABILITY, OR TORT (INCLUDING NEGLIGENCE OR
31 * OTHERWISE) ARISING IN ANY WAY OUT OF THE USE OF THIS SOFTWARE,
 * EVEN IF ADVISED OF THE POSSIBILITY OF SUCH DAMAGE.
 * ---/COPYRIGHT---*/

!!! \file solutions/instaspin_foc/boards/boostxldr8301_revB/f28x/f2806xF/src/user_j1.h
36 !!! \brief Contains the public interface for user initialization data for the CTRL, HAL, and EST modules
!!!
!!! (C) Copyright 2012, Texas Instruments, Inc.

41 // *****
// the includes

!!!
!!!
46 !!! \defgroup USER USER
!!!
!!!@{

51 #ifdef __cplusplus
extern "C" {
#endif

// *****
56 // the defines

!!! \brief CURRENTS AND VOLTAGES
// *****
!!! \brief Defines the full scale frequency for IQ variable, Hz
61 !!! \brief All frequencies are converted into (pu) based on the ratio to this value
!!! \brief WARNING: this value MUST be larger than the maximum speed that you are expecting from the motor
#define USER_IQ_FULL_SCALE_FREQ_Hz (800.0) // 800 Example with buffer for 8-pole 6 KRPM motor to
be run to 10 KRPM with field weakening; Hz =(RPM * Poles) / 120

!!! \brief Defines full scale value for the IQ30 variable of Voltage inside the system
66 !!! \brief All voltages are converted into (pu) based on the ratio to this value
!!! \brief WARNING: this value MUST meet the following condition: USER_IQ_FULL_SCALE_VOLTAGE_V > 0.5 *
USER_MOTOR_MAX_CURRENT * USER_MOTOR_Ls_d * USER_VOLTAGE_FILTER_POLE_rps,
!!! \brief WARNING: otherwise the value can saturate and roll-over, causing an inaccurate value
!!! \brief WARNING: this value is OFTEN greater than the maximum measured ADC value, especially with high
Bemf motors operating at higher than rated speeds
!!! \brief WARNING: if you know the value of your Bemf constant, and you know you are operating at a
multiple speed due to field weakening, be sure to set this value higher than the expected Bemf
voltage
71 !!! \brief It is recommended to start with a value ~3x greater than the USER_ADC_FULL_SCALE_VOLTAGE_V and
increase to 4-5x if scenarios where a Bemf calculation may exceed these limits
!!! \brief This value is also used to calculate the minimum flux value: USER_IQ_FULL_SCALE_VOLTAGE_V/
USER_EST_FREQ_Hz/0.7
#define USER_IQ_FULL_SCALE_VOLTAGE_V (24.0) // 24.0 Example for boostxldr8301_revB typical usage
and the Anaheim motor

```

```

76  /// \brief Defines the maximum voltage at the input to the AD converter
    /// \brief The value that will be represented by the maximum ADC input (3.3V) and conversion (0FFFh)
    /// \brief Hardware dependent, this should be based on the voltage sensing and scaling to the ADC input
    #define USER_ADC_FULL_SCALE_VOLTAGE_V      (26.314) // 26.314 boostxldr8301_revB voltage scaling

    /// \brief Defines the full scale current for the IQ variables, A
    /// \brief All currents are converted into (pu) based on the ratio to this value
    /// \brief WARNING: this value MUST be larger than the maximum current readings that you are expecting
    /// \brief from the motor or the reading will roll over to 0, creating a control issue
    #define USER_IQ_FULL_SCALE_CURRENT_A      (20.0) // 20.0 Example for boostxldr8301_revB typical usage

    /// \brief Defines the maximum current at the AD converter
    /// \brief The value that will be represented by the maximum ADC input (3.3V) and conversion (0FFFh)
    /// \brief Hardware dependent, this should be based on the current sensing and scaling to the ADC input
    #define USER_ADC_FULL_SCALE_CURRENT_A     (33.0) // 33.0 boostxldr8301_revB current scaling

    /// \brief Defines the number of current sensors used
    /// \brief Defined by the hardware capability present
    /// \brief May be (2) or (3)
    #define USER_NUM_CURRENT_SENSORS          (3) // 3 Preferred setting for best performance across full
    /// \brief speed range, allows for 100% duty cycle

    /// \brief Defines the number of voltage (phase) sensors
    /// \brief Must be (3)
    #define USER_NUM_VOLTAGE_SENSORS          (3) // 3 Required

    /// \brief ADC current offsets for A, B, and C phases
    /// \brief One-time hardware dependent, though the calibration can be done at run-time as well
    /// \brief After initial board calibration these values should be updated for your specific hardware so
    /// \brief they are available after compile in the binary to be loaded to the controller
    #define I_A_offset      (0.8331743479)
    #define I_B_offset      (0.8355930448)
    #define I_C_offset      (0.8392037153)

    /// \brief ADC voltage offsets for A, B, and C phases
    /// \brief One-time hardware dependent, though the calibration can be done at run-time as well
    /// \brief After initial board calibration these values should be updated for your specific hardware so
    /// \brief they are available after compile in the binary to be loaded to the controller
    #define V_A_offset      (0.5271264911)
    #define V_B_offset      (0.5257175565)
    #define V_C_offset      (0.5249399543)

    /// \brief CLOCKS & TIMERS
    /// *****
    /// \brief Defines the Pulse Width Modulation (PWM) frequency, kHz
    /// \brief PWM frequency can be set directly here up to 30 KHz safely (60 KHz MAX in some cases)
    /// \brief For higher PWM frequencies (60 KHz+ typical for low inductance, high current ripple motors) it
    /// \brief is recommended to use the ePWM hardware
    /// \brief and adjustable ADC SOC to decimate the ADC conversion done interrupt to the control system, or
    /// \brief to use the software Que example.
    /// \brief Otherwise you risk missing interrupts and disrupting the timing of the control state machine
    #define USER_PWM_FREQ_kHz      (45.0) //30.0 Example, 8.0 – 30.0 KHz typical; 45–80 KHz may be
    /// \brief required for very low inductance, high speed motors

    /// \brief Defines the maximum Voltage vector (Vs) magnitude allowed. This value sets the maximum
    /// \brief magnitude for the output of the
    /// \brief Id and Iq PI current controllers. The Id and Iq current controller outputs are Vd and Vq.
    /// \brief The relationship between Vs, Vd, and Vq is: Vs = sqrt(Vd^2 + Vq^2). In this FOC controller,
    /// \brief the
    #define USER_MAX_VS_MAG_PU      (0.5) // Set to 0.5 if a current reconstruction technique is not used
    /// \brief Vd value is set equal to USER_MAX_VS_MAG*USER_VD_MAG_FACTOR. Vq = sqrt(USER_MAX_VS_MAG^2 - Vd
    /// \brief ^2).
    /// \brief Set USER_MAX_VS_MAG = 0.5 for a pure sinewave with a peak at SQRT(3)/2 = 86.6% duty cycle. No
    /// \brief current reconstruction is needed for this scenario.
    /// \brief Set USER_MAX_VS_MAG = 1/SQRT(3) = 0.5774 for a pure sinewave with a peak at 100% duty cycle.
    /// \brief Current reconstruction will be needed for this scenario (Lab10a-x).
    /// \brief Set USER_MAX_VS_MAG = 2/3 = 0.6666 to create a trapezoidal voltage waveform. Current
    /// \brief reconstruction will be needed for this scenario (Lab10a-x).
    /// \brief For space vector over-modulation, see lab 10 for details on system requirements that will allow
    /// \brief the SVM generator to go all the way to trapezoidal.
    /// \brief Typically the PWM Frequency triggers (can be decimated by the ePWM hardware for less overhead)
    #define USER_MAX_VS_MAG_PU      (0.5) // Set to 0.5 if a current reconstruction technique is not used
    /// \brief . Look at the module svgen_current in lab10a-x for more info.

    /// \brief DECIMATION
    /// *****
    /// \brief Defines the number of pwm clock ticks per isr clock tick
    /// \brief Note: Valid values are 1, 2 or 3 only
    #define USER_NUM_PWM_TICKS_PER_ISR_TICK    (3)

    /// \brief Defines the number of isr ticks (hardware) per controller clock tick (software)
    /// \brief Controller clock tick (CTRL) is the main clock used for all timing in the software
    /// \brief Typically the PWM Frequency triggers (can be decimated by the ePWM hardware for less overhead)

```

```

    an ADC SOC
    /// \brief ADC SOC triggers an ADC Conversion Done
    /// \brief ADC Conversion Done triggers ISR
    /// \brief This relates the hardware ISR rate to the software controller rate
146 /// \brief Typically want to consider some form of decimation (ePWM hardware, CURRENT or EST) over 16KHz
    ISR to insure interrupt completes and leaves time for background tasks
    #define USER_NUM_ISR_TICKS_PER_CTRL_TICK    (1)    // 2 Example, controller clock rate (CTRL) runs at
    PWM / 2; ex 30 KHz PWM, 15 KHz control

    /// \brief Defines the number of controller clock ticks per current controller clock tick
    /// \brief Relationship of controller clock rate to current controller (FOC) rate
151 #define USER_NUM_CTRL_TICKS_PER_CURRENT_TICK    (1)    // 1 Typical, Forward FOC current controller (Iq/
    Id/IPARK/SVPWM) runs at same rate as CTRL.

    /// \brief Defines the number of controller clock ticks per estimator clock tick
    /// \brief Relationship of controller clock rate to estimator (FAST) rate
    /// \brief Depends on needed dynamic performance, FAST provides very good results as low as 1 KHz while
    more dynamic or high speed applications may require up to 15 KHz
156 #define USER_NUM_CTRL_TICKS_PER_EST_TICK    (1)    // 1 Typical, FAST estimator runs at same rate as
    CTRL;

    /// \brief Defines the number of controller clock ticks per speed controller clock tick
    /// \brief Relationship of controller clock rate to speed loop rate
    #define USER_NUM_CTRL_TICKS_PER_SPEED_TICK    (15)    // 15 Typical to match PWM, ex: 15KHz PWM, controller,
    and current loop, 1KHz speed loop
161

    /// \brief Defines the number of controller clock ticks per trajectory clock tick
    /// \brief Relationship of controller clock rate to trajectory loop rate
    /// \brief Typically the same as the speed rate
    #define USER_NUM_CTRL_TICKS_PER_TRAJ_TICK    (15)    // 15 Typical to match PWM, ex: 10KHz controller &
    current loop, 1KHz speed loop, 1 KHz Trajectory
166

    /// \brief LIMITS
    /// *****
    /// \brief Defines the maximum negative current to be applied in Id reference
171 /// \brief Used in field weakening only, this is a safety setting (e.g. to protect against demagnetization
    )
    /// \brief User must also be aware that overall current magnitude [sqrt(Id^2 + Iq^2)] should be kept below
    any machine design specifications
    #define USER_MAX_NEGATIVE_ID_REF_CURRENT_A    (-0.5 * USER_MOTOR_MAX_CURRENT)    // -0.5 *
    USER_MOTOR_MAX_CURRENT Example, adjust to meet safety needs of your motor

    /// \brief Defines the R/L estimation frequency, Hz
176 /// \brief User higher values for low inductance motors and lower values for higher inductance
    /// \brief motors. The values can range from 100 to 300 Hz.
    #define USER_R_OVER_L_EST_FREQ_Hz    (300)    // 300 Default

    /// \brief Defines the low speed limit for the flux integrator, pu
181 /// \brief This is the speed range (CW/CCW) at which the ForceAngle object is active, but only if Enabled
    /// \brief Outside of this speed – or if Disabled – the ForcAngle will NEVER be active and the angle is
    provided by FAST only
    #define USER_ZEROSPEEDLIMIT    (0.5 / USER_IQ_FULL_SCALE_FREQ_Hz)    // 0.002 pu, 1–5 Hz typical; Hz =
    USER_ZEROSPEEDLIMIT * USER_IQ_FULL_SCALE_FREQ_Hz

    /// \brief Defines the force angle frequency, Hz
186 /// \brief Frequency of stator vector rotation used by the ForceAngle object
    /// \brief Can be positive or negative
    #define USER_FORCE_ANGLE_FREQ_Hz    (2.0 * USER_ZEROSPEEDLIMIT * USER_IQ_FULL_SCALE_FREQ_Hz)    // 1.0
    Typical force angle start-up speed

191 /// \brief POLES
    /// *****
    /// \brief Defines the analog voltage filter pole location, Hz
    /// \brief Must match the hardware filter for Vph
196 #define USER_VOLTAGE_FILTER_POLE_Hz    (364.682)    // 364.682, value for boostIdrv8301_revB hardware

    /// \brief USER MOTOR & ID SETTINGS
    /// *****

201 /// \brief Define each motor with a unique name and ID number
    /// BLDC & SMPM motors
    #define Estun_EMJ_04APB22    101
    #define Anaheim_BLY172S    102
    #define Tamagawa_A0100    103
206 #define Teknic_M2310PLN04K    104
    #define Drone_A2212_1000KV    105
    #define Drone_A2313_960KV    106

    /// IPM motors
211 /// If user provides separate Ls-d, Ls-q
    /// else treat as SPM with user or identified average Ls

```

```

#define Belt_Drive_Washer_IPM          201
#define Anaheim_Salient                202

216 // ACIM motors
#define Marathon_5K33GN2A             301

    /// \brief Uncomment the motor which should be included at compile
    /// \brief These motor ID settings and motor parameters are then available to be used by the control
    system
221 /// \brief Once your ideal settings and parameters are identified update the motor section here so it is
    available in the binary code
    ///#define USER_MOTOR Estun_EMJ_04APB22
#define USER_MOTOR Anaheim_BLY172S
    ///#define USER_MOTOR Tamagawa_A0100
    ///#define USER_MOTOR Drone_A2313_960KV
226 ///#define USER_MOTOR Teknic_M2310PLN04K
    ///#define USER_MOTOR Belt_Drive_Washer_IPM
    ///#define USER_MOTOR Marathon_5K33GN2A
    ///#define USER_MOTOR Anaheim_Salient

231 #if (USER_MOTOR == Estun_EMJ_04APB22)
#define USER_MOTOR_TYPE                MOTOR_Type_Pm      // Name must match the motor #define
    , IPM) or Motor_Type_Induction (Asynchronous ACI) // Motor_Type_Pm (All Synchronous: BLDC, PMSM, SMPM)
#define USER_MOTOR_NUM_POLE_PAIRS     (4)                // PAIRS, not total poles. Used to calculate user
    RPM from rotor Hz only
#define USER_MOTOR_Rr                  (NULL)             // Induction motors only, else NULL
236 #define USER_MOTOR_Rs                  (2.303403)         // Identified phase to neutral resistance in a Y
    equivalent circuit (Ohms, float)
#define USER_MOTOR_Ls_d                (0.008464367)      // For PM, Identified average stator inductance (
    Henry, float)
#define USER_MOTOR_Ls_q                (0.008464367)      // For PM, Identified average stator inductance (
    Henry, float)
#define USER_MOTOR_RATED_FLUX          (0.38)            // Identified TOTAL flux linkage between the rotor
    and the stator (V/Hz)
#define USER_MOTOR_MAGNETIZING_CURRENT (NULL)            // Induction motors only, else NULL
241 #define USER_MOTOR_RES_EST_CURRENT     (1.0)             // During Motor ID, maximum current (Amperes, float
    ) used for Rs estimation, 10-20% rated current
#define USER_MOTOR_IND_EST_CURRENT     (-1.0)            // During Motor ID, maximum current (negative
    Amperes, float) used for Ls estimation, use just enough to enable rotation
#define USER_MOTOR_MAX_CURRENT         (3.82)            // CRITICAL: Used during ID and run-time, sets a
    limit on the maximum current command output of the provided Speed PI Controller to the Iq controller
#define USER_MOTOR_FLUX_EST_FREQ_Hz    (20.0)            // During Motor ID, maximum commanded speed (Hz,
    float), ~10% rated

246 #elif (USER_MOTOR == Anaheim_BLY172S)
#define USER_MOTOR_TYPE                MOTOR_Type_Pm
#define USER_MOTOR_NUM_POLE_PAIRS     (4)
#define USER_MOTOR_Rr                  (NULL)
#define USER_MOTOR_Rs                  (0.4110007)
251 #define USER_MOTOR_Ls_d                (0.0007092811)
#define USER_MOTOR_Ls_q                (0.0007092811)
#define USER_MOTOR_RATED_FLUX          (0.03279636)
#define USER_MOTOR_MAGNETIZING_CURRENT (NULL)
#define USER_MOTOR_RES_EST_CURRENT     (1.0)
256 #define USER_MOTOR_IND_EST_CURRENT     (-1.0)
#define USER_MOTOR_MAX_CURRENT         (5.0)
#define USER_MOTOR_FLUX_EST_FREQ_Hz    (20.0)
#define IPD_HFI_EXC_FREQ_HZ             (750.0)           // excitation frequency, Hz
#define IPD_HFI_LP_SPD_FILT_HZ         (35.0)           // lowpass filter cutoff frequency, Hz
#define IPD_HFI_HP_IQ_FILT_HZ          (100.0)          // highpass filter cutoff frequency, Hz
261 #define IPD_HFI_KSPD                   (15.0)           // the speed gain value
#define IPD_HFI_EXC_MAG_COARSE_PU       (0.13)           // coarse IPD excitation magnitude, pu
#define IPD_HFI_EXC_MAG_FINE_PU        (0.12)           // fine IPD excitation magnitude, pu
#define IPD_HFI_EXC_TIME_COARSE_S      (0.5)            // coarse wait time, sec max 0.64
266 #define IPD_HFI_EXC_TIME_FINE_S        (0.5)            // fine wait time, sec max 0.4
#define AFSEL_FREQ_HIGH_PU              (_IQ(15.0 / USER_IQ_FULL_SCALE_FREQ_Hz))
#define AFSEL_FREQ_LOW_PU               (_IQ(10.0 / USER_IQ_FULL_SCALE_FREQ_Hz))
#define AFSEL_IQ_SLOPE_EST              (_IQ((float)(1.0/0.1/USER_ISR_FREQ_Hz)))
#define AFSEL_IQ_SLOPE_HFI              (_IQ((float)(1.0/10.0/USER_ISR_FREQ_Hz)))
271 #define AFSEL_IQ_SLOPE_THROTTLE_DWN    (_IQ((float)(1.0/0.05/USER_ISR_FREQ_Hz)))
#define AFSEL_MAX_IQ_REF_EST            (_IQ(0.6))
#define AFSEL_MAX_IQ_REF_HFI            (_IQ(0.6))

#define USER_MOTOR_FREQ_LOW             (10.0)           // Hz - suggested to set
    to 10% of rated motor frequency
276 #define USER_MOTOR_FREQ_HIGH           (100.0)          // Hz - suggested to set to 100%
    of rated motor frequency
#define USER_MOTOR_FREQ_MAX            (120.0)          // Hz - suggested to set
    to 120% of rated motor frequency
#define USER_MOTOR_VOLT_MIN             (3.0)            // Volt - suggested to set
    to 15% of rated motor voltage
#define USER_MOTOR_VOLT_MAX            (18.0)           // Volt - suggested to set
    to 100% of rated motor voltage

```

```

281 #elif (USER_MOTOR == Tamagawa_A0100)
#define USER_MOTOR_TYPE MOTOR_Type_Pm
#define USER_MOTOR_NUM_POLE_PAIRS (4)
#define USER_MOTOR_Rr (NULL)
#define USER_MOTOR_Rs (0.262230158)
286 #define USER_MOTOR_Ls_d (0.000459346687)
#define USER_MOTOR_Ls_q (0.000459346687)
#define USER_MOTOR_RATED_FLUX (0.0484918393)
#define USER_MOTOR_MAGNETIZING_CURRENT (NULL)
#define USER_MOTOR_RES_EST_CURRENT (1.0)
291 #define USER_MOTOR_IND_EST_CURRENT (-1.0)
#define USER_MOTOR_MAX_CURRENT (5.0)
#define USER_MOTOR_FLUX_EST_FREQ_Hz (20.0)
#define IPD_HFI_EXC_FREQ_HZ (750.0) // excitation frequency, Hz
#define IPD_HFI_LP_SPD_FILT_HZ (35.0) // lowpass filter cutoff frequency, Hz
296 #define IPD_HFI_HP_IQ_FILT_HZ (100.0) // highpass filter cutoff frequency, Hz
#define IPD_HFI_KSPD (15.0) // the speed gain value
#define IPD_HFI_EXC_MAG_COARSE_PU (0.13) // coarse IPD excitation magnitude, pu
#define IPD_HFI_EXC_MAG_FINE_PU (0.12) // fine IPD excitation magnitude, pu
#define IPD_HFI_EXC_TIME_COARSE_S (0.5) // coarse wait time, sec max 0.64
301 #define IPD_HFI_EXC_TIME_FINE_S (0.5) // fine wait time, sec max 0.4
#define AFSEL_FREQ_HIGH_PU (_IQ(15.0 / USER_IQ_FULL_SCALE_FREQ_Hz))
#define AFSEL_FREQ_LOW_PU (_IQ(10.0 / USER_IQ_FULL_SCALE_FREQ_Hz))
#define AFSEL_IQ_SLOPE_EST (_IQ((float)(1.0/0.1/USER_ISR_FREQ_Hz)))
#define AFSEL_IQ_SLOPE_HFI (_IQ((float)(1.0/10.0/USER_ISR_FREQ_Hz)))
306 #define AFSEL_IQ_SLOPE_THROTTLE_DWN (_IQ((float)(1.0/0.05/USER_ISR_FREQ_Hz)))
#define AFSEL_MAX_IQ_REF_EST (_IQ(0.6))
#define AFSEL_MAX_IQ_REF_HFI (_IQ(0.6))

#elif (USER_MOTOR == Drone_A2212_1000KV)
311 #define USER_MOTOR_TYPE MOTOR_Type_Pm
#define USER_MOTOR_NUM_POLE_PAIRS (4)
#define USER_MOTOR_Rr (NULL)
#define USER_MOTOR_Rs (0.4110007)
#define USER_MOTOR_Ls_d (0.0007092811)
316 #define USER_MOTOR_Ls_q (0.0007092811)
#define USER_MOTOR_RATED_FLUX (0.03279636)
#define USER_MOTOR_MAGNETIZING_CURRENT (NULL)
#define USER_MOTOR_RES_EST_CURRENT (1.0)
#define USER_MOTOR_IND_EST_CURRENT (-1.0)
321 #define USER_MOTOR_MAX_CURRENT (5.0)
#define USER_MOTOR_FLUX_EST_FREQ_Hz (20.0)
#define IPD_HFI_EXC_FREQ_HZ (750.0) // excitation frequency, Hz
#define IPD_HFI_LP_SPD_FILT_HZ (35.0) // lowpass filter cutoff frequency, Hz
#define IPD_HFI_HP_IQ_FILT_HZ (100.0) // highpass filter cutoff frequency, Hz
326 #define IPD_HFI_KSPD (15.0) // the speed gain value
#define IPD_HFI_EXC_MAG_COARSE_PU (0.13) // coarse IPD excitation magnitude, pu
#define IPD_HFI_EXC_MAG_FINE_PU (0.12) // fine IPD excitation magnitude, pu
#define IPD_HFI_EXC_TIME_COARSE_S (0.5) // coarse wait time, sec max 0.64
#define IPD_HFI_EXC_TIME_FINE_S (0.5) // fine wait time, sec max 0.4
331 #define AFSEL_FREQ_HIGH_PU (_IQ(15.0 / USER_IQ_FULL_SCALE_FREQ_Hz))
#define AFSEL_FREQ_LOW_PU (_IQ(10.0 / USER_IQ_FULL_SCALE_FREQ_Hz))
#define AFSEL_IQ_SLOPE_EST (_IQ((float)(1.0/0.1/USER_ISR_FREQ_Hz)))
#define AFSEL_IQ_SLOPE_HFI (_IQ((float)(1.0/10.0/USER_ISR_FREQ_Hz)))
#define AFSEL_IQ_SLOPE_THROTTLE_DWN (_IQ((float)(1.0/0.05/USER_ISR_FREQ_Hz)))
336 #define AFSEL_MAX_IQ_REF_EST (_IQ(0.6))
#define AFSEL_MAX_IQ_REF_HFI (_IQ(0.6))

#elif (USER_MOTOR == Drone_A2313_960KV)
#define USER_MOTOR_TYPE MOTOR_Type_Pm
341 #define USER_MOTOR_NUM_POLE_PAIRS (4)
#define USER_MOTOR_Rr (NULL)
#define USER_MOTOR_Rs (0.4110007)
#define USER_MOTOR_Ls_d (0.0007092811)
#define USER_MOTOR_Ls_q (0.0007092811)
346 #define USER_MOTOR_RATED_FLUX (0.03279636)
#define USER_MOTOR_MAGNETIZING_CURRENT (NULL)
#define USER_MOTOR_RES_EST_CURRENT (1.0)
#define USER_MOTOR_IND_EST_CURRENT (-1.0)
#define USER_MOTOR_MAX_CURRENT (5.0)
351 #define USER_MOTOR_FLUX_EST_FREQ_Hz (20.0)
#define IPD_HFI_EXC_FREQ_HZ (750.0) // excitation frequency, Hz
#define IPD_HFI_LP_SPD_FILT_HZ (35.0) // lowpass filter cutoff frequency, Hz
#define IPD_HFI_HP_IQ_FILT_HZ (100.0) // highpass filter cutoff frequency, Hz
#define IPD_HFI_KSPD (15.0) // the speed gain value
356 #define IPD_HFI_EXC_MAG_COARSE_PU (0.13) // coarse IPD excitation magnitude, pu
#define IPD_HFI_EXC_MAG_FINE_PU (0.12) // fine IPD excitation magnitude, pu
#define IPD_HFI_EXC_TIME_COARSE_S (0.5) // coarse wait time, sec max 0.64
#define IPD_HFI_EXC_TIME_FINE_S (0.5) // fine wait time, sec max 0.4
#define AFSEL_FREQ_HIGH_PU (_IQ(15.0 / USER_IQ_FULL_SCALE_FREQ_Hz))
#define AFSEL_FREQ_LOW_PU (_IQ(10.0 / USER_IQ_FULL_SCALE_FREQ_Hz))
361 #define AFSEL_IQ_SLOPE_EST (_IQ((float)(1.0/0.1/USER_ISR_FREQ_Hz)))
#define AFSEL_IQ_SLOPE_HFI (_IQ((float)(1.0/10.0/USER_ISR_FREQ_Hz)))

```



```

#define AFSEL_IQ_SLOPE_THROTTLE_DWN (_IQ((float)(1.0/0.05/USER_ISR_FREQ_Hz)))
#define AFSEL_MAX_IQ_REF_EST (_IQ(0.6))
366 #define AFSEL_MAX_IQ_REF_HFI (_IQ(0.6))

# elif (USER_MOTOR == Anaheim_Salient) // When using IPD_HFI, set decimation to 1 and PWM
  to 15.0 KHz
#define USER_MOTOR_TYPE MOTOR_Type_Pm
#define USER_MOTOR_NUM_POLE_PAIRS (4)
371 #define USER_MOTOR_Rr (NULL)
#define USER_MOTOR_Rs (0.1215855)
#define USER_MOTOR_Ls_d (0.0002298828)
#define USER_MOTOR_Ls_q (0.0002298828)
376 #define USER_MOTOR_RATED_FLUX (0.04821308)
#define USER_MOTOR_MAGNETIZING_CURRENT (NULL)
#define USER_MOTOR_RES_EST_CURRENT (2.0) // Enter amperes(float)
#define USER_MOTOR_IND_EST_CURRENT (-0.5) // Enter negative amperes(float)
#define USER_MOTOR_MAX_CURRENT (10.0)
#define USER_MOTOR_FLUX_EST_FREQ_Hz (20.0)
381 #define IPD_HFI_EXC_FREQ_HZ (750.0) // excitation frequency, Hz
#define IPD_HFI_LP_SPD_FILT_HZ (35.0) // lowpass filter cutoff frequency, Hz
#define IPD_HFI_HP_IQ_FILT_HZ (100.0) // highpass filter cutoff frequency, Hz
#define IPD_HFI_KSPD (15.0) // the speed gain value
#define IPD_HFI_EXC_MAG_COARSE_PU (0.13) // coarse IPD excitation magnitude, pu
386 #define IPD_HFI_EXC_MAG_FINE_PU (0.12) // fine IPD excitation magnitude, pu
#define IPD_HFI_EXC_TIME_COARSE_S (0.5) // coarse wait time, sec max 0.64
#define IPD_HFI_EXC_TIME_FINE_S (0.5) // fine wait time, sec max 0.4
#define AFSEL_FREQ_HIGH_PU (_IQ(15.0 / USER_IQ_FULL_SCALE_FREQ_Hz))
#define AFSEL_FREQ_LOW_PU (_IQ(10.0 / USER_IQ_FULL_SCALE_FREQ_Hz))
391 #define AFSEL_IQ_SLOPE_EST (_IQ((float)(1.0/0.1/USER_ISR_FREQ_Hz)))
#define AFSEL_IQ_SLOPE_HFI (_IQ((float)(1.0/10.0/USER_ISR_FREQ_Hz)))
#define AFSEL_IQ_SLOPE_THROTTLE_DWN (_IQ((float)(1.0/0.05/USER_ISR_FREQ_Hz)))
#define AFSEL_MAX_IQ_REF_EST (_IQ(0.6))
#define AFSEL_MAX_IQ_REF_HFI (_IQ(0.6))
396

# elif (USER_MOTOR == Teknic_M2310PLN04K)
#define USER_MOTOR_TYPE MOTOR_Type_Pm
#define USER_MOTOR_NUM_POLE_PAIRS (4)
#define USER_MOTOR_Rr (NULL)
401 #define USER_MOTOR_Rs (0.3918252)
#define USER_MOTOR_Ls_d (0.00023495)
#define USER_MOTOR_Ls_q (0.00023495)
#define USER_MOTOR_RATED_FLUX (0.03955824)
#define USER_MOTOR_MAGNETIZING_CURRENT (NULL)
406 #define USER_MOTOR_RES_EST_CURRENT (1.0)
#define USER_MOTOR_IND_EST_CURRENT (-0.5)
#define USER_MOTOR_MAX_CURRENT (7.0)
#define USER_MOTOR_FLUX_EST_FREQ_Hz (20.0)

411 # elif (USER_MOTOR == Belt_Drive_Washer_IPM)
#define USER_MOTOR_TYPE MOTOR_Type_Pm
#define USER_MOTOR_NUM_POLE_PAIRS (4)
#define USER_MOTOR_Rr (NULL)
#define USER_MOTOR_Rs (2.832002)
416 #define USER_MOTOR_Ls_d (0.0115)
#define USER_MOTOR_Ls_q (0.0135)
#define USER_MOTOR_RATED_FLUX (0.5022156)
#define USER_MOTOR_MAGNETIZING_CURRENT (NULL)
#define USER_MOTOR_RES_EST_CURRENT (1.0)
421 #define USER_MOTOR_IND_EST_CURRENT (-1.0)
#define USER_MOTOR_MAX_CURRENT (4.0)
#define USER_MOTOR_FLUX_EST_FREQ_Hz (20.0)

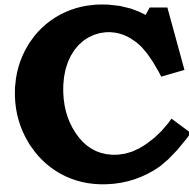
# elif (USER_MOTOR == Marathon_5K33GN2A) // Name must match the motor #define
426 #define USER_MOTOR_TYPE MOTOR_Type_Induction // Motor_Type_Pm (All Synchronous: BLDC, PMSM
, SMPM, IPM) or Motor_Type_Induction (Asynchronous ACI)
#define USER_MOTOR_NUM_POLE_PAIRS (2) // PAIRS, not total poles. Used to calculate
user RPM from rotor Hz only
#define USER_MOTOR_Rr (5.508003) // Identified phase to neutral in a Y
equivalent circuit (Ohms, float)
#define USER_MOTOR_Rs (10.71121) // Identified phase to neutral in a Y
equivalent circuit (Ohms, float)
#define USER_MOTOR_Ls_d (0.05296588) // For Induction, Identified average stator
inductance (Henry, float)
431 #define USER_MOTOR_Ls_q (0.05296588) // For Induction, Identified average stator
inductance (Henry, float)
#define USER_MOTOR_RATED_FLUX (0.8165*220.0/60.0) // sqrt(2/3)* Rated V (line-line) / Rated
Freq (Hz)
#define USER_MOTOR_MAGNETIZING_CURRENT (1.378) // Identified magnetizing current for
induction motors, else NULL
#define USER_MOTOR_RES_EST_CURRENT (0.5) // During Motor ID, maximum current (Amperes,
float) used for Rs estimation, 10-20% rated current
#define USER_MOTOR_IND_EST_CURRENT (NULL) // not used for induction
436 #define USER_MOTOR_MAX_CURRENT (2.0) // CRITICAL: Used during ID and run-time,
sets a limit on the maximum current command output of the provided Speed PI Controller to the Iq

```

```
        controller
#define USER_MOTOR_FLUX_EST_FREQ_Hz    (5.0)           // During Motor ID, maximum commanded speed (
        Hz, float). Should always use 5 Hz for Induction.

#else
#error No motor type specified
441 #endif

#ifdef __cplusplus
}
#endif // extern "C"
446 //@} // ingroup
#endif // end of _USER_J1_H_ definition
```



## proj\_lab11a.c

```
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31 * ---/COPYRIGHT---*/
  ///! \file solutions/instaspin_foc/src/proj_lab011a.c
  ///! \brief A Feature Rich Example without Controller Module
  ///!
  ///! (C) Copyright 2015, Texas Instruments, Inc.
36
  ///! \defgroup PROJ_LAB11A PROJ_LAB11A
  ///@{

  ///! \defgroup PROJ_LAB11A_OVERVIEW Project Overview
41 ///!
  ///! A Feature Rich Example without Controller Module
  ///!

  // *****
46 // the includes

  // system includes
  #include <math.h>
  #include "main.h"
51
  #ifndef FLASH
  #pragma CODE_SECTION(mainISR,"ramfuncs");
  #pragma CODE_SECTION(runSetTrigger,"ramfuncs");
  #pragma CODE_SECTION(runFieldWeakening,"ramfuncs");
56 #pragma CODE_SECTION(runCurrentReconstruction,"ramfuncs");
  #pragma CODE_SECTION(angleDelayComp,"ramfuncs");
  #endif
```

```

// Include header files used in the main function
61 // *****
// the defines
// *****
66 // the globals

CLARKE_Handle  clarkeHandle_I;          //!< the handle for the current Clarke transform
CLARKE_Obj     clarke_I;                //!< the current Clarke transform object

71 CLARKE_Handle  clarkeHandle_V;        //!< the handle for the voltage Clarke transform
CLARKE_Obj     clarke_V;                //!< the voltage Clarke transform object

CPU_USAGE_Handle  cpu_usageHandle;
CPU_USAGE_Obj     cpu_usage;

76 EST_Handle     estHandle;             //!< the handle for the estimator

FW_Handle        fwHandle;
FW_Obj           fw;

81 PID_Obj        pid[3];                //!< three handles for PID controllers 0 – Speed, 1 – Id, 2
    - Iq
PID_Handle       pidHandle[3];          //!< three objects for PID controllers 0 – Speed, 1 – Id, 2
    - Iq
uint16_t         pidCntSpeed;           //!< count variable to decimate the execution of the speed
    PID controller

86 IPARK_Handle  iparkHandle;           //!< the handle for the inverse Park transform
IPARK_Obj        ipark;                 //!< the inverse Park transform object

FILTER_FO_Handle  filterHandle[6];      //!< the handles for the 3–current and 3–voltage filters for
    offset calculation
FILTER_FO_Obj     filter[6];           //!< the 3–current and 3–voltage filters for offset
    calculation

91 SVGENCURRENT_Obj  svgencurrent;
SVGENCURRENT_Handle  svgencurrentHandle;

SVGEN_Handle      svgenHandle;          //!< the handle for the space vector generator
96 SVGEN_Obj       svgen;               //!< the space vector generator object

TRAJ_Handle       trajHandle_Id;        //!< the handle for the id reference trajectory
TRAJ_Obj          traj_Id;              //!< the id reference trajectory object

101 TRAJ_Handle    trajHandle_spd;       //!< the handle for the speed reference trajectory
TRAJ_Obj          traj_spd;             //!< the speed reference trajectory object

#ifdef CSM_ENABLE
#pragma DATA_SECTION(halHandle, "rom_accessed_data");
106 #endif
HAL_Handle        halHandle;            //!< the handle for the hardware abstraction layer (HAL)

HAL_PwmData_t     gPwmData = {_IQ(0.0), _IQ(0.0), _IQ(0.0)};    //!< contains the three pwm values –1.0 –
    0%, 1.0 – 100%

111 HAL_AdcData_t  gAdcData;             //!< contains three current values, three voltage values and
    one DC buss value

MATH_vec3         gOffsets_I_pu = {_IQ(0.0), _IQ(0.0), _IQ(0.0)};    //!< contains the offsets for the current
    feedback

MATH_vec3         gOffsets_V_pu = {_IQ(0.0), _IQ(0.0), _IQ(0.0)};    //!< contains the offsets for the voltage
    feedback

116 MATH_vec2       gIdq_ref_pu = {_IQ(0.0), _IQ(0.0)};             //!< contains the Id and Iq references

MATH_vec2         gVdq_out_pu = {_IQ(0.0), _IQ(0.0)};             //!< contains the output Vd and Vq from
    the current controllers

121 MATH_vec2       gIdq_pu = {_IQ(0.0), _IQ(0.0)};                 //!< contains the Id and Iq measured
    values

#ifdef CSM_ENABLE
#pragma DATA_SECTION(gUserParams, "rom_accessed_data");
126 #endif
USER_Params       gUserParams;

volatile MOTOR_Vars_t gMotorVars = MOTOR_Vars_INIT;    //!< the global motor variables that are defined in
    main.h and used for display in the debugger's watch window

#ifdef FLASH
131 // Used for running BackGround in flash, and ISR in RAM

```

```

extern uint16_t *RamfuncsLoadStart, *RamfuncsLoadEnd, *RamfuncsRunStart;

#ifdef CSM_ENABLE
extern uint16_t *econst_start, *econst_end, *econst_ram_load;
136 extern uint16_t *switch_start, *switch_end, *switch_ram_load;
#endif
#endif

141 MATH_vec3 gIavg = {_IQ(0.0), _IQ(0.0), _IQ(0.0)};
uint16_t gIavg_shift = 1;
MATH_vec3 gPwmData_prev = {_IQ(0.0), _IQ(0.0), _IQ(0.0)};

#ifdef DRV8301_SPI
146 // Watch window interface to the 8301 SPI
DRV_SPI_8301_Vars_t gDrvSpi8301Vars;
#endif

#ifdef DRV8305_SPI
151 // Watch window interface to the 8305 SPI
DRV_SPI_8305_Vars_t gDrvSpi8305Vars;
#endif

_iq gFlux_pu_to_Wb_sf;
156 _iq gFlux_pu_to_VpHz_sf;

_iq gTorque_Ls_Id_Iq_pu_to_Nm_sf;
161 _iq gTorque_Flux_Iq_pu_to_Nm_sf;

_iq gSpeed_krpm_to_pu_sf = _IQ(((float_t)USER_MOTOR_NUM_POLE_PAIRS * 1000.0 / (USER_IQ_FULL_SCALE_FREQ_Hz *
60.0)));

_iq gSpeed_hz_to_krpm_sf = _IQ(60.0 / ((float_t)USER_MOTOR_NUM_POLE_PAIRS / 1000.0));
166 _iq gIs_Max_squared_pu = _IQ((USER_MOTOR_MAX_CURRENT * USER_MOTOR_MAX_CURRENT) / (
USER_IQ_FULL_SCALE_CURRENT_A * USER_IQ_FULL_SCALE_CURRENT_A));

float_t gCpuUsagePercentageMin = 0.0;
float_t gCpuUsagePercentageAvg = 0.0;
171 float_t gCpuUsagePercentageMax = 0.0;

uint32_t gOffsetCalcCount = 0;

uint16_t gTrjCnt = 0;
176 volatile bool gFlag_enableRsOnLine = false;

volatile bool gFlag_updateRs = false;

181 volatile _iq gRsOnLineFreq_Hz = _IQ(0.2);

volatile _iq gRsOnLineId_mag_A = _IQ(0.5);

volatile _iq gRsOnLinePole_Hz = _IQ(0.2);
186 // *****
// the functions
void main(void)
{
191 // Only used if running from FLASH
// Note that the variable FLASH is defined by the project
#ifdef FLASH
// Copy time critical code and Flash setup code to RAM
// The RamfuncsLoadStart, RamfuncsLoadEnd, and RamfuncsRunStart
// symbols are created by the linker. Refer to the linker files.
196 memCopy((uint16_t *)&RamfuncsLoadStart,(uint16_t *)&RamfuncsLoadEnd,(uint16_t *)&RamfuncsRunStart);

#ifdef CSM_ENABLE
//copy .econst to unsecure RAM
201 if(*econst_end - *econst_start)
{
memCopy((uint16_t *)&econst_start,(uint16_t *)&econst_end,(uint16_t *)&econst_ram_load);
}

206 //copy .switch ot unsecure RAM
if(*switch_end - *switch_start)
{
memCopy((uint16_t *)&switch_start,(uint16_t *)&switch_end,(uint16_t *)&switch_ram_load);
}

211 #endif
#endif

```

```

// initialize the hardware abstraction layer
halHandle = HAL_init(&hal, sizeof(hal));
216 // check for errors in user parameters
USER_checkForErrors(&gUserParams);

221 // store user parameter error in global variable
gMotorVars.UserErrorCode = USER_getErrorCode(&gUserParams);

// do not allow code execution if there is a user parameter error
226 if(gMotorVars.UserErrorCode != USER_ErrorCode_NoError)
{
    for(;;)
    {
        gMotorVars.Flag_enableSys = false;
231    }
}

// initialize the Clarke modules
clarkeHandle_I = CLARKE_init(&clarke_I, sizeof(clarke_I));
236 clarkeHandle_V = CLARKE_init(&clarke_V, sizeof(clarke_V));

// initialize the estimator
estHandle = EST_init((void *)USER_EST_HANDLE_ADDRESS, 0x200);

241 // initialize the user parameters
USER_setParams(&gUserParams);

// set the hardware abstraction layer parameters
HAL_setParams(halHandle, &gUserParams);

246 #ifdef FAST_ROM_V1p6
{
    CTRL_Handle ctrlHandle = CTRL_init((void *)USER_CTRL_HANDLE_ADDRESS, 0x200);
    CTRL_Obj *obj = (CTRL_Obj *)ctrlHandle;
251 obj->estHandle = estHandle;

    // initialize the estimator through the controller
    CTRL_setParams(ctrlHandle, &gUserParams);
    CTRL_setUserMotorParams(ctrlHandle);
256 CTRL_setupEstIdleState(ctrlHandle);
}
#else
{
    // initialize the estimator
261 EST_setEstParams(estHandle, &gUserParams);
    EST_setupEstIdleState(estHandle);
}
#endif

266 // disable Rs recalculation by default
gMotorVars.Flag_enableRsRecalc = true;
EST_setFlag_enableRsRecalc(estHandle, false);

// configure RsOnLine
271 EST_setFlag_enableRsOnLine(estHandle, gFlag_enableRsOnLine);
EST_setFlag_updateRs(estHandle, gFlag_updateRs);
EST_setRsOnLineAngleDelta_pu(estHandle, _IQmpy(gRsOnLineFreq_Hz, _IQ(1.0/USER_ISR_FREQ_Hz)));
EST_setRsOnLineId_mag_pu(estHandle, _IQmpy(gRsOnLineId_mag_A, _IQ(1.0/USER_IQ_FULL_SCALE_CURRENT_A)));

276 // Calculate coefficients for all filters
{
    _iq b0 = _IQmpy(gRsOnLinePole_Hz, _IQ(1.0/USER_ISR_FREQ_Hz));
    _iq a1 = b0 - _IQ(1.0);
    EST_setRsOnLineFilterParams(estHandle, EST_RsOnLineFilterType_Current, b0, a1, _IQ(0.0), b0, a1, _IQ(0.0));
281 EST_setRsOnLineFilterParams(estHandle, EST_RsOnLineFilterType_Voltage, b0, a1, _IQ(0.0), b0, a1, _IQ(0.0));
}

// set the number of current sensors
286 setupClarke_I(clarkeHandle_I, USER_NUM_CURRENT_SENSORS);

// set the number of voltage sensors
setupClarke_V(clarkeHandle_V, USER_NUM_VOLTAGE_SENSORS);

// set the pre-determined current and voltage feedback offset values
291 gOffsets_I_pu.value[0] = _IQ(I_A_offset);
gOffsets_I_pu.value[1] = _IQ(I_B_offset);
gOffsets_I_pu.value[2] = _IQ(I_C_offset);
gOffsets_V_pu.value[0] = _IQ(V_A_offset);
gOffsets_V_pu.value[1] = _IQ(V_B_offset);
296 gOffsets_V_pu.value[2] = _IQ(V_C_offset);

```

```

// initialize the PID controllers
{
    _iq maxCurrent_pu = _IQ(USER_MOTOR_MAX_CURRENT / USER_IQ_FULL_SCALE_CURRENT_A);
    _iq maxVoltage_pu = _IQ(USER_MAX_VS_MAG_PU * USER_VD_SF);
301 float_t fullScaleCurrent = USER_IQ_FULL_SCALE_CURRENT_A;
    float_t fullScaleVoltage = USER_IQ_FULL_SCALE_VOLTAGE_V;
    float_t IsrPeriod_sec = 1.0 / USER_ISR_FREQ_Hz;
    float_t Ls_d = USER_MOTOR_Ls_d;
306 float_t Ls_q = USER_MOTOR_Ls_q;
    float_t Rs = USER_MOTOR_Rs;
    float_t RoverLs_d = Rs/Ls_d;
    float_t RoverLs_q = Rs/Ls_q;
    _iq Kp_Id = _IQ((0.25*Ls_d*fullScaleCurrent)/(IsrPeriod_sec*fullScaleVoltage));
    _iq Ki_Id = _IQ(RoverLs_d*IsrPeriod_sec);
311 _iq Kp_Iq = _IQ((0.25*Ls_q*fullScaleCurrent)/(IsrPeriod_sec*fullScaleVoltage));
    _iq Ki_Iq = _IQ(RoverLs_q*IsrPeriod_sec);

    pidHandle[0] = PID_init(&pid[0], sizeof(pid[0]));
316 pidHandle[1] = PID_init(&pid[1], sizeof(pid[1]));
    pidHandle[2] = PID_init(&pid[2], sizeof(pid[2]));

    PID_setGains(pidHandle[0], _IQ(1.0), _IQ(0.01), _IQ(0.0));
    PID_setMinMax(pidHandle[0], -maxCurrent_pu, maxCurrent_pu);
321 PID_setUi(pidHandle[0], _IQ(0.0));
    pidCntSpeed = 0;

    PID_setGains(pidHandle[1], Kp_Id, Ki_Id, _IQ(0.0));
    PID_setMinMax(pidHandle[1], -maxVoltage_pu, maxVoltage_pu);
326 PID_setUi(pidHandle[1], _IQ(0.0));

    PID_setGains(pidHandle[2], Kp_Iq, Ki_Iq, _IQ(0.0));
    PID_setMinMax(pidHandle[2], _IQ(0.0), _IQ(0.0));
    PID_setUi(pidHandle[2], _IQ(0.0));
331 }

// initialize the speed reference in kilo RPM where base speed is USER_IQ_FULL_SCALE_FREQ_Hz
gMotorVars.SpeedRef_krpm = _IQmpy(_IQ(10.0), gSpeed_hz_to_krpm_sf);

336 // initialize the inverse Park module
iparkHandle = IPARK_init(&ipark, sizeof(ipark));

// initialize and configure offsets using filters
{
341 uint16_t cnt = 0;
    _iq b0 = _IQ(gUserParams.offsetPole_rps/(float_t)gUserParams.ctrlFreq_Hz);
    _iq a1 = (b0 - _IQ(1.0));
    _iq b1 = _IQ(0.0);

346 for(cnt=0;cnt<6;cnt++)
    {
        filterHandle[cnt] = FILTER_FO_init(&filter[cnt], sizeof(filter[0]));
        FILTER_FO_setDenCoeffs(filterHandle[cnt], a1);
        FILTER_FO_setNumCoeffs(filterHandle[cnt], b0, b1);
351 FILTER_FO_setInitialConditions(filterHandle[cnt], _IQ(0.0), _IQ(0.0));
    }

    gMotorVars.Flag_enableOffsetcalc = false;
}
356

// initialize the space vector generator module
svgenHandle = SVGEN_init(&svgen, sizeof(svgen));

// Initialize and setup the 100% SVM generator
361 svgencurrentHandle = SVGENCURRENT_init(&svgencurrent, sizeof(svgencurrent));

// setup svgen current
{
    float_t minWidth_microseconds = 2.0;
366 uint16_t minWidth_counts = (uint16_t)(minWidth_microseconds * USER_SYSTEM_FREQ_MHz);
    float_t fdutyLimit = 0.5 - (2.0*minWidth_microseconds*USER_PWM_FREQ_kHz*0.001);
    _iq dutyLimit = _IQ(fdutyLimit);

    SVGENCURRENT_setMinWidth(svgencurrentHandle, minWidth_counts);
371 SVGENCURRENT_setIgnoreShunt(svgencurrentHandle, use_all);
    SVGENCURRENT_setMode(svgencurrentHandle, all_phase_measurable);
    SVGENCURRENT_setVlimit(svgencurrentHandle, dutyLimit);
}

376 // set overmodulation to maximum value
gMotorVars.OverModulation = _IQ(USER_MAX_VS_MAG_PU);
// initialize the speed reference trajectory
trajHandle_spd = TRAJ_init(&traj_spd, sizeof(traj_spd));

381 // configure the speed reference trajectory

```

```

TRAJ_setTargetValue(trajHandle_spd, _IQ(0.0));
TRAJ_setIntValue(trajHandle_spd, _IQ(0.0));
TRAJ_setMinValue(trajHandle_spd, _IQ(-1.0));
TRAJ_setMaxValue(trajHandle_spd, _IQ(1.0));
386 TRAJ_setMaxDelta(trajHandle_spd, _IQ(USER_MAX_ACCEL_Hzps / USER_IQ_FULL_SCALE_FREQ_Hz / USER_ISR_FREQ_Hz)
);

// initialize the Id reference trajectory
trajHandle_Id = TRAJ_init(&traj_Id, sizeof(traj_Id));

391 if(USER_MOTOR_TYPE == MOTOR_Type_Pm)
{
// configure the Id reference trajectory
TRAJ_setTargetValue(trajHandle_Id, _IQ(0.0));
TRAJ_setIntValue(trajHandle_Id, _IQ(0.0));
396 TRAJ_setMinValue(trajHandle_Id, _IQ(-USER_MOTOR_MAX_CURRENT / USER_IQ_FULL_SCALE_CURRENT_A));
TRAJ_setMaxValue(trajHandle_Id, _IQ(USER_MOTOR_MAX_CURRENT / USER_IQ_FULL_SCALE_CURRENT_A));
TRAJ_setMaxDelta(trajHandle_Id, _IQ(USER_MOTOR_RES_EST_CURRENT / USER_IQ_FULL_SCALE_CURRENT_A /
USER_ISR_FREQ_Hz));

// Initialize field weakening
401 fwHandle = FW_init(&fw, sizeof(fw));
FW_setFlag_enableFw(fwHandle, false); // Disable field weakening
FW_clearCounter(fwHandle); // Clear field weakening counter
FW_setNumIsrTicksPerFwTick(fwHandle, FW_NUM_ISR_TICKS_PER_CTRL_TICK); // Set the number of ISR per
field weakening ticks
FW_setDeltas(fwHandle, FW_INC_DELTA, FW_DEC_DELTA); // Set the deltas of field weakening
406 FW_setOutput(fwHandle, _IQ(0.0)); // Set initial output of field weakening to zero
FW_setMinMax(fwHandle, _IQ(USER_MAX_NEGATIVE_ID_REF_CURRENT_A / USER_IQ_FULL_SCALE_CURRENT_A), _IQ(0.0))
; // Set the field weakening controller limits
}
else
{
411 // configure the Id reference trajectory
TRAJ_setTargetValue(trajHandle_Id, _IQ(0.0));
TRAJ_setIntValue(trajHandle_Id, _IQ(0.0));
TRAJ_setMinValue(trajHandle_Id, _IQ(0.0));
TRAJ_setMaxValue(trajHandle_Id, _IQ(USER_MOTOR_MAGNETIZING_CURRENT / USER_IQ_FULL_SCALE_CURRENT_A));
416 TRAJ_setMaxDelta(trajHandle_Id, _IQ(USER_MOTOR_MAGNETIZING_CURRENT / USER_IQ_FULL_SCALE_CURRENT_A /
USER_ISR_FREQ_Hz));
}

// initialize the CPU usage module
cpu_usageHandle = CPU_USAGE_init(&cpu_usage, sizeof(cpu_usage));
421 CPU_USAGE_setParams(cpu_usageHandle,
HAL_getTimerPeriod(halHandle, 1), // timer period, cnts
(uint32_t)USER_ISR_FREQ_Hz); // average over 1 second of ISRs

// setup faults
426 HAL_setupFaults(halHandle);

// initialize the interrupt vector table
HAL_initIntVectorTable(halHandle);

431 // enable the ADC interrupts
HAL_enableAdcInts(halHandle);

// enable global interrupts
HAL_enableGlobalInts(halHandle);
436 // enable debug interrupts
HAL_enableDebugInt(halHandle);

// disable the PWM
441 HAL_disablePwm(halHandle);

// compute scaling factors for flux and torque calculations
gFlux_pu_to_Wb_sf = USER_computeFlux_pu_to_Wb_sf();
gFlux_pu_to_VpHz_sf = USER_computeFlux_pu_to_VpHz_sf();
446 gTorque_Ls_Id_Iq_pu_to_Nm_sf = USER_computeTorque_Ls_Id_Iq_pu_to_Nm_sf();
gTorque_Flux_Iq_pu_to_Nm_sf = USER_computeTorque_Flux_Iq_pu_to_Nm_sf();

// enable the system by default
gMotorVars.Flag_enableSys = true;

451 #ifndef DRV8301_SPI
// turn on the DRV8301 if present
HAL_enableDrv(halHandle);
// initialize the DRV8301 interface
456 HAL_setupDrvSpi(halHandle, &gDrvSpi8301Vars);
#endif

#ifndef DRV8305_SPI
// turn on the DRV8305 if present

```



```

461 HAL_enableDrv(halHandle);
    // initialize the DRV8305 interface
    HAL_setupDrvSpi(halHandle,&gDrvSpi8305Vars);
#endif

466 // Begin the background loop
for(;;)
{
    // Waiting for enable system flag to be set
    while(!(gMotorVars.Flag_enableSys));

471 // loop while the enable system flag is true
    while(gMotorVars.Flag_enableSys)
    {
476         if(gMotorVars.Flag_Run_Identify)
        {
            // disable Rs recalculation
            EST_setFlag_enableRsRecalc(estHandle, false);

            // update estimator state
481 EST_updateState(estHandle,0);

            #ifdef FAST_ROM_V1p6
                // call this function to fix 1p6
                softwareUpdate1p6(estHandle);
486 #endif

            // enable the PWM
            HAL_enablePwm(halHandle);

491 // set trajectory target for speed reference
            TRAJ_setTargetValue(trajHandle_spd, _IQmpy(gMotorVars.SpeedRef_krpm, gSpeed_krpm_to_pu_sf));

            if(USER_MOTOR_TYPE == MOTOR_Type_Pm)
            {
496 // set trajectory target for Id reference
                TRAJ_setTargetValue(trajHandle_Id, gIdq_ref_pu.value[0]);
            }
            else
            {
501         if(gMotorVars.Flag_enablePowerWarp)
                {
                    _iq Id_target_pw_pu = EST_runPowerWarp(estHandle, TRAJ_getIntValue(trajHandle_Id),
                        gIdq_pu.value[1]);
                    TRAJ_setTargetValue(trajHandle_Id, Id_target_pw_pu);
                    TRAJ_setMinValue(trajHandle_Id, _IQ(USER_MOTOR_MAGNETIZING_CURRENT * 0.3 /
506 USER_IQ_FULL_SCALE_CURRENT_A));
                    TRAJ_setMaxDelta(trajHandle_Id, _IQ(USER_MOTOR_MAGNETIZING_CURRENT * 0.3 /
                        USER_IQ_FULL_SCALE_CURRENT_A / USER_ISR_FREQ_Hz));
                }
                else
                {
511 // set trajectory target for Id reference
                    TRAJ_setTargetValue(trajHandle_Id, _IQ(USER_MOTOR_MAGNETIZING_CURRENT /
                        USER_IQ_FULL_SCALE_CURRENT_A));
                    TRAJ_setMinValue(trajHandle_Id, _IQ(0.0));
                    TRAJ_setMaxDelta(trajHandle_Id, _IQ(USER_MOTOR_MAGNETIZING_CURRENT /
                        USER_IQ_FULL_SCALE_CURRENT_A / USER_ISR_FREQ_Hz));
                }
            }
        }
516     }
    else if(gMotorVars.Flag_enableRsRecalc)
    {
        // set angle to zero
        EST_setAngle_pu(estHandle, _IQ(0.0));

521 // enable or disable Rs recalculation
        EST_setFlag_enableRsRecalc(estHandle, true);

        // update estimator state
526 EST_updateState(estHandle,0);

        #ifdef FAST_ROM_V1p6
            // call this function to fix 1p6
            softwareUpdate1p6(estHandle);
531 #endif

        // enable the PWM
        HAL_enablePwm(halHandle);

536 // set trajectory target for speed reference
        TRAJ_setTargetValue(trajHandle_spd, _IQ(0.0));

        // set trajectory target for Id reference

```

```

    TRAJ_setTargetValue(trajHandle_Id, _IQ(USER_MOTOR_RES_EST_CURRENT /
541         USER_IQ_FULL_SCALE_CURRENT_A));
    // if done with Rs recalculation, disable flag
    if (EST_getState(estHandle) == EST_State_OnLine) gMotorVars.Flag_enableRsRecalc = false;
}
else
546 {
    // set estimator to Idle
    EST_setIdle(estHandle);

    // disable the PWM
551 if (!gMotorVars.Flag_enableOffsetcalc) HAL_disablePwm(halHandle);

    // clear the speed reference trajectory
    TRAJ_setTargetValue(trajHandle_spd, _IQ(0.0));
    TRAJ_setIntValue(trajHandle_spd, _IQ(0.0));
556

    // clear the Id reference trajectory
    TRAJ_setTargetValue(trajHandle_Id, _IQ(0.0));
    TRAJ_setIntValue(trajHandle_Id, _IQ(0.0));

561 // configure trajectory Id defaults depending on motor type
    if (USER_MOTOR_TYPE == MOTOR_Type_Pm)
    {
        TRAJ_setMinValue(trajHandle_Id, _IQ(-USER_MOTOR_MAX_CURRENT / USER_IQ_FULL_SCALE_CURRENT_A)
        );
        TRAJ_setMaxDelta(trajHandle_Id, _IQ(USER_MOTOR_RES_EST_CURRENT /
566         USER_IQ_FULL_SCALE_CURRENT_A / USER_ISR_FREQ_Hz));
    }
    else
    {
        TRAJ_setMinValue(trajHandle_Id, _IQ(0.0));
        TRAJ_setMaxDelta(trajHandle_Id, _IQ(USER_MOTOR_MAGNETIZING_CURRENT /
571         USER_IQ_FULL_SCALE_CURRENT_A / USER_ISR_FREQ_Hz));
    }

    // clear integral outputs
    PID_setUi(pidHandle[0], _IQ(0.0));
    PID_setUi(pidHandle[1], _IQ(0.0));
576 PID_setUi(pidHandle[2], _IQ(0.0));

    // clear Id and Iq references
    gIdq_ref_pu.value[0] = _IQ(0.0);
    gIdq_ref_pu.value[1] = _IQ(0.0);
581

    // disable RsOnLine flags
    gFlag_enableRsOnLine = false;
    gFlag_updateRs = false;

586 // disable PowerWarp flag
    gMotorVars.Flag_enablePowerWarp = false;
}

// update the global variables
591 updateGlobalVariables(estHandle);

// set field weakening enable flag depending on user's input
FW_setFlag_enableFw(fwHandle, gMotorVars.Flag_enableFieldWeakening);

596 // set the speed acceleration
    TRAJ_setMaxDelta(trajHandle_spd, _IQmpy(MAX_ACCEL_KRPMPS_SF, gMotorVars.MaxAccel_krpmmps));

// update CPU usage
updateCPUusage();
601

updateRsOnLine(estHandle);

// enable/disable the forced angle
EST_setFlag_enableForceAngle(estHandle, gMotorVars.Flag_enableForceAngle);
606
#ifdef DRV8301_SPI
    HAL_writeDrvData(halHandle, &gDrvSpi8301Vars);
    HAL_readDrvData(halHandle, &gDrvSpi8301Vars);
611 #endif
#ifdef DRV8305_SPI
    HAL_writeDrvData(halHandle, &gDrvSpi8305Vars);
    HAL_readDrvData(halHandle, &gDrvSpi8305Vars);
616 #endif
} // end of while(gFlag_enableSys) loop

```

```

621     // disable the PWM
        HAL_disablePwm(halHandle);

        gMotorVars.Flag_Run_Identify = false;
    } // end of for(;;) loop
} // end of main() function
626

//! \brief The main ISR that implements the motor control.
interrupt void mainISR(void)
{
631     _iq angle_pu = _IQ(0.0);
    _iq speed_pu = _IQ(0.0);
    _iq oneOverDcBus;
    MATH_vec2 Iab_pu;
    MATH_vec2 Vab_pu;
636     MATH_vec2 phasor;
    uint32_t timer1Cnt;

    // read the timer 1 value and update the CPU usage module
    timer1Cnt = HAL_readTimerCnt(halHandle,1);
641     CPU_USAGE_updateCnts(cpu_usageHandle, timer1Cnt);

    // acknowledge the ADC interrupt
    HAL_acqAdcInt(halHandle, ADC_IntNumber_1);

646     // convert the ADC data
    HAL_readAdcDataWithOffsets(halHandle, &gAdcData);

    // remove offsets
    gAdcData.I.value[0] = gAdcData.I.value[0] - gOffsets_I_pu.value[0];
651     gAdcData.I.value[1] = gAdcData.I.value[1] - gOffsets_I_pu.value[1];
    gAdcData.I.value[2] = gAdcData.I.value[2] - gOffsets_I_pu.value[2];
    gAdcData.V.value[0] = gAdcData.V.value[0] - gOffsets_V_pu.value[0];
    gAdcData.V.value[1] = gAdcData.V.value[1] - gOffsets_V_pu.value[1];
656     gAdcData.V.value[2] = gAdcData.V.value[2] - gOffsets_V_pu.value[2];

    // run the current reconstruction algorithm
    runCurrentReconstruction();

    // run Clarke transform on current
661     CLARKE_run(clarkeHandle_I, &gAdcData.I, &Iab_pu);

    // run Clarke transform on voltage
    CLARKE_run(clarkeHandle_V, &gAdcData.V, &Vab_pu);

666     // run a trajectory for Id reference, so the reference changes with a ramp instead of a step
    TRAJ_run(trajHandle_Id);

    // run the estimator
    EST_run(estHandle,
671         &Iab_pu,
        &Vab_pu,
        gAdcData.dcBus,
        TRAJ_getIntValue(trajHandle_spd));

676     // generate the motor electrical angle
    angle_pu = EST_getAngle_pu(estHandle);
    speed_pu = EST_getFm_pu(estHandle);

    // get Idq from estimator to avoid sin and cos
681     EST_getIdq_pu(estHandle, &gIdq_pu);

    // run the appropriate controller
    if((gMotorVars.Flag_Run_Identify) || (gMotorVars.Flag_enableRsRecalc))
    {
686         _iq refValue;
        _iq fbackValue;
        _iq outMax_pu;

        // when appropriate, run the PID speed controller
691         if((pidCntSpeed++ >= USER_NUM_CTRL_TICKS_PER_SPEED_TICK) && (!gMotorVars.Flag_enableRsRecalc))
            {
                // calculate Id reference squared
                _iq Id_ref_squared_pu = _IQmpy(PID_getRefValue(pidHandle[1]), PID_getRefValue(pidHandle[1]));

696                // Take into consideration that  $I_q^2 + I_d^2 = I_s^2$ 
                _iq Iq_Max_pu = _IQsqrt(gIs_Max_squared_pu - Id_ref_squared_pu);

                // clear counter
                pidCntSpeed = 0;

701                // Set new min and max for the speed controller output
                PID_setMinMax(pidHandle[0], -Iq_Max_pu, Iq_Max_pu);
            }
    }
}

```

```

706     // run speed controller
    PID_run_spd(pidHandle[0], TRAJ_getIntValue(trajHandle_spd), speed_pu, &(gIdq_ref_pu.value[1]));
}

// get the reference value from the trajectory module
711 refValue = TRAJ_getIntValue(trajHandle_Id) + EST_getRsOnLineId_pu(estHandle);

// get the feedback value
fbackValue = gIdq_pu.value[0];

// run the Id PID controller
716 PID_run(pidHandle[1], refValue, fbackValue, &(gVdq_out_pu.value[0]));

// set Iq reference to zero when doing Rs recalculation
if(gMotorVars.Flag_enableRsRecalc) gIdq_ref_pu.value[1] = _IQ(0.0);

721 // get the Iq reference value
refValue = gIdq_ref_pu.value[1];

// get the feedback value
fbackValue = gIdq_pu.value[1];
726

// calculate Iq controller limits, and run Iq controller
_iq_max_vs = _IQmpy(gMotorVars.OverModulation, EST_getDcBus_pu(estHandle));
outMax_pu = _IQsqrt(_IQmpy(max_vs, max_vs) - _IQmpy(gVdq_out_pu.value[0], gVdq_out_pu.value[0]));
PID_setMinMax(pidHandle[2], -outMax_pu, outMax_pu);
731 PID_run(pidHandle[2], refValue, fbackValue, &(gVdq_out_pu.value[1]));

// compensate angle for PWM delay
angle_pu = angleDelayComp(speed_pu, angle_pu);

736 // compute the sin/cos phasor
phasor.value[0] = _IQcosPU(angle_pu);
phasor.value[1] = _IQsinPU(angle_pu);

// set the phasor in the inverse Park transform
741 IPARK_setPhasor(iparkHandle, &phasor);

// run the inverse Park module
IPARK_run(iparkHandle, &gVdq_out_pu, &Vab_pu);

746 // run the space Vector Generator (SVGEN) module
oneOverDcBus = EST_getOneOverDcBus_pu(estHandle);
Vab_pu.value[0] = _IQmpy(Vab_pu.value[0], oneOverDcBus);
Vab_pu.value[1] = _IQmpy(Vab_pu.value[1], oneOverDcBus);
SVGEN_run(svggenHandle, &Vab_pu, &(gPwmData.Tabc));

751 // run the PWM compensation and current ignore algorithm
SVGENCURRENT_compPwmData(svggencurrentHandle, &(gPwmData.Tabc), &gPwmData_prev);

gTrjCnt++;
756 }
else if(gMotorVars.Flag_enableOffsetcalc == true)
{
runOffsetsCalculation();
}
761 else
{
// disable the PWM
HAL_disablePwm(halHandle);

766 // Set the PWMs to 50% duty cycle
gPwmData.Tabc.value[0] = _IQ(0.0);
gPwmData.Tabc.value[1] = _IQ(0.0);
gPwmData.Tabc.value[2] = _IQ(0.0);
}

771 // write the PWM compare values
HAL_writePwmData(halHandle, &gPwmData);

if(gTrjCnt >= gUserParams.numCtrlTicksPerTrajTick)
776 {
// clear counter
gTrjCnt = 0;

// run a trajectory for speed reference, so the reference changes with a ramp instead of a step
781 TRAJ_run(trajHandle_spd);
}

// run function to set next trigger
if(!gMotorVars.Flag_enableRsRecalc) runSetTrigger();
786

// run field weakening

```

```

    if(USER_MOTOR_TYPE == MOTOR_Type_Pm) runFieldWeakening();

    // read the timer 1 value and update the CPU usage module
791 timer1Cnt = HAL_readTimerCnt(halHandle,1);
    CPU_USAGE_updateCnts(cpu_usageHandle, timer1Cnt);

    // run the CPU usage module
    CPU_USAGE_run(cpu_usageHandle);
796
    return;
} // end of mainISR() function

801 _iq angleDelayComp(const _iq fm_pu, const _iq angleUncomp_pu)
{
    _iq angleDelta_pu = _IQmpy(fm_pu, _IQ(USER_IQ_FULL_SCALE_FREQ_Hz/(USER_PWM_FREQ_kHz*1000.0)));
    _iq angleCompFactor = _IQ(1.0 + (float_t)USER_NUM_PWM_TICKS_PER_ISR_TICK * 0.5);
    _iq angleDeltaComp_pu = _IQmpy(angleDelta_pu, angleCompFactor);
806 uint32_t angleMask = ((uint32_t)0xFFFFFFFF >> (32 - GLOBAL_Q));
    _iq angleComp_pu;
    _iq angleTmp_pu;

    // increment the angle
811 angleTmp_pu = angleUncomp_pu + angleDeltaComp_pu;

    // mask the angle for wrap around
    // note: must account for the sign of the angle
    angleComp_pu = _IQabs(angleTmp_pu) & angleMask;
816

    // account for sign
    if(angleTmp_pu < _IQ(0.0))
    {
821         angleComp_pu = -angleComp_pu;
    }

    return(angleComp_pu);
} // end of angleDelayComp() function

826 void runCurrentReconstruction(void)
{
    SVGENCURRENT_MeasureShunt_e measurableShuntThisCycle = SVGENCURRENT_getMode(svgencurrentHandle);

831 // run the current reconstruction algorithm
    SVGENCURRENT_RunRegenCurrent(svgencurrentHandle, (MATH_vec3 *)(&gAdcData.I.value));

    gIavg.value[0] += (gAdcData.I.value[0] - gIavg.value[0])>>gIavg_shift;
    gIavg.value[1] += (gAdcData.I.value[1] - gIavg.value[1])>>gIavg_shift;
836 gIavg.value[2] += (gAdcData.I.value[2] - gIavg.value[2])>>gIavg_shift;

    if(measurableShuntThisCycle > two_phase_masurable)
    {
841         gAdcData.I.value[0] = gIavg.value[0];
        gAdcData.I.value[1] = gIavg.value[1];
        gAdcData.I.value[2] = gIavg.value[2];
    }

    return;
846 } // end of runCurrentReconstruction() function

void runSetTrigger(void)
{
    SVGENCURRENT_IgnoreShunt_e ignoreShuntNextCycle = SVGENCURRENT_getIgnoreShunt(svgencurrentHandle);
851 SVGENCURRENT_VmidShunt_e midVolShunt = SVGENCURRENT_getVmid(svgencurrentHandle);

    // Set trigger point in the middle of the low side pulse
    HAL_setTrigger(halHandle, ignoreShuntNextCycle, midVolShunt);

856 return;
} // end of runSetTrigger() function

void runFieldWeakening(void)
{
861 if(FW_getFlag_enableFw(fwHandle) == true)
    {
        FW_incCounter(fwHandle);

        if(FW_getCounter(fwHandle) > FW_getNumIsrTicksPerFwTick(fwHandle))
866         {
            _iq refValue;
            _iq fbackValue;

            FW_clearCounter(fwHandle);
871

```

```

        refValue = gMotorVars.VsRef;
        fbackValue = _IQmpy(gMotorVars.Vs, EST_getOneOverDcBus_pu(estHandle));
876        FW_run(fwHandle, refValue, fbackValue, &(gIdq_ref_pu.value[0]));
        gMotorVars.IdRef_A = _IQmpy(gIdq_ref_pu.value[0], _IQ(USER_IQ_FULL_SCALE_CURRENT_A));
    }
881    else
    {
        gIdq_ref_pu.value[0] = _IQmpy(gMotorVars.IdRef_A, _IQ(1.0/USER_IQ_FULL_SCALE_CURRENT_A));
    }
886    return;
} // end of runFieldWeakening() function

void runOffsetsCalculation(void)
891 {
    uint16_t cnt;

    // enable the PWM
    HAL_enablePwm(halHandle);
896    for(cnt=0;cnt<3;cnt++)
    {
        // Set the PWMs to 50% duty cycle
        gPwmData.Tabc.value[cnt] = _IQ(0.0);
901        // reset offsets used
        gOffsets_I_pu.value[cnt] = _IQ(0.0);
        gOffsets_V_pu.value[cnt] = _IQ(0.0);
906        // run offset estimation
        FILTER_FO_run(filterHandle[cnt],gAdcData.I.value[cnt]);
        FILTER_FO_run(filterHandle[cnt+3],gAdcData.V.value[cnt]);
    }
911    if(gOffsetCalcCount++ >= gUserParams.ctrlWaitTime[CTRL_State_OffLine])
    {
        gMotorVars.Flag_enableOffsetcalc = false;
        gOffsetCalcCount = 0;
916        for(cnt=0;cnt<3;cnt++)
        {
            // get calculated offsets from filter
            gOffsets_I_pu.value[cnt] = FILTER_FO_get_y1(filterHandle[cnt]);
            gOffsets_V_pu.value[cnt] = FILTER_FO_get_y1(filterHandle[cnt+3]);
921            // clear filters
            FILTER_FO_setInitialConditions(filterHandle[cnt],_IQ(0.0),_IQ(0.0));
            FILTER_FO_setInitialConditions(filterHandle[cnt+3],_IQ(0.0),_IQ(0.0));
926        }
    }
    return;
} // end of runOffsetsCalculation() function

931 void softwareUpdate1p6(EST_Handle handle)
{
    float_t fullScaleInductance = USER_IQ_FULL_SCALE_VOLTAGE_V/(USER_IQ_FULL_SCALE_CURRENT_A*
        USER_VOLTAGE_FILTER_POLE_rps);
    float_t Ls_coarse_max = _IQ30toF(EST_getLs_coarse_max_pu(handle));
936    int_least8_t lShift = ceil(log(USER_MOTOR_Ls_d/(Ls_coarse_max*fullScaleInductance))/log(2.0));
    uint_least8_t Ls_qFmt = 30 - lShift;
    float_t L_max = fullScaleInductance * pow(2.0, lShift);
    _iq Ls_d_pu = _IQ30(USER_MOTOR_Ls_d / L_max);
    _iq Ls_q_pu = _IQ30(USER_MOTOR_Ls_q / L_max);
941
    // store the results
    EST_setLs_d_pu(handle, Ls_d_pu);
    EST_setLs_q_pu(handle, Ls_q_pu);
946    EST_setLs_qFmt(handle, Ls_qFmt);
    return;
} // end of softwareUpdate1p6() function

951 /// \brief Setup the Clarke transform for either 2 or 3 sensors.
/// \param[in] handle The clarke (CLARKE) handle
/// \param[in] numCurrentSensors The number of current sensors
void setupClarke_I(CLARKE_Handle handle, const uint_least8_t numCurrentSensors)

```

```

{
956  _iq alpha_sf, beta_sf;
    // initialize the Clarke transform module for current
    if(numCurrentSensors == 3)
    {
961      alpha_sf = _IQ(MATH_ONE_OVER_THREE);
      beta_sf = _IQ(MATH_ONE_OVER_SQRT_THREE);
    }
    else if(numCurrentSensors == 2)
    {
966      alpha_sf = _IQ(1.0);
      beta_sf = _IQ(MATH_ONE_OVER_SQRT_THREE);
    }
    else
    {
971      alpha_sf = _IQ(0.0);
      beta_sf = _IQ(0.0);
    }

    // set the parameters
976  CLARKE_setScaleFactors(handle, alpha_sf, beta_sf);
    CLARKE_setNumSensors(handle, numCurrentSensors);

    return;
} // end of setupClarke_I() function
981

///! \brief Setup the Clarke transform for either 2 or 3 sensors.
///! \param[in] handle The clarke (CLARKE) handle
///! \param[in] numVoltageSensors The number of voltage sensors
986 void setupClarke_V(CLARKE_Handle handle, const uint_least8_t numVoltageSensors)
{
    _iq alpha_sf, beta_sf;

    // initialize the Clarke transform module for voltage
991  if(numVoltageSensors == 3)
    {
      alpha_sf = _IQ(MATH_ONE_OVER_THREE);
      beta_sf = _IQ(MATH_ONE_OVER_SQRT_THREE);
    }
996  else
    {
      alpha_sf = _IQ(0.0);
      beta_sf = _IQ(0.0);
    }
1001

    // set the parameters
    CLARKE_setScaleFactors(handle, alpha_sf, beta_sf);
    CLARKE_setNumSensors(handle, numVoltageSensors);

1006  return;
} // end of setupClarke_V() function

///! \brief Update the global variables (gMotorVars).
1011 ///! \param[in] handle The estimator (EST) handle
void updateGlobalVariables(EST_Handle handle)
{
    // get the speed estimate
1016  gMotorVars.Speed_krpm = EST_getSpeed_krpm(handle);

    // get the torque estimate
    {
      _iq Flux_pu = EST_getFlux_pu(handle);
      _iq Id_pu = PID_getFbackValue(pidHandle[1]);
      _iq Iq_pu = PID_getFbackValue(pidHandle[2]);
      _iq Ld_minus_Lq_pu = _IQ30toIQ(EST_getLs_d_pu(handle) - EST_getLs_q_pu(handle));
      _iq Torque_Flux_Iq_Nm = _IQmpy(_IQmpy(Flux_pu, Iq_pu), gTorque_Flux_Iq_pu_to_Nm_sf);
      _iq Torque_Ls_Id_Iq_Nm = _IQmpy(_IQmpy(_IQmpy(Ld_minus_Lq_pu, Id_pu), Iq_pu),
1026  gTorque_Ls_Id_Iq_pu_to_Nm_sf);
      _iq Torque_Nm = Torque_Flux_Iq_Nm + Torque_Ls_Id_Iq_Nm;

      gMotorVars.Torque_Nm = Torque_Nm;
    }

    // get the magnetizing current
1031  gMotorVars.MagnCurr_A = EST_getIdRated(handle);

    // get the rotor resistance
    gMotorVars.Rr_Ohm = EST_getRr_Ohm(handle);

1036  // get the stator resistance
    gMotorVars.Rs_Ohm = EST_getRs_Ohm(handle);

```

```

// get the online stator resistance
gMotorVars.RsOnLine_Ohm = EST_getRsOnLine_Ohm(handle);
1041 // get the stator inductance in the direct coordinate direction
gMotorVars.Lsd_H = EST_getLs_d_H(handle);

// get the stator inductance in the quadrature coordinate direction
1046 gMotorVars.Lsq_H = EST_getLs_q_H(handle);

// get the flux in V/Hz in floating point
gMotorVars.Flux_VpHz = EST_getFlux_VpHz(handle);

1051 // get the flux in Wb in fixed point
gMotorVars.Flux_Wb = _IQmpy(EST_getFlux_pu(handle), gFlux_pu_to_Wb_sf);

// get the estimator state
gMotorVars.EstState = EST_getState(handle);
1056 // Get the DC buss voltage
gMotorVars.VdcBus_kV = _IQmpy(gAdcData.dcBus, _IQ(USER_IQ_FULL_SCALE_VOLTAGE_V/1000.0));

// read Vd and Vq vectors per units
1061 gMotorVars.Vd = gVdq_out_pu.value[0];
gMotorVars.Vq = gVdq_out_pu.value[1];

// calculate vector Vs in per units
1066 gMotorVars.Vs = _IQsqrt(_IQmpy(gMotorVars.Vd, gMotorVars.Vd) + _IQmpy(gMotorVars.Vq, gMotorVars.Vq));

// read Id and Iq vectors in amps
gMotorVars.Id_A = _IQmpy(gIdq_pu.value[0], _IQ(USER_IQ_FULL_SCALE_CURRENT_A));
gMotorVars.Iq_A = _IQmpy(gIdq_pu.value[1], _IQ(USER_IQ_FULL_SCALE_CURRENT_A));

1071 // calculate vector Is in amps
gMotorVars.Is_A = _IQsqrt(_IQmpy(gMotorVars.Id_A, gMotorVars.Id_A) + _IQmpy(gMotorVars.Iq_A, gMotorVars.
    Iq_A));

return;
} // end of updateGlobalVariables() function
1076

void updateRsOnLine(EST_Handle handle)
{
// execute Rs OnLine code
1081 if(gMotorVars.Flag_Run_Identify == true)
    {
if((EST_getState(handle) == EST_State_OnLine) && (gFlag_enableRsOnLine))
    {
1086 float_t RsError_Ohm = gMotorVars.RsOnLine_Ohm - gMotorVars.Rs_Ohm;

EST_setFlag_enableRsOnLine(handle, true);
EST_setRsOnLineId_mag_pu(handle, _IQmpy(gRsOnLineId_mag_A, _IQ(1.0/USER_IQ_FULL_SCALE_CURRENT_A)));
;
EST_setRsOnLineAngleDelta_pu(handle, _IQmpy(gRsOnLineFreq_Hz, _IQ(1.0/USER_ISR_FREQ_Hz)));

1091 if(abs(RsError_Ohm) < (gMotorVars.Rs_Ohm * 0.05))
    {
EST_setFlag_updateRs(handle, true);
    }
    }
}

1096 else
    {
EST_setRsOnLineId_mag_pu(handle, _IQ(0.0));
EST_setRsOnLineId_pu(handle, _IQ(0.0));
EST_setRsOnLine_pu(handle, EST_getRs_pu(handle));
1101 EST_setFlag_enableRsOnLine(handle, false);
EST_setFlag_updateRs(handle, false);
EST_setRsOnLine_qFmt(handle, EST_getRs_qFmt(handle));
    }
}

1106 return;
} // end of updateRsOnLine() function
void updateCPUusage(void)
{
1111 uint32_t minDeltaCntObserved = CPU_USAGE_getMinDeltaCntObserved(cpu_usageHandle);
uint32_t avgDeltaCntObserved = CPU_USAGE_getAvgDeltaCntObserved(cpu_usageHandle);
uint32_t maxDeltaCntObserved = CPU_USAGE_getMaxDeltaCntObserved(cpu_usageHandle);
uint16_t pwmPeriod = HAL_readPwmPeriod(halHandle, PWM_Number_1);
float_t cpu_usage_den = (float_t)pwmPeriod * (float_t)USER_NUM_PWM_TICKS_PER_ISR_TICK * 2.0;
1116 // calculate the minimum cpu usage percentage
gCpuUsagePercentageMin = (float_t)minDeltaCntObserved / cpu_usage_den * 100.0;

```



```
1121 // calculate the average cpu usage percentage
gCpuUsagePercentageAvg = (float_t)avgDeltaCntObserved / cpu_usage_den * 100.0;
// calculate the maximum cpu usage percentage
gCpuUsagePercentageMax = (float_t)maxDeltaCntObserved / cpu_usage_den * 100.0;
1126 return;
} // end of updateCPUusage() function

//@} //defgroup
1131 // end of file
```



# D

## can.c code

```
1 /*
 * can.c
 * This library is free software; you can redistribute it and/or
 * modify it under the terms of the GNU Lesser General Public
 * License as published by the Free Software Foundation; either
6 * version 2.1 of the License, or (at your option) any later version.
 * This library is distributed in the hope that it will be useful,
 * but WITHOUT ANY WARRANTY; without even the implied warranty of
 * MERCHANTABILITY or FITNESS FOR A PARTICULAR PURPOSE. See the GNU
 * Lesser General Public License for more details.
11 * You should have received a copy of the GNU Lesser General Public
 * License along with this library; if not, write to the Free Software
 * Foundation, Inc., 59 Temple Place, Suite 330, Boston, MA 02111-1307 USA
 *
 * See LICENCE file for LGPL details.
16 *
 * Contains the various functions related to the eCAN
 * Target Device: TMS320F2802x
 * Copyright (C): 2017 Andrew Buckin
 * Created on: April 20, 2017
21 * Author: Andrew Buckin
 *
 */
#include <stdlib.h>
#include "can.h"
26
#define NELEMS(x) (sizeof(x)/sizeof((x)[0]))
///! \brief Define to allow protected register writes (legacy)
///!
#define EALLOW asm("_EALLOW")
31
///! \brief Define to allow protected register writes
///!
#define ENABLE_PROTECTED_REGISTER_WRITE_MODE asm("_EALLOW")
36
///! \brief Define to disable protected register writes (legacy)
///!
#define EDIS asm("_EDIS")

///! \brief Define to disable protected register writes
41 ///!
#define DISABLE_PROTECTED_REGISTER_WRITE_MODE asm("_EDIS")

ECAN_Handle ECAN_init(){
46     ECAN_Handle handle = (ECAN_Handle)calloc(1, sizeof(ECAN_Obj));

    if(handle == NULL){
        return (ECAN_Handle)NULL;
    }
51
    handle->ECanaRegs = (ECAN_REGS_t*)ECANA_REGS_ADDR;
    handle->ECanaMboxes = (ECAN_MBOXES_t*)ECANA_MBOX_ADDR;
    handle->ECanaLAMRegs = (LAM_REGS_t*)ECANA_LAM_ADDR;
    handle->ECanaMOTORegs = (MOTO_REGS_t*)ECANA_MOTO_ADDR;
56    handle->ECanaMOTSRegs = (MOTS_REGS_t*)ECANA_MOTS_ADDR;

    return handle;
}
```

```

void ECAN_setBitrate(ECAN_Handle handle, ECAN_Bitrate_e bitrate){
61     struct ECAN_REGS ECanaShadow;

    ALLOW; // Allow access to protected bits

    ECanaShadow.CANMC.all = handle->ECanaRegs->CANMC.all;
66     ECanaShadow.CANMC.bit.CCR = 1; // Set CCR = 1
    handle->ECanaRegs->CANMC.all = ECanaShadow.CANMC.all;

    // Wait until the CPU has been granted permission to change the configuration registers
    do
71     {
        ECanaShadow.CANES.all = handle->ECanaRegs->CANES.all;
    } while(ECanaShadow.CANES.bit.CCE != 1); // Wait for CCE bit to be set..

    ECanaShadow.CANBTC.all = 0;
76     // http://www.bittiming.can-wiki.info/ BT=15
    // 90 MHz SYSCLKOUT. (45 MHz CAN module clock)
    switch(bitrate) {
        case Bitrate_1M: ECanaShadow.CANBTC.all = 0x00020059; break;
        case Bitrate_500K: ECanaShadow.CANBTC.all = 0x00050059; break;
81     case Bitrate_250K: ECanaShadow.CANBTC.all = 0x000b0059; break;
        case Bitrate_125K: ECanaShadow.CANBTC.all = 0x00170059; break;
        case Bitrate_100K: ECanaShadow.CANBTC.all = 0x001d0059; break;
        case Bitrate_83K: ECanaShadow.CANBTC.all = 0x00230059; break;
        case Bitrate_50K: ECanaShadow.CANBTC.all = 0x003b0059; break;
86     case Bitrate_20K: ECanaShadow.CANBTC.all = 0x00950059; break;
        default: ECanaShadow.CANBTC.all = 0x000503BD; break; //500K 100ns
            sprac35
            //ECanaShadow.CANBTC.bit.BRPREG = 5;
            //ECanaShadow.CANBTC.bit.SJWREG = 3;
            //ECanaShadow.CANBTC.bit.SAM = 1;
91     //ECanaShadow.CANBTC.bit.TSEG1REG = 7;
            //ECanaShadow.CANBTC.bit.TSEG2REG = 5;
    }

    handle->ECanaRegs->CANBTC.all = ECanaShadow.CANBTC.all;
96

    ECanaShadow.CANMC.all = handle->ECanaRegs->CANMC.all;
    ECanaShadow.CANMC.bit.CCR = 0; // Set CCR = 0
    handle->ECanaRegs->CANMC.all = ECanaShadow.CANMC.all;

101    // Wait until the CPU no longer has permission to change the configuration registers
    do
    {
        ECanaShadow.CANES.all = handle->ECanaRegs->CANES.all;
    } while(ECanaShadow.CANES.bit.CCE != 0); // Wait for CCE bit to be cleared..
106

    EDIS; // Disable access to protected bits
}

111 void ECAN_setBTCreg(ECAN_Handle handle, long BTC_ALL){
    struct ECAN_REGS ECanaShadow;

    ALLOW; // Allow access to protected bits

116    ECanaShadow.CANMC.all = handle->ECanaRegs->CANMC.all;
    ECanaShadow.CANMC.bit.CCR = 1; // Set CCR = 1
    handle->ECanaRegs->CANMC.all = ECanaShadow.CANMC.all;

    // Wait until the CPU has been granted permission to change the configuration registers
121    do
    {
        ECanaShadow.CANES.all = handle->ECanaRegs->CANES.all;
    } while(ECanaShadow.CANES.bit.CCE != 1); // Wait for CCE bit to be set..

126    ECanaShadow.CANBTC.all = BTC_ALL;

    handle->ECanaRegs->CANBTC.all = ECanaShadow.CANBTC.all;

    ECanaShadow.CANMC.all = handle->ECanaRegs->CANMC.all;
131    ECanaShadow.CANMC.bit.CCR = 0; // Set CCR = 0
    handle->ECanaRegs->CANMC.all = ECanaShadow.CANMC.all;

    // Wait until the CPU no longer has permission to change the configuration registers
136    do
    {
        ECanaShadow.CANES.all = handle->ECanaRegs->CANES.all;
    } while(ECanaShadow.CANES.bit.CCE != 0); // Wait for CCE bit to be cleared..

141    EDIS; // Disable access to protected bits
}

```

```

void ECAN_enableAllInt(ECAN_Handle handle){
    struct ECAN_REGS ECanaShadow;
146     EALLOW; // Allow access to protected bits

    //Enable interrupts.
    ECanaShadow.CANGIM.all = 0;
151     ECanaShadow.CANGIM.bit.AAIM = 1; /* Abort acknowledge */
    ECanaShadow.CANGIM.bit.WDIM = 1; /* Write denied */
    ECanaShadow.CANGIM.bit.WUJIM = 1; /* Wake up */
    ECanaShadow.CANGIM.bit.BOIM = 1; /* Bus-off */
    ECanaShadow.CANGIM.bit.EPIM = 1; /* Error-passive */
156     ECanaShadow.CANGIM.bit.WLIM = 1; /* Warning level */
    ECanaShadow.CANGIM.bit.GIL = 1; /* Global Interrup Level. */ //the GIL (GIM.2) bit can be set to
        have the global interrupts on another level than the mailbox interrupts
    ECanaShadow.CANGIM.bit.IOEN = 1; /* Interrupt 0 enable */
    ECanaShadow.CANGIM.bit.I1EN = 1; /* Interrupt 1 enable */
    ECanaShadow.CANGIM.bit.RMLIM = 1; /* Received Messae Lost */

161     handle->ECanaRegs->CANGIM.all = ECanaShadow.CANGIM.all;

    EDIS; // Disable access to protected bits
}
166 void ECAN_disableAllInt(ECAN_Handle handle){
    struct ECAN_REGS ECanaShadow;

    EALLOW; // Allow access to protected bits
171     //Disable interrupts.
    ECanaShadow.CANGIM.all = 0;
    handle->ECanaRegs->CANGIM.all = ECanaShadow.CANGIM.all;

176     EDIS; // Disable access to protected bits
}

void ECAN_clearMSGCTRL(ECAN_Handle handle){
181 //     volatile struct MBOX *mbox = (&(handle->ECanaMboxes->MBOX0));
    EALLOW; // Allow access to protected bits

    int i = 0;
    for(i = 0; i < 32; i++)
    {
186         mbox->MSGCTRL.all = 0x00000000;
        //mbox->MSGCTRL.all = i; //Test
        *mbox++;
    }

191 //     EDIS; // Disable access to protected bits
}

void ECAN_clearMSGID(ECAN_Handle handle){
196 //     volatile struct MBOX *mbox = (&(handle->ECanaMboxes->MBOX0));
    EALLOW; // Allow access to protected bits
    /* Disable all Mailboxes */
    handle->ECanaRegs->CANME.all = 0x00000000; // Required before writing the MSGIDs

    int i = 0;
    for(i = 0; i < 32; i++)
    {
201         mbox->MSGID.all = 0x00000000;
        //mbox->MSGID.all = i; //Test
        *mbox++;
    }
206 //     handle->ECanaRegs->CANME.all = 0xFFFFFFFF;
    //     EDIS; // Disable access to protected bits
}

211 void ECAN_clearMDL(ECAN_Handle handle){
    volatile struct MBOX *mbox = (&(handle->ECanaMboxes->MBOX0));
    //     EALLOW; // Allow access to protected bits

    int i = 0;
    for(i = 0; i < 32; i++)
    {
216         mbox->MDL.all = 0x00000000;
        //mbox->MDL.all = i; //Test
        *mbox++;
    }
221 //     EDIS; // Disable access to protected bits
}

```

```

226 void ECAN_clearMDH(ECAN_Handle handle){
    volatile struct MBOX *mbox = (&(handle->ECanaMboxes->MBOX0));
    // ALLOW; // Allow access to protected bits

    int i = 0;
231 for(i = 0; i < 32; i++)
    {
        mbox->MDH.all = 0x00000000;
        //mbox->MDH.all = i; //Test
        *mbox++;
236 }

    // EDIS; // Disable access to protected bits
}

241 void ECAN_enableAllMailbox(ECAN_Handle handle){
    // ALLOW; // Allow access to protected bits
    /* enable all Mailboxes */
    handle->ECanaRegs->CANME.all = 0xFFFFFFFF;
    // EDIS; // Disable access to protected bits
246 }

void ECAN_disableAllMailbox(ECAN_Handle handle){
    // ALLOW; // Allow access to protected bits
    /* disable all Mailboxes */
251 handle->ECanaRegs->CANME.all = 0x00000000;
    // EDIS; // Disable access to protected bits
}

void ECAN_setTXIO(ECAN_Handle handle){
256 struct ECAN_REGS ECanaShadow;
    ALLOW; // Allow access to protected bits
    ECanaShadow.CANTIOC.all = handle->ECanaRegs->CANTIOC.all;
    ECanaShadow.CANTIOC.bit.TXFUNC = 1;
    handle->ECanaRegs->CANTIOC.all = ECanaShadow.CANTIOC.all;
261 EDIS; // Disable access to protected bits
}

void ECAN_setRXIO(ECAN_Handle handle){
266 struct ECAN_REGS ECanaShadow;
    ALLOW; // Allow access to protected bits
    ECanaShadow.CANRIOCI.all = handle->ECanaRegs->CANRIOCI.all;
    ECanaShadow.CANRIOCI.bit.RXFUNC = 1;
    handle->ECanaRegs->CANRIOCI.all = ECanaShadow.CANRIOCI.all;
271 EDIS; // Disable access to protected bits
}

void ECAN_resetTXIO(ECAN_Handle handle){
    struct ECAN_REGS ECanaShadow;
276 ALLOW; // Allow access to protected bits
    ECanaShadow.CANTIOC.all = handle->ECanaRegs->CANTIOC.all;
    ECanaShadow.CANTIOC.bit.TXFUNC = 0;
    handle->ECanaRegs->CANTIOC.all = ECanaShadow.CANTIOC.all;
    EDIS; // Disable access to protected bits
}

281 void ECAN_resetRXIO(ECAN_Handle handle){
    struct ECAN_REGS ECanaShadow;
    ALLOW; // Allow access to protected bits
    ECanaShadow.CANRIOCI.all = handle->ECanaRegs->CANRIOCI.all;
    ECanaShadow.CANRIOCI.bit.RXFUNC = 0;
286 handle->ECanaRegs->CANRIOCI.all = ECanaShadow.CANRIOCI.all;
    EDIS; // Disable access to protected bits
}

291 void ECAN_setSCCmode(ECAN_Handle handle){
    struct ECAN_REGS ECanaShadow;
    ALLOW; // Allow access to protected bits
    /* Configure eCAN for HECC mode - (reqd to access mailboxes 16 thru 31) SCC mode */
    // HECC mode also enables
    // time-stamping feature

    ECanaShadow.CANMC.all = handle->ECanaRegs->CANMC.all;
    ECanaShadow.CANMC.bit.SCB = 1;
    handle->ECanaRegs->CANMC.all = ECanaShadow.CANMC.all;
    EDIS; // Disable access to protected bits
}

301 void ECAN_setECANmode(ECAN_Handle handle){
    struct ECAN_REGS ECanaShadow;
    ALLOW; // Allow access to protected bits
    ECanaShadow.CANMC.all = handle->ECanaRegs->CANMC.all;
    ECanaShadow.CANMC.bit.SCB = 0;
306 handle->ECanaRegs->CANMC.all = ECanaShadow.CANMC.all;
    EDIS; // Disable access to protected bits
}

```

```

}

311 void ECAN_Mode(ECAN_Handle handle, SCB_Bit_e mode){
    struct ECAN_REGS ECanaShadow;
    EALLOW; // Allow access to protected bits
    ECanaShadow.CANMC.all = handle->ECanaRegs->CANMC.all;
    ECanaShadow.CANMC.bit.SCB = mode;
316 handle->ECanaRegs->CANMC.all = ECanaShadow.CANMC.all;
    EDIS; // Disable access to protected bits
}

321 void ECAN_setSelfTest(ECAN_Handle handle){
    struct ECAN_REGS ECanaShadow;
    EALLOW; // Allow access to protected bits
    ECanaShadow.CANMC.all = handle->ECanaRegs->CANMC.all;
    ECanaShadow.CANMC.bit.STM = 1; // Enable self-test mode.
326 handle->ECanaRegs->CANMC.all = ECanaShadow.CANMC.all;
    EDIS; // Disable access to protected bits
}

void ECAN_resetSelfTest(ECAN_Handle handle){
331 struct ECAN_REGS ECanaShadow;
    EALLOW; // Allow access to protected bits
    ECanaShadow.CANMC.all = handle->ECanaRegs->CANMC.all;
    ECanaShadow.CANMC.bit.STM = 0; // Disable self-test mode.
    handle->ECanaRegs->CANMC.all = ECanaShadow.CANMC.all;
336 EDIS; // Disable access to protected bits
}

void ECAN_SelfTest(ECAN_Handle handle, STM_Bit_e mode){
341 struct ECAN_REGS ECanaShadow;
    EALLOW; // Allow access to protected bits
    ECanaShadow.CANMC.all = handle->ECanaRegs->CANMC.all;
    ECanaShadow.CANMC.bit.STM = mode; // Disable self-test mode.
    handle->ECanaRegs->CANMC.all = ECanaShadow.CANMC.all;
346 EDIS; // Disable access to protected bits
}

void ECAN_clearCANTA(ECAN_Handle handle){
    // EALLOW; // Allow access to protected bits
    /* Clear all Transmission-Acknowledge Register bits */
351 handle->ECanaRegs->CANTA.all = 0xFFFFFFFF;
    // EDIS; // Disable access to protected bits
}

void ECAN_clearCANRMP(ECAN_Handle handle){
    // EALLOW; // Allow access to protected bits
    /* Clear all Received-Message-Pending Register bits */
356 handle->ECanaRegs->CANRMP.all = 0xFFFFFFFF;
    // EDIS; // Disable access to protected bits
}

void ECAN_clearCANGIF0(ECAN_Handle handle){
361 // EALLOW; // Allow access to protected bits
    /* Clear all Global Interrupt Flag 0 */
    handle->ECanaRegs->CANGIF0.all = 0xFFFFFFFF;
    // EDIS; // Disable access to protected bits
}

void ECAN_clearCANGIF1(ECAN_Handle handle){
366 // EALLOW; // Allow access to protected bits
    /* Clear all Global Interrupt Flag 1 */
    handle->ECanaRegs->CANGIF1.all = 0xFFFFFFFF;
    // EDIS; // Disable access to protected bits
371 }

void ECAN_setMailboxDir(ECAN_Handle handle, long dir){
    // EALLOW; // Allow access to protected bits
    /* Mailbox-Direction Register */
376 handle->ECanaRegs->CANMD.all = dir;
    // EDIS; // Disable access to protected bits
}

void ECAN_setMailboxIntMask(ECAN_Handle handle, long mask){
381 EALLOW; // Allow access to protected bits
    /* Mailbox Interrupt Mask Register */
    handle->ECanaRegs->CANMIM.all = mask;
    EDIS; // Disable access to protected bits
}

386 void ECAN_configMailbox(ECAN_Handle handle, ECAN_MailBox_e MailBoxN, uint32_t msgid, Enable_Mbox_e
enable_t, ECAN_MailDir_e dir_t, IDE_Bit_e IDE_t, DLC_Bit_e length, LAMI_Bit_e lami_bit, AME_Bit_e
AME_t, uint32_t mask){
    struct ECAN_REGS ECanaShadow;
    volatile struct MBOX *mbox = (&(handle->ECanaMboxes->MBOX0)) + /*(uint32_t)*/MailBoxN;
    volatile union CANLAM_REG *lam = (&(handle->ECanaLAMRegs->LAM0)) + /*(uint32_t)*/MailBoxN;

```

```

391     uint8_t enable = enable_t;
    uint8_t dir = dir_t;
    // ALLOW; // Allow access to protected bits

    ECanaShadow.CANME.all = handle->ECanaRegs->CANME.all;
396     ECanaShadow.CANME.all = (~((~ECanaShadow.CANME.all) | (((uint32_t)1) << MailBoxN))) | (((uint32_t)
        Disable_Mbox) << MailBoxN);
    handle->ECanaRegs->CANME.all = ECanaShadow.CANME.all;

    lam->all = mask;
    lam->bit.LAMI = lami_bit;
401
    if (IDE_t == Extended_ID)
    {
        mbox->MSGID.all = msgid;
    }
406     else
    {
        mbox->MSGID.bit.EXTMSGID_L = 0;
        mbox->MSGID.bit.EXTMSGID_H = 0;
        mbox->MSGID.bit.STDMSGID = (uint16_t)msgid;
411     }

    mbox->MSGID.bit.IDE = IDE_t;
    mbox->MSGID.bit.AME = AME_t;
    mbox->MSGID.bit.AAM = Normal_transmit;
416
    // Specify that bits will be sent/received
    mbox->MSGCTRL.bit.DLC = length; //8;

    //Enable/disable mbox.
421     enable = enable & 1; //Making sure it's only one bit.
    ECanaShadow.CANME.all = handle->ECanaRegs->CANME.all;
    ECanaShadow.CANME.all = (~((~ECanaShadow.CANME.all) | (((uint32_t)1) << MailBoxN))) | (((uint32_t)
        enable) << MailBoxN);
    handle->ECanaRegs->CANME.all = ECanaShadow.CANME.all;

426     //Setting rx/tx mode.
    dir = dir & 1; //Making sure it's only one bit.
    ECanaShadow.CANMD.all = handle->ECanaRegs->CANMD.all;
    ECanaShadow.CANMD.all = (~((~ECanaShadow.CANMD.all) | (((uint32_t)1) << MailBoxN))) | (((uint32_t)
        dir) << MailBoxN);
    handle->ECanaRegs->CANMD.all = ECanaShadow.CANMD.all;
431 //
    }

    void ECAN_putDataMailbox(ECAN_Handle handle, ECAN_MailBox_e MailBoxN, long MDL_t, long MDH_t){
436 //
        volatile struct MBOX *mbox = (&(handle->ECanaMboxes->MBOX0)) + /*(uint32_t)*/MailBoxN;
        // ALLOW; // Allow access to protected bits
        mbox->MDL.all = MDL_t;
        mbox->MDH.all = MDH_t;
        // EDIS; // Disable access to protected bits
    }
441

    void ECAN_configMasterReg(ECAN_Handle handle, CCR_Bit_e CCR_t, PDR_Bit_e PDR_t, DBO_Bit_e DBO_t,
        WUBA_Bit_e WUBA_t, CDR_Bit_e CDR_t, ABO_Bit_e ABO_t, SRES_Bit_e SRES_t, MBNR_Bit_e MBNR_t){
        struct ECAN_REGS ECanaShadow;
        ALLOW; // Allow access to protected bits
        /* config Master Control Register */
446     ECanaShadow.CANMC.all = handle->ECanaRegs->CANMC.all;
        ECanaShadow.CANMC.bit.CCR = CCR_t;
        ECanaShadow.CANMC.bit.PDR = PDR_t;
        ECanaShadow.CANMC.bit.DBO = DBO_t;
        ECanaShadow.CANMC.bit.WUBA = WUBA_t;
451     ECanaShadow.CANMC.bit.CDR = CDR_t;
        ECanaShadow.CANMC.bit.ABO = ABO_t;
        ECanaShadow.CANMC.bit.SRES = SRES_t;
        ECanaShadow.CANMC.bit.MBNR = MBNR_t;
        handle->ECanaRegs->CANMC.all = ECanaShadow.CANMC.all;
456     EDIS; // Disable access to protected bits
    }

    int ECAN_sendMSG(ECAN_Handle handle, ECAN_MailBox_e MailBoxN, long MDL_t, long MDH_t){
461     volatile struct MBOX *mbox = (&(handle->ECanaMboxes->MBOX0)) + MailBoxN;

        mbox->MDL.all = MDL_t;
        mbox->MDH.all = MDH_t;

        handle->ECanaRegs->CANTRS.all |= 1 << MailBoxN;
466     //Wait for transmit acknowledge
        while(!(handle->ECanaRegs->CANTA.all >> MailBoxN));
        //Wait TRS.n = 0
        while(handle->ECanaRegs->CANTRS.all >> MailBoxN);
        //Set TA.n

```



```
471  handle->ECanaRegs->CANTA.all |= 1 << MailBoxN;  
      //Wait until read TA.n is 0  
      while(handle->ECanaRegs->CANTA.all >> MailBoxN);  
      return 0;  
}
```



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