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3D printed and punched porous surfaces of a non-resorbable, biphasic implant for the repair of osteochondral lesions improves repair tissue adherence and ingrowth

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Summary: The objective of this study was to evaluate a non-resorbable implant for the focal repair of osteochondral defects. Enhanced adherence of repair cartilage overgrowing the implants was the secondary goal and was tested by introducing porosities on the articular surface of the implant. This study evaluated four versions of the construct composed of a polycarbonate-urethane-urea biomaterial (elastomer) and a bone anchor. In order to induce porosities on the surface of the implant, either vertical holes were punched into it, or the chondral component was 3D-printed onto the implant. Fabrication, biomechanical characterization and cell infiltration of the implant were evaluated *in-vitro*. Subsequently the implants were tested in an *in-vivo* study in four Shetland ponies for 5 weeks. Enhanced porosity was successfully obtained for all implants. The 3D-printing of the elastomeric material produced pore diameters of 775 μm and 690 μm whilst the micro-punched pores had a diameter of 319 μm . The elastic modulus of the elastomer decreased with the introduction of porosity but stayed above values of native cartilage in all versions of the implant. Clinically the implant was well tolerated. The over-growing repair tissue was mostly flush with surrounding cartilage and attached to the elastomer through ingrowth of the tissue into the pores. Overall the tested implants all showed good mechanical performance *in vitro* and subjectively also *in vivo*. The repair cartilage was solidly attached to the porous surface of the implant. The printing approach potentially enables fine-tuning of the biomechanical properties of the implant depending on the specific requirements for a given location.

Keywords: cartilage, Joint, 3D printing, osteoarthritis, implant, horse model

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Introduction

The need for optimal functional treatment of chondral and osteochondral defects in human and veterinary patients is still unmet. Cartilage lesions, if left untreated, ultimately lead to a degenerative catabolic cascade within the joint that eventually develops into osteoarthritis (Hunziker 1999, Mankin 1982). In a functional therapeutical approach, non-resorbable implants consisting of polymers, alone or combined with metals, have been applied clinically in large-animal models, as well as in humans (Martinez Carranza et al. 2019, 2016, Husby et al. 2016, Nathwani et al. 2017, Danielski and Farrell 2018, Becher et al. 2011). The disadvantage of these types of implants, remains their continuous wear due to exposure at the joint surface and differing biomechanical characteristics between implants and surrounding native cartilage. Further,

their success also depends on the condition of the opposing cartilage surfaces (Damen et al. 2020).

A novel type of bi-layered, non-resorbable osteochondral implant has been tested recently in a horse model (Korthagen et al. 2019). Different to other prosthetic implants, this one is placed just below the articular surface allowing repair tissue to grow over it, creating a flush transition between the neo-tissue, which grows over the implant, and the adjacent original cartilage. The rationale behind this approach is that in these circumstances also a thin layer of fibrocartilage may lead to durable functional repair, which is, unlike surfaces made of artificial materials, self-maintaining. In that pilot study, the implant was completely covered with smooth repair tissue after 12 weeks and the neo-tissue exhibited good adherence to the surrounding native cartilage. However, the repair tissue did

not attach to the underlying elastomer, making it easily glide over the elastomer's surface (Korthagen et al. 2019).

In the present study, we aimed to improve the mechanical stability of the repair tissue on the elastomer. To achieve improved attachment of the over-growing repair tissue, we first roughened the upper surface of the elastomeric implant by punching vertical pores into its surface to facilitate tissue ingrowth. When this approach appeared to have the desired effect, we increased the implants' porosity in a more controlled manner, using a 3D printing-based fabrication process for the elastomer. We hypothesized that the 3D character architecture of the pores would induce not only vertical, but also horizontal fibrocartilage ingrowth, further fomenting tissue integration. In order to assess the mechanical performance after the introduction of porosity, the mechanical and biological proprieties of the implants were initially evaluated *in vitro*. Subsequently, the implants were tested in a pilot equine experimental model.

Material and Methods

The tested implants all were composed by a chondral component consisting of polycarbonate-urethane-urea biomaterial (PCUU elastomer) and a bone anchor consisting of polyetherketoneketone (PEKK). Four versions of the implant were manufactured and differed from each other only in the chondral component of its bi-layered structure. The previously tested version of the implant (Korthagen et al. 2019), with a smooth surface (smooth elastomer: SE) was compared in a study in two ponies to a new version in which the chondral component contained vertical micro-punched pores (punched elastomer: PE). The other two manufactured implants contained 3D-printed versions of the elastomeric urethane on top of the bone anchor component. They differed from each other only by the size of the printed pores (3D-printed large pores, 3D-L and 3D-printed small pores, 3D-S). These two versions were compared in a second pilot in two further ponies. Only the three new versions PE, 3D-L and 3D-S were tested mechanically and *in-vitro*, whilst all four versions (including SE) were tested *in-vivo*.

Preparation of chondral component of the implant

Punched elastomer (PE) and smooth elastomer (SE)

The SE implant was fabricated using a Polycarbonate-urethane-urea biomaterial (PCUU elastomer; PolyVation B.V., Groningen, the Netherlands) and was left untreated, as previously described (Korthagen et al. 2019). For the PE, 14 equally distributed pores with a diameter of 319 μm and a depth of 800 μm were punched into the elastomer with a custom-made owl. The optimum pore-size for cell-infiltration and practical manufacturing had been determined previously (Fig. S1).

3D-printing for 3D-L and 3D-S

The biomaterial ink was prepared by dissolving 180 mg/ml PCUU in 5 v/v% trifluoroacetic acid (TFA) in dichlorometh-

ane (DCM) (Sigma-Aldrich, Germany) for 24 hours. PCUU implants with smaller (3D-S) and larger (3D-L) pores were printed using an extrusion-based 3D-printing system (3DDiscovery, regenHu, Switzerland). The ink was transferred to a 3 mL syringe (Nordson EFD, USA) and extruded through a 27G conical nozzle, 0.2 mm (Nordson EFD, USA). Continuous ink deposition was achieved by applying a pneumatic pressure of 1.3 bar at 2 mm/s. Printability of the biomaterial ink was first evaluated by a filament fusion test according to a protocol described elsewhere (Golafshan et al. 2021) (Suppl. 1).

Structural characterization of the printed product

The surface morphology of the chondral component was evaluated using a stereomicroscope (Olympus SZ61) and the pore size of the 3D printed implants was analyzed using a Scanning Electron Microscope (XL30SFEG, FEI, USA) at an acceleration voltage of 10 kV. The porosity of the chondral components was evaluated by Image J (public source program) comparing area of pores and elastomer material.

Assessment of mechanical properties of PE, 3D-L and 3D-S

Implants were characterized under uniaxial compression using a universal testing machine (Zwick Z010, Germany) equipped with a 1 kN load cell (0.2 mm/min). Dynamic compression tests were performed by applying a ramp force to a height of 2 mm (equivalent to a strain of 20%) followed by a sinus wave deformation at a frequency of 0.1 Hz. The methods used to obtain all resulting mechanical parameters are described in the supplementary section (Suppl. 2).

In vitro cell culture of PE, 3D-L and 3D-S

Three groups containing each 3 sterilized samples of PE, 3D-L and 3D-S were seeded with equine cartilage progenitor cells at a density of 30,000 cells per sample ($d = 5 \text{ mm}$, $h = 1 \text{ mm}$) and cultured for 14 days as described (Suppl. A). Samples were taken at day 1 and day 14 after seeding (3 samples per group). At both timepoints, cell metabolic activity was quantified using the Alamar blue assay (ThermoFischer), following manufacturer's instruction, while DNA content was measured using a Qubit dsDNA BR assay (ThermoFisher) according to the manufacturer's protocol. Imaging techniques are described in the supplementary material and methods (Suppl. 3).

Fabrication of the osteochondral implants

The bone component of the osteochondral implant was made of polyetherketoneketone (PEKK) that anchors the implant to the native subchondral bone. In order to fixate the PE on the PEKK bone anchor, a layer of 0.2 mm PCUU was compression-moulded onto the PEKK after which the PE was 'glued' on top of that using a 5%TFA/DCM solution. The SE was manufactured identically.

For the 3D-L and 3D-S, the PEKK was placed in a negative mould and PCUU was printed on top of the mould. The fabrication process is schematically shown in Fig. S3.

In-vivo evaluation

Experimental set up

In a first experiment the SE was compared to the PE in two ponies (each stifle receiving a different implant). The diameter of these plugs was 6 mm and total height was 7 mm. In the second experiment the two 3D printed versions were compared in two ponies. The diameter of these plugs was increased to that of a critical-size defect of 10 mm and total height was 7 mm. The animals were female adults, with mean age 5 years (range 4 to 9), weighing between 200 and 270 kg. Further inclusion criteria are described in Supplementary material and methods.

The experiments were carried out with the approval of the Animal Welfare Body Utrecht (IvD Utrecht, Project number AVD1080020186885).

Surgical procedure

First experiment – SE vs PE

Pre-operative preparation and anesthesia followed routine protocols (see Supplementary material and methods). After surgical preparation, bilaterally a medial femoro-patellar and a femoro-tibial arthrotomy were performed and 4 implants per pony were placed, 2 in each stifle. For both ponies a SEs implant of 6 mm in diameter was placed in the medial trochlea and another one in the medial condyle of the right stifle. Similarly, PEs implants of the same diameter and in the same two locations were placed in the left stifle, again for both ponies. The defects were made on the axial side of the medial trochlea, halfway between the apex of the patella and the most proximal aspect of the tibial tuberosity and on the weightbearing surface of the medial femoral condyle. The osteochondral defects (6 mm diameter and 7.5 mm depth) were created using a customized drill bit and drill sleeve. The rim of the round defect was trimmed until a clean perpendicular cartilage border was obtained. The implant was inserted manually and carefully press-fitted with a custom-made punch until the elastomer was about 0.5 mm below the surrounding cartilage surface. The depth of placement was assessed subjectively. After flushing the surgical site with saline, the joint was closed in 4 layers and a stent was placed over the incision.

Second experiment – 3DP-L vs 3DP-S

To test the two 3D-printed implant versions (both 10 mm in diameter), a similar procedure was performed in two additional animals. In total 2 implants were used per pony. A 3DP-L was placed in the right stifle in the medial trochlear ridge and the 3DP-S in the left stifle at the same site.

Post-mortem evaluation

After 5 weeks, general anesthesia was induced with midazolam (0.06 mg/kg) and ketamine (2.2 mg/kg) and the ponies

were humanely euthanized with an overdose of Pentobarbital. The joints were exposed and macroscopic assessment performed by visual inspection and palpation. Any signs of kissing lesions or macroscopic changes in the joint were recorded. It was attempted to displace the overgrowing tissue by hand with an arthroscopic probe. When the tissue appeared firmly attached to the elastomer, a rectangular osteochondral block of cartilage and bone containing the plug was harvested. The blocks were fixated in formalin and later embedded in Polymethylmetacrylate (PMMA). After hardening, the PMMA embedded plug was cut with a Leica 4 SP1600 Saw Microtome system (Leica) to yield 50–60 µm sections and stained with basic fuchsin-methylene blue. The sections were analyzed for signs of tissue ingrowth into the pores or into the 3D-printed structure of the elastomer, respectively. A sagittal section of one of the pores of each implant was used to measure the surface of the tissue core in the pore as a quantitative approximation of tissue ingrowth. This ingrowing tissue area was measured three times with a digital image analysis tool (Image J) and averaged.

Statistical analysis

Statistical analyses of mechanical properties and in vitro culture were performed using GraphPad prism V6. Data were represented as mean ± standard deviation. The significance of differences between the three groups was assessed using a one-way ANOVA and post-hoc Tukey's test. Differences were considered significant at a probability error (p) of $p < 0.05$.

Results

Implant fabrication

The osteochondral implants with enhanced porosity were successfully generated using two techniques: by the introduction of punched pores and by 3D-printing of the elastomeric material (Fig. 1). Prior to 3D-printing of the implants, the filament fusion investigation of the elastomeric biomaterial ink revealed that the minimum inter-fiber spacing for a single layer that could be achieved was 800–1000 µm (Fig. S2). Based on this, two pore sizes (0.8 mm and 1 mm) were selected for chondral implant fabrication. The experimental average pore diameter achievable for multiple layers of 3D-S and for 3D-L versions was 690 µm and 775 µm, respectively. The overall average porosity of the cartilage phase of the PE implants was 2.1 %, while for the 3D-S and 3D-L this was 40.2 % and 67.4 %, respectively (Fig. 1B). Underscoring the significant differences in the surface morphology of the three different implants (Fig. 1C-E).

Mechanical properties

The stress-strain curve of the various implants under quasi static compression is shown in Fig. 2A. The increase of porosity resulted in a decrease in both elastic modulus and yield stress of the elastomers. The elastic modulus of PE, 3D-S, and 3D-L are 24.9 MPa, 16.1 MPa, and 3.8 MPa, respectively

(Fig. 2C). Moreover, the yield stress of PE, 3D-S, and 3D-L are 23.3 MPa, 8.4 MPa, and 4.2 MPa, respectively (Fig. 2D). The strain energy for PE was 6 times higher than for the 3D-L (Fig. 2E). Further, recovery and energy dissipated under cyclic loading at 20% strain was evaluated for 20 cycles. Interestingly, all three elastomer versions could resist over 20 cycles

of compression without sign of any permanent deformation (Fig. 2F). Moreover, the recovery percentage of the elastomer was the highest for the elastomer with the higher porosity (Fig. 2G). The energy dissipation was inversely proportioned to the porosity of the implant, being highest for the punched pore elastomer (PE).

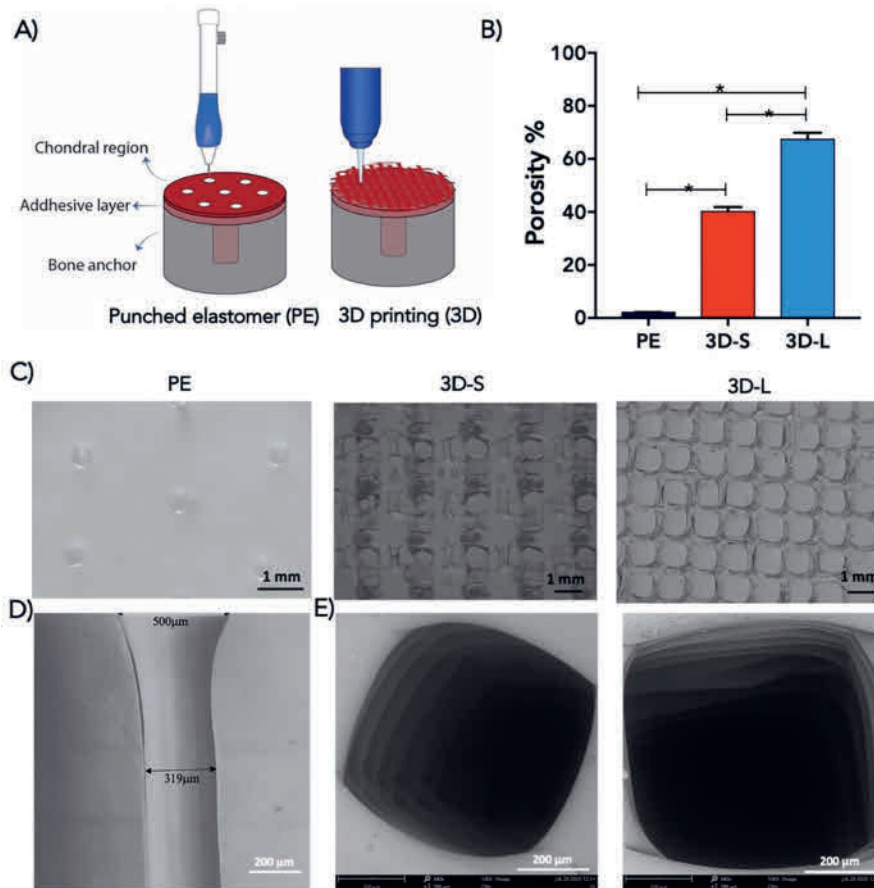


Fig. 1 A) Illustration of the fabrication procedure of the implants. B) The porosity of the chondral component for all the versions of the implants. C) Stereomicroscopic images of the implants. D) Microscopic transverse section of PE. E) SEM cross-sectional images of the pores of the implants 3D-S and 3D-L.

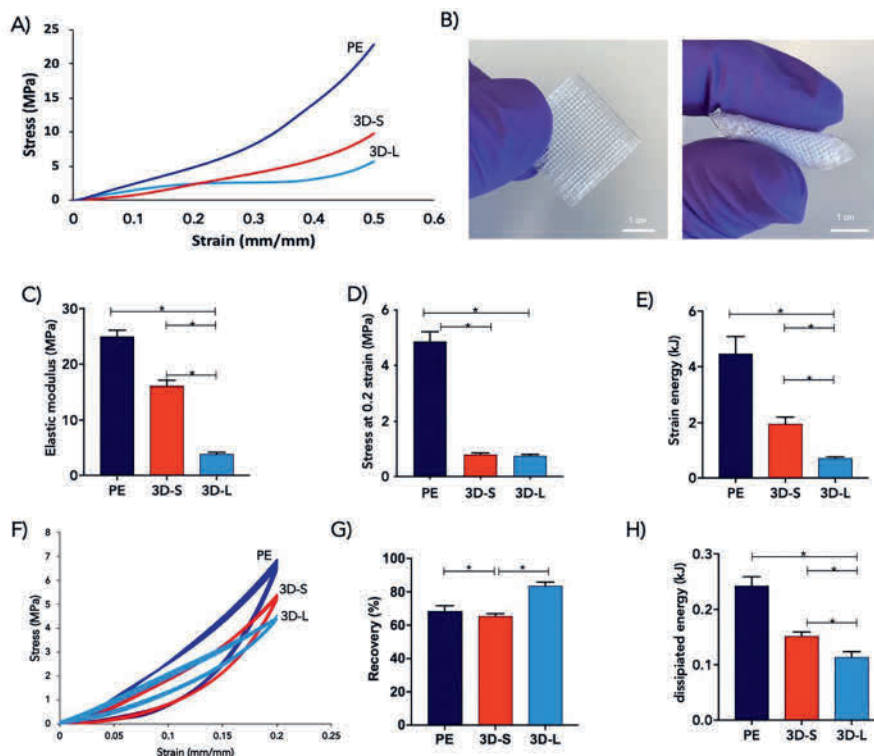


Fig. 2 A) Longitudinal compression profile of implants. B) Photographic illustration of the elastic behavior of the implants. C) Elastic modulus, D) Stress at 0.2 mm/mm strain, and E) strain energy from compressive loading profile for various implants. F) The cyclic compression profile for various implants (20 cycles). G) recovery and H) Dissipated energy of the implants after each test.

Cytocompatibility and cell infiltration of porous chondral parts

To evaluate the cytocompatibility and the cell infiltration capability of the implants, articular cartilage progenitor cells were cultured on the implants for 14 days. The metabolic activity analysis confirmed that the cells were active during the whole duration of the *in vitro* study (Fig. 3A). Moreover, no negative effects on cell activity were observed as a result of the use of a solvent-based extrusion printing approach. The quantitative DNA measurements revealed an increase of DNA over time for all the implants from day 1 to day 14. (Fig 3B). Cell nuclei staining evaluated the infiltration of the cells into the pores of the implant and were visible after 14 days of culture (Fig 3C).

Surgery and clinical outcome

In the first *in vivo* pilot, comparing SE and PE, all 8 implants (4 per pony) were placed successfully in the two desired locations (medial condyle and medial trochlea). In the subsequent *in vivo* pilot, comparing 3D-L and 3D-S, 4 plugs of 10 mm diameter were to be placed in the medial trochlea. However, two out of four implants could not be completely placed below the articular surface. In these cases, one third of the implant surface was flush with the articular surface, but not below the surface, as desired. Post-operative recovery was good in all ponies. After removing the surgical stents on the third day post-operatively, the animals showed unhindered motion. Surgical wounds healed uneventfully, and a mild effusion of all treated stifle joints remained throughout the study. At 5 weeks the animals did not show any signs of lameness. Oblique radiographs depicting the medial trochlea showed the implant in place with no to mild sclerosis and no signs of lysis in the surrounding bone for all three types of implants (Fig. 4C).

Macroscopic outcome and subjective mechanical testing

At necropsy, 5 weeks after surgery, the implant location was clearly visible. In the SE vs PE experiment, the implants on the medial trochlea were covered with newly-formed tissue, which differed in color and thickness between the two animals (Fig. 4D). When being pushed with a metallic probe,

the tissue covering the SE, slid off the surface with no resistance, once it was not anymore attached to adjacent cartilage. In the other implant with punched pores, the tissue could not be moved over the surface and the whole implant unit could be conserved intact for histological evaluation. In the femoral condyles, only partial covering of the implant from the borders was visible. This tissue appeared thicker and glossier than the tissue covering the medial trochlea (Fig. 5). The difference in resistance of repair tissue to manual displacement with the probe between the two types of implant was the same as for the trochlea implantation sites.

In the second experiment comparing the two 3D printed implants, two out of four implants on the medial trochlear showed overgrowth of tissue (Fig. 4D). The two implants that could not be placed correctly during surgery were covered only by 50% in one case and not covered at all in the other case. The portion of the implant that had been flush with and not below the surface, was slightly protruding at the post-mortem examination. The newly overgrown tissue of all implants resisted mechanical probing and could not be dislocated or detached from the elastomer. There was no macroscopic difference between the two 3D-printed versions of the elastomer with different pore sizes.

Histologic outcome

Histology revealed that the implants from the SE vs PE experiment showed ingrowth of tissue into the punched (PE) pores (Fig. 6). Cells could be seen within the ingrowing tissue. Depth of ingrowth was 100 μm . The transition to the surrounding cartilage was confluent, without step formation or interruption, even though a clear demarcation between native and repair tissue could be observed. Trabecular bone was surrounding the PEKK implant and new bone formation around the PEKK was seen in some sections. In the experiment comparing the two 3D-printed versions, tissue ingrowth occurred in both 3D-L and 3D-S. Depth of ingrowth was 100 μm in both versions (Fig. 6). No tissue was seen in deeper layers and no horizontal ingrowth was visible. Also here, the bone was tightly surrounding the PEKK and newly formed bone could be detected adjacent to the PEKK.

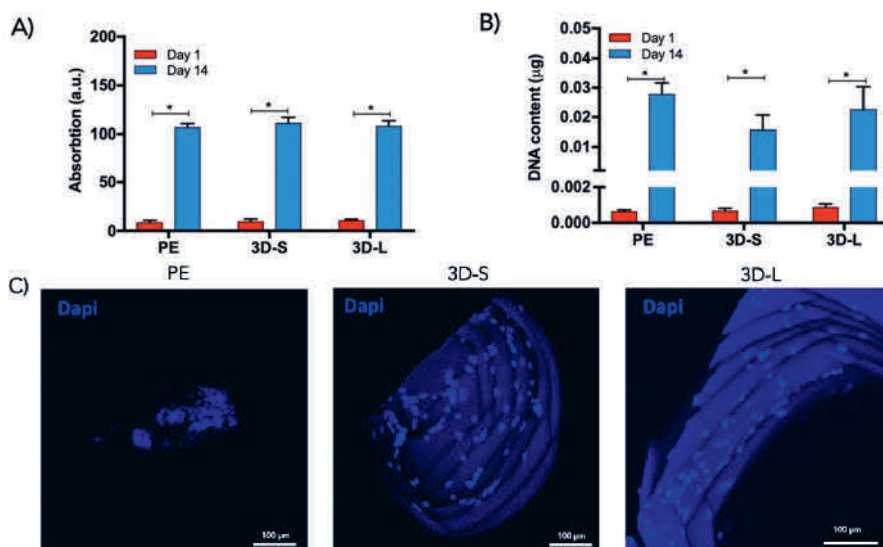


Fig. 3 A) Metabolic activity and B) DNA content of Articular Cartilage Progenitor Cells (ACPCs) during 14 days of culturing. C) DAPI staining of infiltrated ACPCs within the pores after 14 days of culturing.

The largest transectional surface area of vertical tissue ingrowth through the porosity was measured in the larger 3D-printed version of the implant (Fig. 6D)

Discussion

The main hypothesis that roughening the surface of the elastomer would allow ingrowth of the repair cartilage, resulting in better adherence to the implant, was confirmed. This is already a proven strategy in bone repair, where osteoconductive materials preferably have a porous surface (Cornell 1999).

In the attempt to test different pore structures for increased cell infiltration and better mechanical stability of the repair tissue-implant complex, two different concepts of surface manipulation were tested. With both pore-sizes of $319\mu\text{m}$ and $775\mu\text{m}$ the repair tissue appeared to be tightly connected to the implant and subjectively did not respond differently to manual probing. Admittedly, assessment was qualitative only; in this pilot study no quantitative measurements of maximal shear force resistance were carried out as larger sample numbers would be required to study significance. It lies at hand, however, that larger volumes of ingrowing tissue relate to stronger anchorage of the tissue. The quantity of tissue growing into the pores, was clearly larger in the 3D-L.

The 3D-printed version of the elastomer showed vertical, but no horizontal ingrowth respective to the articular surface, and reached only $100\mu\text{m}$ of depth (equal to or even less than 10% of the thickness of the layer of hyaline cartilage in most diarthrodial joints in both horses and humans) in both varieties of the printed elastomer. This might be explained by the fact that in contrast to the native extracellular matrix as found in normal cartilage, the ingrowing repair tissue was surrounded by an in-

ert material with no fluid dynamics. Therefore, the physiologic “pumping mechanism” for nutrient diffusion might have been impaired in deeper layers of the elastomeric 3D structure, preventing deeper ingrowth.

By increasing the porosity of the elastomer in a controlled way, the elastic modulus and yield stress of the elastomer decreased. The elastic modulus ranged from 24.9 ± 1.2 MPa in the punched version to 3.8 ± 0.4 MPa in the large pore 3D-printed version. This last value is still well above the elastic modulus for native cartilage (0.45 to 0.80 MPa (Athanasίου et al. 1991)). To verify the elastic behavior of the elastomer, a repetitive strain of 20% was applied, representing a high-level strain during human activities (Sutter et al. 2015, Liu et al. 2010) All three elastomer versions could resist the compressive forces over 20 cycles, without signs of permanent deformation. The recovery percentage of the elastomer was highest for the elastomer with higher porosity whilst the energy dissipation was inversely proportional to the porosity of the implant, being highest for the punched pore elastomer. These results show that the larger total ingrowth volume in the most porous implant did not mean a negative trade-off with respect to its biomechanical characteristics.

In the SE vs. PE experiment the implants on the femoral condyles showed scarce tissue overgrowth when compared to the medial trochlear ridge. The relative distribution of compressive and shear loading across the compartments of the stifle joint varies (Halley et al. 2014, Changoor et al. 2006, Moore and Burris 2015). This could explain why tissue overgrowth varied depending on the site of implantation. In the future development of this implant, a site-specific manipulation of porosity might be warranted in order to mimic more closely the local mechanical conditions.

The concept of this treatment would dictate to place the implant completely below the articular surface, in order to

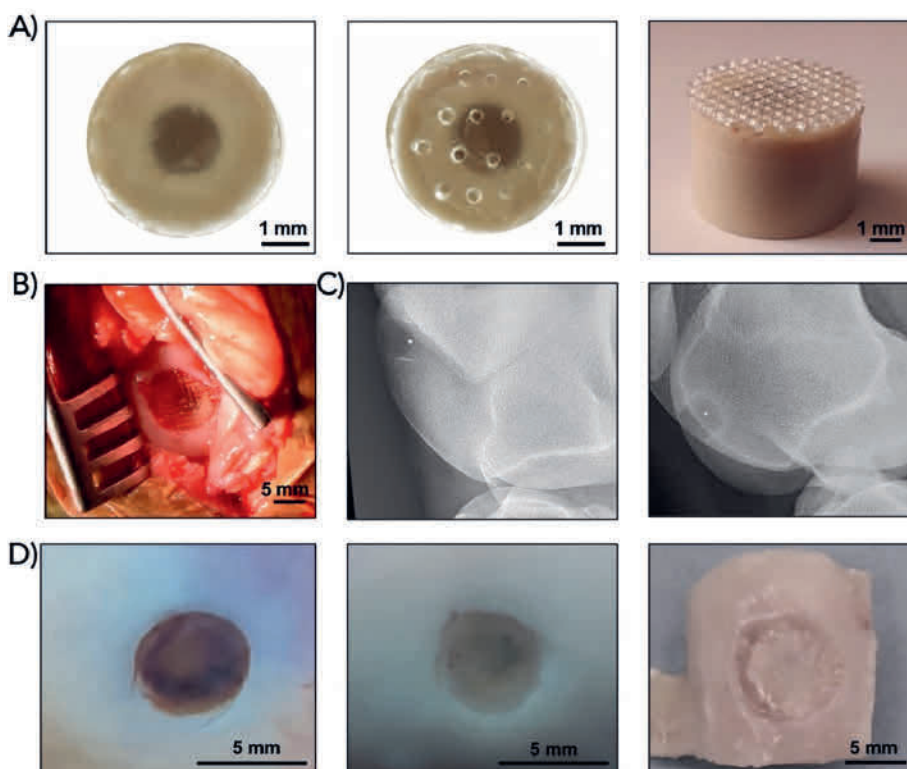


Fig. 4 Three versions of the tested implant. Only the elastomer (chondral component) of the implant varied: smooth elastomer (SE), elastomer with punched pores of $319\mu\text{m}$ (PE) and 3D-printed with pores of $690\mu\text{m}$ and pores of $775\mu\text{m}$ (3D-S and 3D-L; only one version of the 3D printed implants is depicted). B) printed elastomer implanted in the axial aspect of the medial trochlea, 0.5 mm below the articular surface. C) Craniolateral-caudomedial oblique radiographs of two stifles with implant with punched pores and large 3D printed pores. The radiodense area in the middle of the implant represents a metal marker, that was integrated in the implant during fabrication D) Smooth, punched and 3D printed implants on the axial aspect of the medial trochlea, covered with repair tissue, after 5 weeks.

allow tissue overgrowth. This was not possible for two of the 10 mm diameter plugs. Strategies to match the curvature of implants to that of the treated articular surface and to improve the implantation angle are being increasingly sought for (Heuveljans et al. 2018, Martinez-Carranza et al. 2014, Kirker-Head et al. 2006). The application of a curved radius to the elastomer surface might achieve an improved fitting of the construct below the articular surface in a controlled manner. Hereby a better integration of the entire circumference of the implant could be achieved. As signaled earlier, a major drawback of our approach/design was the lack of objective biomechanical testing of the tissue-covered implant in the post-mortem assessment. Also, a larger number of animals would be necessary in order to provide objectively

measured parameters, that can be compared to values of native cartilage or to other repair techniques.

It can be concluded that the surface roughening approach that was investigated in this study indeed succeeded in good adherence of the neo-tissue on the elastomer. This was true for both the punched holes and the printed versions with no visible differences between both approaches. The fact that outcome was similar for both the 6 mm and the 10 mm plugs was encouraging, as the last size is of more clinical relevance than the smaller size. The printing approach resulted in a larger volume of tissue ingrowth and appeared to facilitate manipulation of the biomechanical characteristics of the elastomer. The latter observation is interesting and po-

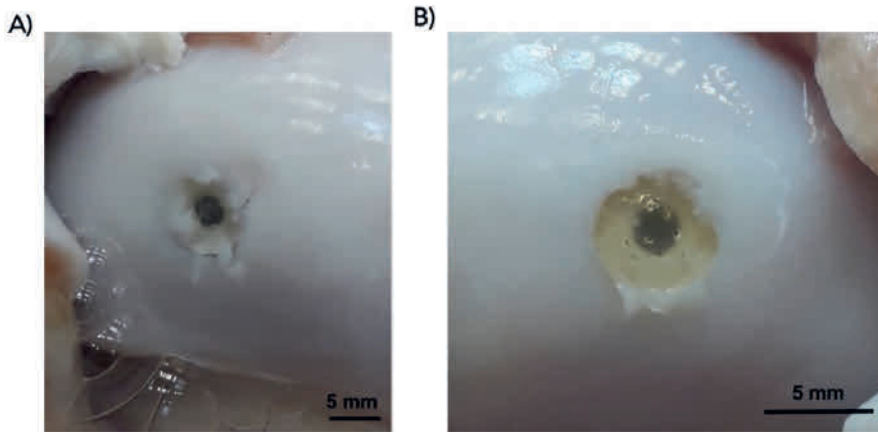


Fig. 5 Implant in situ on the weight bearing surface of the medial femoral condyle, only partially covered with tissue after 5 weeks. A) smooth elastomer B) punched elastomer.

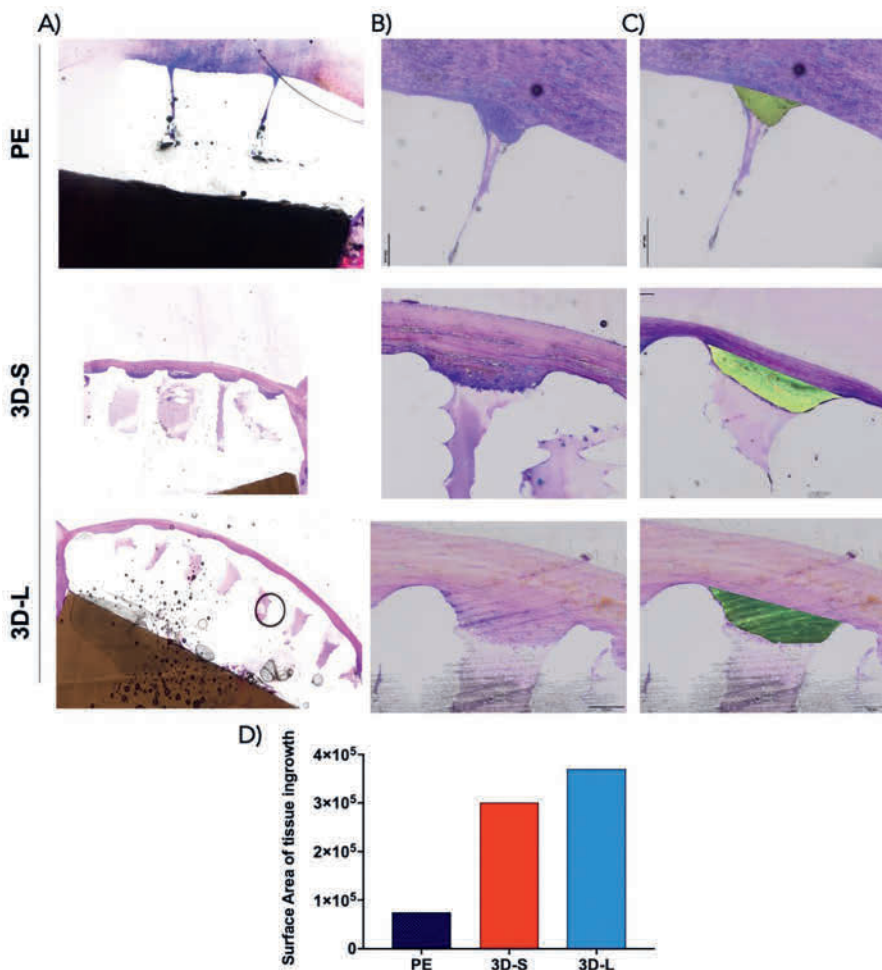


Fig. 6 Representative images of polymethylmethacrylate (PMMA) embedded slides of implants of 6 mm in diameter with microdrilled pores and of polymethylmethacrylate (PMMA) embedded slides of implants with 3D printed elastomer (3D-S and 3D-L), after 5 weeks (1.25x and 2x magnification). The bulging artifact of the elastomer seen in the images is due to the PMMA imbedding process. D) measurement of area of vertical tissue ingrowth in the three implant versions.

tentially enables fine-tuning of the biomechanical properties of the implant depending on the specific requirements for a given location. Considering the short-termed nature of this experiment, the tested implants all showed good mechanical performance *in vitro* and subjectively also *in vivo*. Similarly, from a biological and clinical point of view, no adverse effects were observed. This favorable outcome opens the way for a long-term experimental evaluation of the construct in which the improved adherence and stability of the repair tissue needs to be assessed and quantitatively analyzed in a larger group of animals.

Conflict of interests

Gied Hermsen and Ward van Buul have a financial relationship with JointSphere BV but had no influence on the interpretation of the results.

Declaration of funding

JointSphere BV covered the material costs of the study.

Ethical approval of animal experimentation

This experiment has been carried out with the approval of the Animal Welfare Body Utrecht (IvD Utrecht,) under the Project number AVD1080020186885 with validity until the 31-01-2024 and work protocol number: 6885-2-1.

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Supplementary material and methods

1. Filament fusion test

For the filament fusion test, the elastomer was printed in meandering patterns composed of parallel strands at increasing spacings, from 0.5 mm to 1 mm (Fig. S2) After taking pic-

tures, the fused segment length (fs) at each filament distance (fd) were measured using ImageJ and normalized by dividing fs by the average of filament thickness (ft) to avoid the effect of filament thickness variation. At least 3 measurements used for the quantification and the images were recorded by a stereomicroscope (Olympus SZ61, magnification $4.2\times$, resolution 2040×1536 pixels) immediately after printing.

2. Mechanical characterization of implants

The elastic modulus (defined as the slope of the linear region from 0.1 to 0.2 mm/mm), the stress (defined as the stress at 0.2 mm/mm strain), and the strain energy (defined as the absorbed energy by the scaffolds up to yield stress) were determined.

Further, the elastic behavior of the implants, was assessed under dynamic compression. From the dynamic tests, the dissipated energy was assessed by the loss of energy after the unloading. In addition, the recovery was calculated by dividing the loaded energy of the 20th cycle by the loaded energy of the 1st cycle.

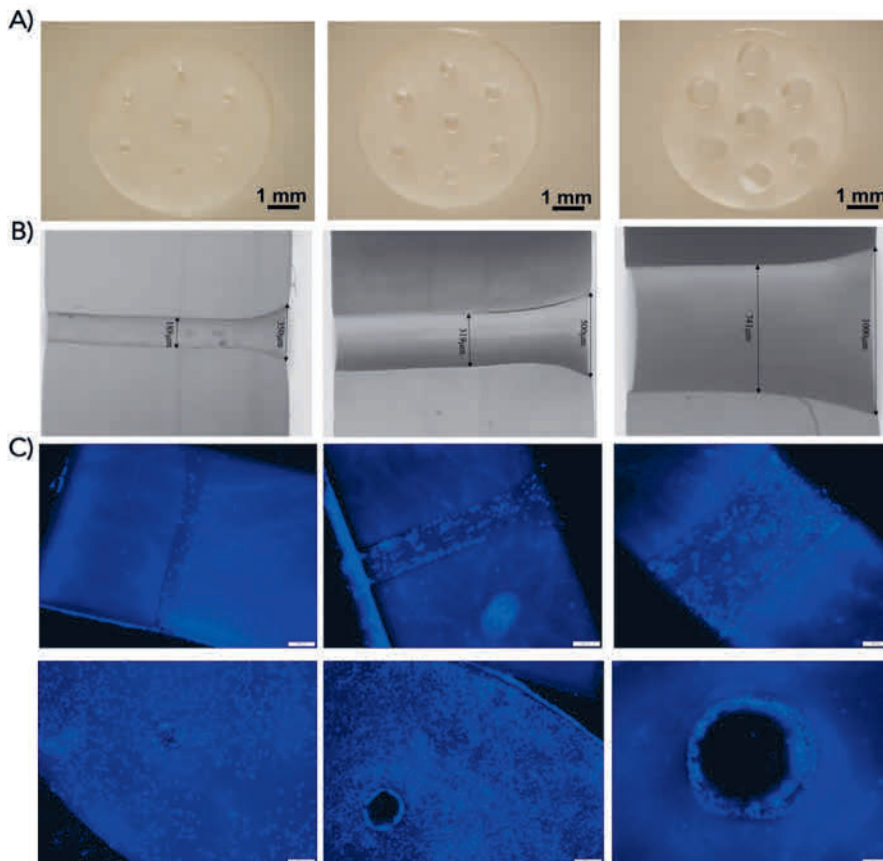


Fig. S1 A) Images of the punched elastomer with different pore sizes. B) The cross-section images of the punched elastomer to show the inner diameter. C) DAPI staining of in pores infiltrated ACPCs after 14 days of culturing for the punched elastomers with different pore sizes.

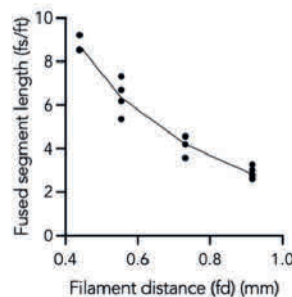
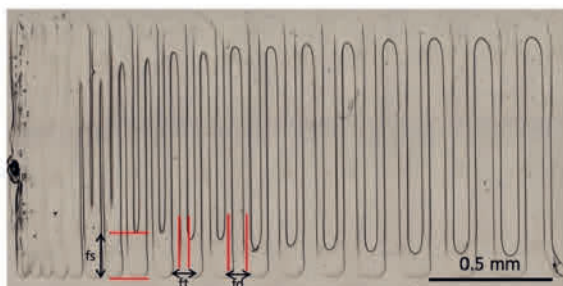


Fig. S2 Filament fusion test for printability evaluation of PCUU. fs: filament segment length; ft: filament thickness; fd: filament distance.

Culturing protocol

The implants were cultured in DMEM (high glucose, GlutaMAX-TM, pyruvate) (Gibco, USA), 10% FBS (Biowest, France), 10 µl/ml pen/strep (Gibco, USA), 5 µl/ml ASAP (Sigma, USA), and 1 µl/ml (-FGF (R&D Systems, USA). Medium was changed every 3 days.

3. Cell imaging technique

In order to image the cells within the scaffolds, the cells were fixed in formalin, washed with 0.2% Triton in PBS for 10 min and stained with DAPI solution. Subsequently the cells were imaged with a confocal microscope (Leica SP8X Laser Scanning, Germany) with 358 nm and 461 nm excitation filters, and 3 samples were analysed per group per timepoint.

4. Inclusion criteria and surgical pre- and post-operative protocol

The ponies were admitted to the clinic 2 weeks prior to surgery to acclimate to the environment. They were fed on hay (2% body weight) and had free water access. Clinical lameness examination was performed by the author assist-

ed by a quantitative gait analysis device (EquiMoves). All animals were clinically sound and lame-free. Radiographic images on four projections of the stifle (antero-posterior, latero-medial, dorsolateral-caudomedial and dorsomedial – caudolateral) were obtained pre-operatively. Only ponies with normal radiographic appearance were included in the study. On the day of surgery, ampicillin (10–15 mg/kg IV), gentamicin (6.6 mg/kg IV) and meloxicam (0.6 mg/kg) were administered through a previously placed jugular vein catheter. The ponies were then sedated with detomidine (10 mcg/kg IV) and morphine (0.1 mg/kg IV). General anesthesia was induced with midazolam (0.06 mg/kg) and ket-

amine (2.2 mg/kg) and maintained with isoflurane in oxygen through endotracheal tubing and a continuous rate infusion (CRI) of detomidine (10 mcg/kg/h) and ketamine (0.5 mg/kg/h).

Postoperatively a single dose of procaine penicillin (20 mg/kg im) was administered and meloxicam (0.6 mg/kg) and morphine (0.1 mg/kg) were administered orally twice a day for 3 days. Ponies were daily assessed for clinical parameters and lameness and were box-rested for 5 weeks. A lameness examination was performed by the author assisted by a quantitative gait analysis device (EquiMoves®)

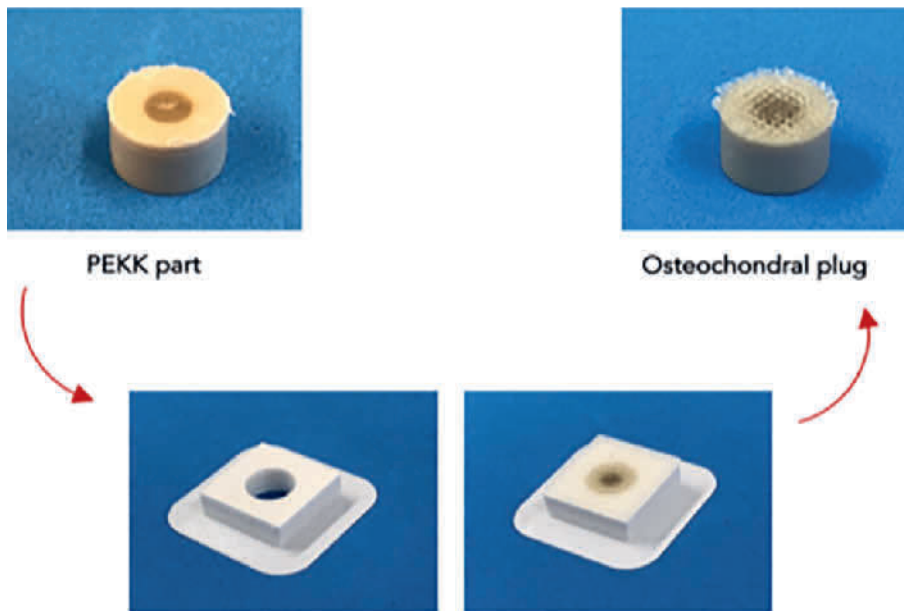


Fig. S3 3D fabrication procedure of the 3D-printed implants.