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## On a comparison of Newton–Raphson solvers for power flow problems



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### ABSTRACT

A general framework is given for applying the Newton–Raphson method to solve power flow problems, using power and current-mismatch functions in polar, Cartesian coordinates and complex form. These two mismatch functions and three coordinates, result in six possible ways to apply the Newton–Raphson method for the solution of power flow problems. We present a theoretical framework to analyze these variants for load (PQ) buses and generator (PV) buses. Furthermore, we compare newly developed versions in this paper with existing variants of the Newton power flow method. The convergence behavior of all methods is investigated by numerical experiments on transmission and distribution networks. We conclude that variants using the polar current-mismatch and Cartesian current-mismatch functions that are developed in this paper, performed the best result for both distribution and transmission networks.

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### 1. Introduction

A power flow computation that determines the steady state behavior of the network is one of the most important tools for grid operators. The solution of a power flow computation can be used to assess whether the power system can function properly for the given generation and consumption. Therefore, power flow computations are performed in power system operation, control and planning.

The power flow or load flow problem is the problem of computing the voltage *magnitude*  $|V_i|$  and *angle*  $\delta_i$  in each bus of a power system where the power generation and consumption are specified. Over the years, various power flow solution techniques [1–15] have been developed on transmission networks. Gauss–Seidel (G–S), Newton power flow (N–R) and Fast Decoupled Load Flow (FDLF) based algorithms are the most widely used methods for the solution of transmission power flow problems. In practice, the Newton power flow method is preferred in terms of quadratic convergence and improved robustness [16]. Furthermore, many new methods [17–28] have been developed for distribution power flow problems and generally they are divided into two main categories such as modification of conventional power flow solution methods (G–S, N–R, FDLF) and Backward–Forward Sweep (BFS)-based algorithms. Several reviews on distribution power flow solution methods can be found in [29–32].

In this paper, we focus on the Newton based power flow methods for balanced transmission and distribution networks. Depending on problem formulations (power or current mismatch) and coordinates (polar, Cartesian and complex form), the Newton–Raphson method can be applied in six different ways as a solution method for power flow problems. These six versions of the Newton power flow method are considered as the fundamental Newton power flow methods from which the further modified versions [8–15] are derived. Table 1 shows the previously published papers considering each variation of the Newton power flow method.

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**Table 1**  
Known versions of the Newton power flow method.

Mismatch formulation	Coordinates		
	Polar	Cartesian	Complex form
Power	[2]	[33]	[34]
Current	[35]	[35,36]	

The most widely used version is the Newton power flow method using the power-mismatch and polar coordinates which is introduced in [2]. In this method, the reactive power mismatch  $\Delta Q$  and the voltage magnitude correction  $\Delta V$  for each generator (PV) bus are eliminated from the Jacobian matrix equations and therefore the order of the equation is  $(2N - N_g - 2)$ .

In the version using the power-mismatch and Cartesian (rectangular) coordinates introduced in [33], the reactive power mismatch  $\Delta Q$  is not eliminated from the Jacobian matrix equations for each PV bus but replaced by a voltage-magnitude-squared mismatch equation:

$$\Delta|V|^2 = (|V|^{sp})^2 - (V^r)^2 + (V^m)^2. \tag{1}$$

where  $|V|^{sp}$  is specified voltage magnitudes and  $V^r$  and  $V^m$  are the real and imaginary parts of the complex voltages respectively. Therefore, the order of the Jacobian matrix equation is  $(2N - 2)$  and it is concluded in [33] that the method is slightly less reliable and less rapid in convergence than the polar version developed in [2].

Although it is mentioned in [2,16] that the complex power flow formulation does not mathematically lead to an analytic function of the complex voltage because of conjugate terms, the paper [34] investigated the version of the Newton power flow method using the power-mismatch in complex form. In paper [34], the Jacobian matrix equations are developed in complex form for each load (PQ) bus whereas two separate equations are created for each PV bus. The correction values of complex voltage for the PQ and PV buses are computed separately using different tolerances at each iteration. However, it is preferred to calculate correction values for both PQ and PV buses using common Jacobian matrix equations and the same tolerance.

The version using the current-mismatch and a mix of Cartesian and polar coordinates is discussed in [35]. In this method, each PQ bus is represented by two equations that are constructed from the real and imaginary parts of the complex current-mismatch function. A PV bus is represented by a single active power-mismatch  $\Delta P$  and the voltage-magnitude-squared mismatch equation (1). The order of the Jacobian matrix equation is  $(2N - 2)$  and it is concluded in [16] that these versions perform less satisfactorily than the power-mismatch versions.

The version using the current-mismatch and Cartesian coordinates is considered again in [36]. This method introduces a new dependent variable  $\Delta Q$  for each PV bus and additional equations relating the corrections in polar and Cartesian coordinates:

$$\Delta|V| = \frac{V^r}{|V|} \Delta V^r + \frac{V^m}{|V|} \Delta V^m \tag{2}$$

$$\Delta\delta = \frac{V^r}{|V|^2} \Delta V^m - \frac{V^m}{|V|^2} \Delta V^r. \tag{3}$$

Using Eqs. (2) and (3), this method makes the Jacobian matrix equation square in order to have a unique solution. In this method, the real  $\Delta I^r$  and imaginary  $\Delta I^m$  current-mismatch functions are expressed in terms of the real  $\Delta P$  and reactive  $\Delta Q$  power-mismatch functions. Then the reactive power-mismatch  $\Delta Q$  is considered as a dependent variable for each PV bus and computed at each Newton iteration. Minor attempts were made to speed up the solution method using a partly constant approximation of the Jacobian during the iterations, but the results were not encouraging [36].

We did not find any discussion covering the Newton power flow method using the current-mismatch in complex form.

All variations of the Newton power flow method are developed by different researchers in different ways. This paper aims to discuss all six versions of the Newton power flow method using a common framework and to introduce new developments to improve the performance of other versions besides the most used version using the power-mismatch and polar coordinates [2]. Major improvements were done by us in Cartesian power-mismatch, polar current-mismatch and Cartesian current-mismatch versions. In versions using Cartesian coordinates, Eqs. (2) and (3) are used for PV buses instead of the voltage-magnitude-squared mismatch equation (1). In case of versions using the current-mismatch regardless of the choice of the coordinates, the reactive power  $Q$  is considered as a dependent variable for each PV bus. Thus, we compute the correction  $\Delta Q$  at each iteration and update  $Q$  using the computed corrections. In case of the Cartesian power-mismatch, the order of the system is decreased to  $(2N - N_g - 2)$  whereas [33] uses a system with the order  $(2N - 2)$ . The complex current-mismatch and complex power-mismatch versions are developed only for PQ buses.

This paper is structured as follows. In Section 2, a mathematical model of a power system is introduced briefly. Section 3 mathematically describes the power flow problem. The Newton–Raphson method and its all six versions for the solution of power flow problems are explained in Section 4. The numerical results of all solution techniques on balanced distribution and transmission networks, are presented in Section 5. Finally, the conclusion is given in Section 6.

**Table 2**  
Network bus type.

Bus type	Number of buses	Known	Unknown
Slack node or swing bus	1	$ V_i , \delta_i$	$P_i, Q_i$
Generator node or PV bus	$N_g$	$P_i,  V_i $	$Q_i, \delta_i$
Load node or PQ bus	$N - N_g - 1$	$P_i, Q_i$	$ V_i , \delta_i$

## 2. Power system model

Power systems are modeled as a network of buses and transmission lines whereas a network bus represents a system component such as a generator, load and transmission substation etc. There are three types of network buses such as a slack bus, a generator (PV) bus and a load (PQ) bus. Each bus in the power network is fully described by the following four electrical quantities:

- $|V_i|$ : the voltage magnitude
- $\delta_i$ : the voltage phase angle
- $P_i$ : the active power
- $Q_i$ : the reactive power

Depending on the type of the bus, two of the four electrical quantities are specified as shown in Table 2:

Here,  $i$  is the index of the bus,  $N_g$  is the number of generator buses and  $N$  is the total number of buses in the network. For more details on the power system model we refer to [37].

## 3. Power flow problem

The power flow, or load flow, problem is the problem of computing the voltage magnitude  $|V_i|$  and angle  $\delta_i$  in each bus of a power system where the power generation and consumption are given. According to the Kirchhoff's Current Law (KCL), the relation between the injected currents and bus voltages, is described by the admittance matrix  $\mathbf{Y}$ :

$$I = \mathbf{Y}V \Leftrightarrow \begin{bmatrix} I_1 \\ I_2 \\ \vdots \\ I_N \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} & \cdot & \cdot & Y_{1N} \\ Y_{21} & Y_{22} & \cdot & \cdot & Y_{2N} \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ Y_{N1} & Y_{N2} & \cdot & \cdot & Y_{NN} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ \cdot \\ V_N \end{bmatrix} \tag{4}$$

where  $I_i$  is the injected complex current,  $V_i$  is the complex voltage at bus  $i$  and  $Y_{ij}$  is the element of the admittance matrix. From Eq. (4), the injected current at bus  $i$  can be written as:

$$I_i = \sum_{k=1}^N Y_{ik} V_k. \tag{5}$$

The mathematical equations for the power flow problem are given by:

$$S_i = V_i I_i^* \tag{6}$$

$$= V_i \sum_{k=1}^N Y_{ik}^* V_k^* \tag{7}$$

where  $S_i$  is the injected complex power at bus  $i$  and  $I_i^*$  is the complex conjugate of the injected current. Mathematically, the power flow problem comes down to solving a nonlinear system of equations where all variables are given in complex numbers.

## 4. Newton power flow solution methods

The Newton based power flow methods use the Newton–Raphson (NR) method that is applied to solve a nonlinear system of equations  $F(\vec{x}) = 0$ . In NR method, the linearized problem is constructed as the Jacobian matrix equation

$$-J(\vec{x})\Delta\vec{x} = F(\vec{x}) \tag{8}$$

where  $J(\vec{x})$  is the square Jacobian matrix and  $\Delta\vec{x}$  is the correction vector. The Jacobian matrix is obtained by  $J_{ik} = \frac{\partial F_i(\vec{x})}{\partial x_k}$  and is highly sparse in power flow applications [2,16]. The iteration process of the Newton based power flow method is shown in Algorithm 1.

**Algorithm 1** Newton’s power flow method

- 1:  $h := 0$
- 2: given initial iterate  $\vec{x}^0$
- 3: **while** not converged **do**
- 4:   solve the correction  $-J(\vec{x}^h)\Delta\vec{x}^h = F(\vec{x}^h)$
- 5:   update iterate  $\vec{x}^{h+1} := \vec{x}^h + \Delta\vec{x}^h$
- 6:    $h := h + 1$
- 7: **end while**

**Table 3**  
Variable  $\vec{x}$  in different coordinates.

Coordinates	Variable $\vec{x}$
Polar ( $V_i =  V_i e^{i\theta_i}$ )	$[\delta_1, \dots, \delta_N,  V_1 , \dots,  V_N ]^T$
Cartesian ( $V_i = V_i^r + iV_i^m$ )	$[V_1^m, \dots, V_N^m, V_1^r, \dots, V_N^r]^T$
Complex form ( $V_i$ )	$[V_1, \dots, V_N]^T$

Traditionally, direct solvers are used to solve the Jacobian matrix equation (8). Convergence of the method is mostly measured in the residual norm  $\|F(\vec{x}^h)\|$  or relative residual norm  $\|\frac{F(\vec{x}^h)}{F(\vec{x}^0)}\|$  of the mismatch function  $F(\vec{x}^h)$  at each iteration. The Newton power flow method has a quadratic convergence when iterates are close enough to the solution. The Newton power flow methods formulate  $F(\vec{x})$  as power or current mismatch functions and designate the unknown bus voltages and angles as the problem variables  $\vec{x}$  using three different coordinates such as polar, Cartesian and complex form. Table 3 displays the problem variables defined in different coordinates.

4.1. Power-mismatch formulation:

The power flow problem (7) is formulated as the power-mismatch function  $F(\vec{x})$  as follows:

$$\begin{aligned}
 F_i(\vec{x}) &= \Delta S_i(\vec{x}) = S_i^{sp} - S_i(\vec{x}) \\
 &= S_i^{sp} - V_i \sum_{k=1}^N Y_{ik}^* V_k^* \quad \forall i \in 1 \dots N
 \end{aligned}
 \tag{9}$$

where  $S_i^{sp} = P_i^{sp} + iQ_i^{sp}$  is the specified complex power injection at bus  $i$ . In general, specified active power  $P_i^{sp}$  and reactive power  $Q_i^{sp}$  injections at bus  $i$  are given by following equations:

$$P_i^{sp} = P_i^G - P_i^L \tag{10}$$

$$Q_i^{sp} = Q_i^G - Q_i^L \tag{11}$$

where  $P_i^G$  and  $Q_i^G$  are specified active and reactive power generation whereas  $P_i^L$  and  $Q_i^L$  are specified active and reactive power loads respectively. In this paper,  $P_i^L$  and  $Q_i^L$  are modeled as constant power loads.

The complex power-mismatch function (9) is separated into real equations and variables using polar and Cartesian coordinates. Table 4 shows power-mismatch functions in different coordinates. An application of the first order Taylor approximation to the power-mismatch functions results in a linear system of Eqs. (8) that is solved at each Newton iteration. Table 5 presents all equations computing the elements of the Jacobian matrix in different coordinates which are the partial derivatives of the power-mismatch function.

4.1.1. Polar power-mismatch version (NR-p-pol [2])

The Jacobian matrix equation (8) derived from the power-mismatch function in polar coordinates is given in the partitioned form for convenience of presentation:

$$- \left[ \begin{array}{c|c} J^{11} & J^{12} \\ \hline J^{21} & J^{22} \end{array} \right] \left[ \begin{array}{c} \Delta\delta \\ \Delta|V| \end{array} \right] = \left[ \begin{array}{c} \Delta P \\ \Delta Q \end{array} \right] \tag{12}$$

where all sub-matrices are computed as  $J^{11} = \frac{\partial \Delta P}{\partial \delta}$ ,  $J^{12} = \frac{\partial \Delta P}{\partial |V|}$ ,  $J^{21} = \frac{\partial \Delta Q}{\partial \delta}$  and  $J^{22} = \frac{\partial \Delta Q}{\partial |V|}$ . The Jacobian matrix equation (12) has to be modified for all PV buses since the voltage magnitude  $|V_j|$  is specified instead of the reactive power  $Q_j$  at each PV bus  $j$ . Therefore,  $Q_j^{sp}$  cannot be computed and  $\Delta Q_j$  cannot be formulated for each PV bus  $j$ . All partial derivatives of it with respect to voltage magnitude  $|V_i|$  and angle  $\delta_i$  cannot be taken. Similarly,  $\Delta|V_j|$  does need to be computed for

**Table 4**  
Power-mismatch function in different coordinates.

Coordinates	Power-mismatch function: $F_i(\vec{x}) = \Delta S_i(\vec{x})$
Polar	$\Delta P_i(\vec{x}) = P_i^{sp} - \sum_{k=1}^N  V_i  V_k (G_{ik} \cos \delta_{ik} + B_{ik} \sin \delta_{ik})$
	$\Delta Q_i(\vec{x}) = Q_i^{sp} - \sum_{k=1}^N  V_i  V_k (G_{ik} \sin \delta_{ik} - B_{ik} \cos \delta_{ik})$
Cartesian	$\Delta P_i(\vec{x}) = P_i^{sp} - \sum_{k=1}^N (V_i^r(G_{ik}V_k^r - B_{ik}V_k^m) + V_i^m(B_{ik}V_k^r + G_{ik}V_k^m))$
	$\Delta Q_i(\vec{x}) = Q_i^{sp} - \sum_{k=1}^N (V_i^m(G_{ik}V_k^r - B_{ik}V_k^m) - V_i^r(B_{ik}V_k^r + G_{ik}V_k^m))$
Complex form	$\Delta S_i(\vec{x}) = S_i^{sp} - V_i \sum_{k=1}^N Y_{ik}^* V_k^*$

**Table 5**  
The partial derivatives of the power-mismatch function in different coordinates.

Coordinates	$J_{ik} = \frac{\partial F_i(\vec{x})}{\partial x_k}$	
Polar	$i \neq k$	$\frac{\partial \Delta P_i(\vec{x})}{\partial  V_k } = - V_i (G_{ik} \cos \delta_{ik} + B_{ik} \sin \delta_{ik})$
		$\frac{\partial \Delta Q_i(\vec{x})}{\partial  V_k } = - V_i (G_{ik} \sin \delta_{ik} - B_{ik} \cos \delta_{ik})$
		$\frac{\partial \Delta P_i(\vec{x})}{\partial \delta_k} = - V_i  V_k (G_{ik} \sin \delta_{ik} - B_{ik} \cos \delta_{ik})$
		$\frac{\partial \Delta Q_i(\vec{x})}{\partial \delta_k} = - V_i  V_k (-G_{ik} \cos \delta_{ik} - B_{ik} \sin \delta_{ik})$
	$i = k$	$\frac{\partial \Delta P_i(\vec{x})}{\partial  V_i } = -(2 V_i G_{ii} + \sum_{i \neq k}  V_k (G_{ik} \cos \delta_{ik} + B_{ik} \sin \delta_{ik}))$
		$\frac{\partial \Delta Q_i(\vec{x})}{\partial  V_i } = -(2 V_i B_{ii} + \sum_{i \neq k}  V_k (G_{ik} \sin \delta_{ik} - B_{ik} \cos \delta_{ik}))$
		$\frac{\partial \Delta P_i(\vec{x})}{\partial \delta_i} = -\sum_{i \neq k}  V_i  V_k (-G_{ik} \sin \delta_{ik} + B_{ik} \cos \delta_{ik})$
		$\frac{\partial \Delta Q_i(\vec{x})}{\partial \delta_i} = -\sum_{i \neq k}  V_i  V_k (G_{ik} \cos \delta_{ik} + B_{ik} \sin \delta_{ik})$
Cartesian	$i \neq k$	$\frac{\partial \Delta P_i(\vec{x})}{\partial V_k^r} = -(V_i^r G_{ik} + V_i^m B_{ik})$
		$\frac{\partial \Delta Q_i(\vec{x})}{\partial V_k^r} = -(V_i^m G_{ik} - V_i^r B_{ik})$
		$\frac{\partial \Delta P_i(\vec{x})}{\partial V_k^m} = -(V_i^m G_{ik} - V_i^r B_{ik})$
		$\frac{\partial \Delta Q_i(\vec{x})}{\partial V_k^m} = V_i^r G_{ik} + V_i^m B_{ik}$
	$i = k$	$\frac{\partial \Delta P_i(\vec{x})}{\partial V_i^r} = -(V_i^r G_{ii} + V_i^m B_{ii} + \sum_{k=1}^N (G_{ik}V_k^r - B_{ik}V_k^m))$
		$\frac{\partial \Delta Q_i(\vec{x})}{\partial V_i^r} = -(V_i^m G_{ii} - V_i^r B_{ii} + \sum_{k=1}^N (B_{ik}V_k^r + G_{ik}V_k^m))$
Complex form	$i \neq k$	$\frac{\partial \Delta S_i(\vec{x})}{\partial V_k} = -V_i Y_{ik}^*$
	$i = k$	$\frac{\partial \Delta S_i(\vec{x})}{\partial V_i} = -(V_i Y_{ii}^* + I^*)$

PV bus  $j$  since  $|V_j|$  is now known. Therefore, we eliminate all the  $\frac{\partial \Delta P_i}{\partial |V_j|}$ ,  $\frac{\partial \Delta Q_i}{\partial |V_j|}$ ,  $\frac{\partial \Delta Q_j}{\partial \delta_i}$  and  $\frac{\partial \Delta Q_j}{\partial |V_i|}$  from the Jacobian matrix  $J(\vec{x})$ ,  $\Delta |V_j|$  from the correction vector  $\Delta \vec{x}$  and  $\Delta Q_j$  from the power mismatch vector  $F(\vec{x})$  for each PV bus  $j$ . The order of the resulting Jacobian matrix equation is  $(2N - N_g - 2)$ .

4.1.2. Cartesian power-mismatch version (NR-p-car)

The Jacobian matrix equation (8) is defined using the power-mismatch function in Cartesian coordinates as:

$$-\begin{bmatrix} J^{11} & J^{12} \\ J^{21} & J^{22} \end{bmatrix} \begin{bmatrix} \Delta V^m \\ \Delta V^r \end{bmatrix} = \begin{bmatrix} \Delta P \\ \Delta Q \end{bmatrix} \tag{13}$$

where all sub-matrices are given as  $J^{11} = \frac{\partial \Delta P}{\partial V^m}$ ,  $J^{12} = \frac{\partial \Delta P}{\partial V^r}$ ,  $J^{21} = \frac{\partial \Delta Q}{\partial V^m}$  and  $J^{22} = \frac{\partial \Delta Q}{\partial V^r}$ . The Jacobian matrix equation (13) has to be modified for all PV buses for the same reason as we saw in 4.1.1. In this version, the reactive power-mismatch  $\Delta Q_j$  cannot be formulated for each PV bus  $j$  and therefore all partial derivatives  $\frac{\partial \Delta Q_j}{\partial V_k^m}$  and  $\frac{\partial \Delta Q_j}{\partial V_k^r}$  cannot be taken.

In paper [33], the reactive power mismatch  $\Delta Q$  is replaced by a voltage-magnitude-squared mismatch equation (1) for all PV buses and therefore all partial derivatives  $\frac{\partial \Delta Q_j}{\partial V_k^m}$  and  $\frac{\partial \Delta Q_j}{\partial V_k^r}$  are also replaced by  $\frac{\partial \Delta |V_j|^2}{\partial V_k^m}$  and  $\frac{\partial \Delta |V_j|^2}{\partial V_k^r}$  respectively.

Moreover, the order of the Jacobian matrix equation remains  $(2N - 2)$  and it is concluded in [33] that the method is slightly less reliable and less rapid in convergence than the polar power-mismatch version 4.1.1.

In this paper, we develop a new approach that improves the performance of this version. In our approach, the reactive power-mismatch  $\Delta Q_j$  is removed from the power-mismatch vector  $F(\vec{x})$  for all PV buses and therefore all partial derivatives  $\frac{\partial \Delta Q_i}{\partial V_k^m}$  and  $\frac{\partial \Delta Q_i}{\partial V_k^r}$  are also eliminated from the Jacobian matrix  $J(\vec{x})$ . As a result of the elimination, the Jacobian matrix becomes a rectangular matrix. In order to make the Jacobian matrix square, we use Eq. (2) with  $\Delta|V_j| = 0$  since  $|V_j|$  is now specified for each PV bus  $j$ . This gives us the relation between the corrections  $\Delta V_j^r$  and  $\Delta V_j^m$  as:

$$\Delta V_j^r = -\frac{V_j^m}{V_j^r} \Delta V_j^m. \tag{14}$$

Using Eq. (14), the column of the Jacobian matrix with respect to the derivatives  $\frac{\partial \Delta P_i}{\partial V_j^r}$  and  $\frac{\partial \Delta Q_i}{\partial V_j^r}$  is added to the column with respect to the derivatives  $\frac{\partial \Delta P_i}{\partial V_j^m}$  and  $\frac{\partial \Delta Q_i}{\partial V_j^m}$  as follows:

$$\frac{\partial \Delta P_i}{\partial V_j^m} \Delta V_j^m = \left( \frac{\partial \Delta P_i}{\partial V_j^m} - \frac{V_j^m}{V_j^r} \frac{\partial \Delta P_i}{\partial V_j^r} \right) \Delta V_j^m \tag{15}$$

$$\frac{\partial \Delta Q_i}{\partial V_j^m} \Delta V_j^m = \left( \frac{\partial \Delta Q_i}{\partial V_j^m} - \frac{V_j^m}{V_j^r} \frac{\partial \Delta Q_i}{\partial V_j^r} \right) \Delta V_j^m. \tag{16}$$

Now the correction  $\Delta V_j^r$  can be eliminated from the correction vector  $\Delta \vec{x}$  for each PV bus  $j$  and therefore the order of the Jacobian matrix equation (13) is  $(2N - N_g - 2)$ .

4.1.3. Complex power-mismatch version (NR-p-com)

The Jacobian matrix equation (8) is computed using the power-mismatch function in complex form as:

$$- [ J ] [ \Delta V ] = [ \Delta S ] \tag{17}$$

where the Jacobian matrix  $J = \frac{\partial \Delta S}{\partial V}$  is obtained by taking the first order partial derivatives of the complex power-mismatch functions with respect to the complex voltage  $V$ . The Jacobian matrix equation (17) holds for all PQ buses but not for all PV buses because the complex power mismatch  $\Delta S$  cannot be formulated for all PV buses. Therefore, this version can be applied to solve the power flow problem on networks with only a slack bus and PQ buses.

4.2. Current-mismatch formulation:

The current equation (5) and the power flow problem (6) are used to formulate the current-mismatch function  $F(\vec{x})$  as follows:

$$\begin{aligned} F_i(\vec{x}) &= \Delta I_i(\vec{x}) = I_i^{sp} - I_i(\vec{x}) \\ &= \left( \frac{S_i^{sp}}{V_i} \right)^* - \sum_{k=1}^N Y_{ik} V_k \quad \forall i \in 1 \dots N \end{aligned} \tag{18}$$

where  $I_i^{sp} = \left( \frac{S_i^{sp}}{V_i} \right)^*$  is the specified complex current injection at bus  $i$ .

The current-mismatch function (18) can be also expressed in terms of the power-mismatch function (9) as follows:

$$\Delta I_i = \left( \frac{\Delta S_i}{V_i} \right)^* \quad (\text{complex}) \tag{19}$$

$$= \frac{\cos \delta_i \Delta P_i + \sin \delta_i \Delta Q_i}{|V_i|} + i \frac{\sin \delta_i \Delta P_i - \cos \delta_i \Delta Q_i}{|V_i|} \quad (\text{polar}) \tag{20}$$

$$= \frac{V_i^r \Delta P_i + V_i^m \Delta Q_i}{|V_i|^2} + i \frac{V_i^m \Delta P_i - V_i^r \Delta Q_i}{|V_i|^2} \quad (\text{Cartesian}). \tag{21}$$

The complex current-mismatch function (18) is separated into real equations and variables using polar and Cartesian coordinates. Table 6 shows the current-mismatch functions in different coordinates. An application of a first order Taylor approximation to the current-mismatch function results in a linear system of Eqs. (8) that is solved in every Newton iteration. Table 7 gives all equations defining the elements of the Jacobian matrix in different coordinates.

4.2.1. Polar current-mismatch version (NR-c-pol)

The Jacobian matrix equation (8) is derived from the current-mismatch function in polar coordinates as:

$$- \begin{bmatrix} J^{11} & | & J^{12} \\ J^{21} & | & J^{22} \end{bmatrix} \begin{bmatrix} \Delta \delta \\ \Delta |V| \end{bmatrix} = \begin{bmatrix} \Delta I^r \\ \Delta I^m \end{bmatrix} \tag{22}$$



**Table 6**  
Current-mismatch function in different coordinates.

Coordinates	Current-mismatch function: $F_i(\vec{x}) = \Delta I_i(\vec{x})$
Polar	$\Delta I_i^r(\vec{x}) = \frac{P_i^{SP} \cos \delta_i + Q_i^{SP} \sin \delta_i}{ V_i } - \sum_{k=1}^N  V_k  (G_{ik} \cos \delta_k - B_{ik} \sin \delta_k)$
	$\Delta I_i^m(\vec{x}) = \frac{P_i^{SP} \sin \delta_i - Q_i^{SP} \cos \delta_i}{ V_i } - \sum_{k=1}^N  V_k  (G_{ik} \sin \delta_k + B_{ik} \cos \delta_k)$
Cartesian	$\Delta I_i^r(\vec{x}) = \frac{P_i^{SP} V_i^r + Q_i^{SP} V_i^m}{(V_i^r)^2 + (V_i^m)^2} - \sum_{k=1}^N (G_{ik} V_k^r - B_{ik} V_k^m)$
	$\Delta I_i^m(\vec{x}) = \frac{P_i^{SP} V_i^m - Q_i^{SP} V_i^r}{(V_i^r)^2 + (V_i^m)^2} - \sum_{k=1}^N (G_{ik} V_k^m + B_{ik} V_k^r)$
Complex form	$\Delta I_i(\vec{x}) = \left( \frac{S_i^r}{V_i} \right)^* - \sum_{k=1}^N Y_{ik} V_k$

**Table 7**  
The partial derivatives of the current-mismatch function in different coordinates.

Coordinates	$J_{ik} = \frac{\partial F_i(\vec{x})}{\partial x_k}$			
Polar	$i \neq k$	$\frac{\partial \Delta I_i^r(\vec{x})}{\partial  V_k } = -(G_{ik} \cos \delta_k - B_{ik} \sin \delta_k)$ $\frac{\partial \Delta I_i^m(\vec{x})}{\partial  V_k } = -(G_{ik} \sin \delta_k + B_{ik} \cos \delta_k)$ $\frac{\partial \Delta I_i^r(\vec{x})}{\partial \delta_k} =  V_k  (G_{ik} \sin \delta_k + B_{ik} \cos \delta_k)$ $\frac{\partial \Delta I_i^m(\vec{x})}{\partial \delta_k} = - V_k  (G_{ik} \cos \delta_k - B_{ik} \sin \delta_k)$		
	$i = k$	$\frac{\partial \Delta I_i^r(\vec{x})}{\partial  V_i } = -(G_{ii} \cos \delta_i - B_{ii} \sin \delta_i) - \frac{P_i^{SP} \cos \delta_i + Q_i^{SP} \sin \delta_i}{ V_i ^2}$ $\frac{\partial \Delta I_i^m(\vec{x})}{\partial  V_i } = -(G_{ii} \sin \delta_i + B_{ii} \cos \delta_i) - \frac{P_i^{SP} \sin \delta_i - Q_i^{SP} \cos \delta_i}{ V_i ^2}$ $\frac{\partial \Delta I_i^r(\vec{x})}{\partial \delta_i} =  V_i  (G_{ii} \sin \delta_i + B_{ii} \cos \delta_i) - \frac{P_i^{SP} \sin \delta_i - Q_i^{SP} \cos \delta_i}{ V_i }$ $\frac{\partial \Delta I_i^m(\vec{x})}{\partial \delta_i} = - V_i  (G_{ii} \cos \delta_i - B_{ii} \sin \delta_i) + \frac{P_i^{SP} \cos \delta_i + Q_i^{SP} \sin \delta_i}{ V_i }$		
	Cartesian	$i \neq k$	$\frac{\partial \Delta I_i^r(\vec{x})}{\partial V_k^r} = -G_{ik}$ $\frac{\partial \Delta I_i^m(\vec{x})}{\partial V_k^m} = B_{ik}$ $\frac{\partial \Delta I_i^r(\vec{x})}{\partial V_k^m} = B_{ik}$ $\frac{\partial \Delta I_i^m(\vec{x})}{\partial V_k^r} = -G_{ik}$	
		$i = k$	$\frac{\partial \Delta I_i^r(\vec{x})}{\partial V_i^r} = -G_{ii} - \frac{P_i^{SP} ((V_i^r)^2 - (V_i^m)^2) + 2V_i^r V_i^m Q_i^{SP}}{ V_i ^4}$ $\frac{\partial \Delta I_i^m(\vec{x})}{\partial V_i^r} = -B_{ii} + \frac{Q_i^{SP} ((V_i^r)^2 - (V_i^m)^2) - 2V_i^r V_i^m P_i^{SP}}{ V_i ^4}$ $\frac{\partial \Delta I_i^r(\vec{x})}{\partial V_i^m} = B_{ii} + \frac{Q_i^{SP} ((V_i^r)^2 - (V_i^m)^2) - 2V_i^r V_i^m P_i^{SP}}{ V_i ^4}$ $\frac{\partial \Delta I_i^m(\vec{x})}{\partial V_i^m} = -G_{ii} + \frac{P_i^{SP} ((V_i^r)^2 - (V_i^m)^2) + 2V_i^r V_i^m Q_i^{SP}}{ V_i ^4}$	
		Complex form	$i \neq k$	$\frac{\partial \Delta I_i(\vec{x})}{\partial V_k} = -Y_{ik}$
			$i = k$	$\frac{\partial \Delta I_i(\vec{x})}{\partial V_i} = -\left( \frac{S_i^r}{V_i^2} + Y_{ii} \right)$

where all sub-matrices are computed as  $J^{11} = \frac{\partial \Delta I^r}{\partial \delta}$ ,  $J^{12} = \frac{\partial \Delta I^r}{\partial |V|}$ ,  $J^{21} = \frac{\partial \Delta I^m}{\partial \delta}$  and  $J^{22} = \frac{\partial \Delta I^m}{\partial |V|}$ . Same as the polar power-mismatch version 4.1.1,  $\Delta |V_j|$  needs to be computed for each PV bus  $j$  since  $|V_j|$  is now known. Therefore, we eliminate all the  $\frac{\partial \Delta I_i^r}{\partial |V_j|}$  and  $\frac{\partial \Delta I_i^m}{\partial |V_j|}$  from the Jacobian matrix  $J(\vec{x})$  and  $\Delta |V_j|$  from the correction vector  $\Delta \vec{x}$  for each PV bus  $j$ . As a result of the elimination, the Jacobian matrix becomes a rectangular matrix.

In paper [35], each PQ bus is represented by the real  $\Delta I^r$  and imaginary  $\Delta I^m$  current-mismatch functions. A PV bus is represented by the active power-mismatch  $\Delta P$  and the voltage-magnitude-squared mismatch equation (1). Thus, the order of the Jacobian matrix equation is  $(2N - 2)$  and it is concluded in [16] that these versions perform less satisfactorily than the power-mismatch versions.

**Table 8**

The partial derivatives of the current-mismatch function in polar coordinates with respect to the reactive power  $Q_j$ .

$J_{ij} = \frac{\partial F_i}{\partial x_j}$	$i \neq j$	$\frac{\partial \Delta I_i^r(\vec{x})}{\partial Q_j} = 0$
		$\frac{\partial \Delta I_i^m(\vec{x})}{\partial Q_j} = 0$
	$i = j$	$\frac{\partial \Delta I_j^r(\vec{x})}{\partial Q_j} = \frac{\sin \delta_j}{ V_j ^{3p}}$
		$\frac{\partial \Delta I_j^m(\vec{x})}{\partial Q_j} = -\frac{\cos \delta_j}{ V_j ^{3p}}$

**Table 9**

The partial derivatives of the current-mismatch function in Cartesian coordinates with respect to the reactive power  $Q_j$ .

$J_{ij} = \frac{\partial F_i}{\partial x_j}$	$i \neq j$	$\frac{\partial \Delta I_i^r(\vec{x})}{\partial Q_j} = 0$
		$\frac{\partial \Delta I_i^m(\vec{x})}{\partial Q_j} = 0$
	$i = j$	$\frac{\partial \Delta I_j^r(\vec{x})}{\partial Q_j} = \frac{V_j^m}{(V_j^r)^2 + (V_j^m)^2}$
		$\frac{\partial \Delta I_j^m(\vec{x})}{\partial Q_j} = \frac{-V_j^r}{(V_j^r)^2 + (V_j^m)^2}$

In our approach, the reactive power  $Q_j$  is chosen as a dependent variable as  $|V|$  and  $\delta$  for each PV bus  $j$  because we use the current-mismatch formulation directly. Since  $Q_j$  is an unknown variable, all first order partial derivatives  $\frac{\partial \Delta I_i^r}{\partial Q_j}$  and  $\frac{\partial \Delta I_i^m}{\partial Q_j}$  have to be computed as given in Table 8:

Now we add the derivatives  $\frac{\partial \Delta I_i^r}{\partial Q_j}$  and  $\frac{\partial \Delta I_i^m}{\partial Q_j}$  into the Jacobian matrix  $J(\vec{x})$  and the correction  $\Delta Q_j$  into the correction vector  $\Delta \vec{x}$  for each PV bus  $j$ . As a result, the Jacobian matrix becomes a square again. The initial reactive power  $Q_j^0$  at each PV bus  $j$  is computed as follows:

$$Q_j^0 = \sum_{k=1}^N |V_j| |V_k| (G_{jk} \sin \delta_{jk} - B_{jk} \cos \delta_{jk}). \tag{23}$$

In each Newton iteration, the correction  $\Delta Q_j$  is computed and the reactive power  $Q_j$  is updated using the computed correction.

4.2.2. Cartesian current-mismatch version (NR-c-car)

The Jacobian matrix equation (8) is computed using the current-mismatch function in Cartesian coordinates as:

$$-\begin{bmatrix} J^{11} & J^{12} \\ J^{21} & J^{22} \end{bmatrix} \begin{bmatrix} \Delta V^m \\ \Delta V^r \end{bmatrix} = \begin{bmatrix} \Delta I^r \\ \Delta I^m \end{bmatrix} \tag{24}$$

where all sub-matrices are given as  $J^{11} = \frac{\partial \Delta I^r}{\partial V^m}$ ,  $J^{12} = \frac{\partial \Delta I^r}{\partial V^r}$ ,  $J^{21} = \frac{\partial \Delta I^m}{\partial V^m}$  and  $J^{22} = \frac{\partial \Delta I^m}{\partial V^r}$ .

In paper [36], the real  $\Delta I^r$  and imaginary  $\Delta I^m$  current-mismatch functions are expressed in terms of the real  $\Delta P$  and reactive  $\Delta Q$  power-mismatch functions. Then the reactive power-mismatch  $\Delta Q$  is considered as a dependent variable for each PV bus and computed at each Newton iteration. Minor attempts were made to speed up the solution method using a partly constant approximation of the Jacobian during the iterations, but the results were not encouraging [36].

In our approach, the reactive power  $Q_j$  is chosen as a dependent variable for each PV bus  $j$  as polar current-mismatch version 4.2.1. Since  $Q_j$  is an unknown variable, all the first order partial derivatives  $\frac{\partial \Delta I_i^r}{\partial Q_j}$  and  $\frac{\partial \Delta I_i^m}{\partial Q_j}$  have to be computed as shown in Table 9:

Now we add the derivatives  $\frac{\partial \Delta I_i^r}{\partial Q_j}$  and  $\frac{\partial \Delta I_i^m}{\partial Q_j}$  into the Jacobian matrix  $J(\vec{x})$  and the correction  $\Delta Q_j$  into the correction vector  $\Delta \vec{x}$  for each PV bus  $j$ . After the addition, the Jacobian matrix becomes a rectangular matrix. In order to make the Jacobian matrix square, we add the column of the Jacobian matrix with respect to the derivatives  $\frac{\partial \Delta I_i^r}{\partial V_j^r}$  and  $\frac{\partial \Delta I_i^m}{\partial V_j^r}$  to the column with respect to the derivatives  $\frac{\partial \Delta I_i^r}{\partial V_j^m}$  and  $\frac{\partial \Delta I_i^m}{\partial V_j^m}$  using (14) as follows:

$$\frac{\partial \Delta I_i^r}{\partial V_j^m} \Delta V_j^m = \left( \frac{\partial \Delta I_i^r}{\partial V_j^m} - \frac{V_j^m}{V_j^r} \frac{\partial \Delta I_i^r}{\partial V_j^r} \right) \Delta V_j^m \tag{25}$$

**Table 10**  
Bus voltage corrections in different coordinates.

Coordinates	Type of Bus	$\vec{x}^{h+1} := \vec{x}^h + \Delta\vec{x}^h$
Polar	PQ and PV	$V_i^{(h+1)} =  V_i ^{(h+1)} e^{j\delta_i^{(h+1)}}$
		$ V_i ^{(h+1)} =  V_i ^{(h)} + \Delta V_i ^{(h)}$
		$\delta_i^{(h+1)} = \delta_i^{(h)} + \Delta\delta_i^{(h)}$
Cartesian	PQ and PV	$V_i^{(h+1)} = (V_i^r)^{(h+1)} + j(V_i^m)^{(h+1)}$
		$(V_i^r)^{(h+1)} = (V_i^r)^{(h)} + (\Delta V_i^r)^{(h)}$
	PQ	$(V_i^m)^{(h+1)} = (V_i^m)^{(h)} + (\Delta V_i^m)^{(h)}$
		$V_i^{(h+1)} =  V_i ^{(h+1)} e^{j\delta_i^{(h+1)}}$
Complex	PQ	$\Delta V_j  = \frac{V_j^r}{ V_j } \Delta V_j^r + \frac{V_j^m}{ V_j } \Delta V_j^m$
		$\Delta\delta_j = \frac{V_j^r}{ V_j ^2} \Delta V_j^m - \frac{V_j^m}{ V_j ^2} \Delta V_j^r$
	PV	$\Delta\delta_j = \frac{\Delta V_j^m}{V_j^r}$
	PQ (NR-p-com)	$V_i^{(h+1)} = V_i^{(h)} + (\Delta V_i^{(h)})^*$
	PQ (NR-c-com)	$V_i^{(h+1)} = V_i^{(h)} + \Delta V_i^{(h)}$

$$\frac{\partial \Delta I_i^m}{\partial V_j^m} \Delta V_j^m = \left( \frac{\partial \Delta I_i^m}{\partial V_j^m} - \frac{V_j^m}{V_j^r} \frac{\partial \Delta I_i^m}{\partial V_j^r} \right) \Delta V_j^m. \tag{26}$$

Then the correction  $\Delta V_j^r$  can be eliminated from the correction vector  $\Delta\vec{x}$  for each PV bus  $j$ . The initial reactive power  $Q_j^0$  at a PV bus  $j$  is computed as follows:

$$Q_j^0 = \sum_{k=1}^N \left( V_j^m (G_{jk} V_k^r - B_{jk} V_k^m) - V_j^r (B_{jk} V_k^r + G_{jk} V_k^m) \right). \tag{27}$$

In each Newton iteration, the correction  $\Delta Q_j$  is computed and the reactive power  $Q_j$  is updated using the computed correction.

4.2.3. *Complex current-mismatch version (NR-c-com)*

The Jacobian matrix equation (8) is calculated using the current-mismatch function in complex form as:

$$- [ J ] [ \Delta V ] = [ \Delta I ] \tag{28}$$

where the Jacobian matrix  $J = \frac{\partial \Delta S}{\partial V}$  is obtained by taking the first order partial derivatives of the complex current-mismatch functions with respect to the complex voltage  $V$ . Same as the complex power-mismatch version 4.1.3, this version is applicable for the power flow problem on networks with only a slack bus and PQ buses.

Bus voltage corrections in different coordinates are given in Table 10:

5. Numerical experiment

The newly developed/improved versions of the Newton power flow method (Cartesian power-mismatch, polar current-mismatch, Cartesian current-mismatch and complex current-mismatch) discussed in Section 4, are compared to the existing versions of the Newton power flow method (polar power-mismatch [2], Cartesian power-mismatch [33] and Cartesian current-mismatch [36]) for the numerical experiments. Two distribution networks (DCase33 [38] and DCase69 [39]) and four transmission networks taken from Matpower [40] (case1354pegase, case2737sop, case9241pegase and case13659pegase) are used to test the convergence ability and scalability of all variants of the Newton power flow solution method. All methods are implemented in Matlab and the constant power load model is used for loads. The relative convergence tolerance is set to  $10^{-5}$  and the maximum number of iterations is set to 10. All experiments are performed on an Intel computer with four cores i5-4690 3.5 GHz CPU and 64Gb memory, running a Debian 64-bit Linux 8.7 distribution.

5.1. Distribution networks

The convergence result of all Newton power solution methods for two distribution network (DCase33 and DCase69) is shown in Table 11.

**Table 11**  
Distribution networks: DCase33 and DCase69.

Methods	Test cases					
	DCase33			DCase69		
	iter	time	$\ F(\vec{x})\ _\infty$	iter	time	$\ F(\vec{x})\ _\infty$
NR-p-pol [2]	3	0.0072	7.4675e−06	4	0.0113	5.5875e−09
NR-p-car	3	0.0063	1.0433e−06	3	0.0068	8.1777e−06
NR-p-car [33]	3	0.0072	1.0897e−06	3	0.0081	8.0940e−06
NR-p-com	6	0.0055	6.4610e−06	7	0.0063	4.0138e−06
NR-c-pol	3	0.0081	1.4291e−09	3	0.0094	8.5226e−09
NR-c-car	3	0.0068	1.3954e−09	3	0.0081	1.9503e−08
NR-c-car [36]	3	0.0111	1.3964e−09	3	0.0124	1.9476e−08
NR-c-com	7	0.0055	5.3792e−06	10	0.0076	2.7697e−06

**Table 12**  
Small transmission networks: TCase1354 and TCase2737.

Methods	Test cases					
	TCase1354			TCase2737		
	iter	time	$\ F(\vec{x})\ _\infty$	iter	time	$\ F(\vec{x})\ _\infty$
NR-p-pol [2]	3	0.0284	6.2678e−06	4	0.0640	1.5353e−08
NR-p-car	3	0.0265	1.5795e−06	4	0.0634	2.3500e−06
NR-p-car [33]	3	0.0298	2.2486e−06	5	0.0777	2.8518e−06
NR-c-pol	3	0.0313	8.3005e−10	4	0.0700	6.1735e−07
NR-c-car	3	0.0306	6.1446e−10	4	0.0649	8.6780e−07
NR-c-car [36]	5	0.0507	9.9969e−06	5	0.0838	7.9842e−07

**Table 13**  
Large transmission networks: TCase9241 and TCase13659.

Methods	Test cases					
	TCase9241			TCase13659		
	iter	time	$\ F(\vec{x})\ _\infty$	iter	time	$\ F(\vec{x})\ _\infty$
NR-p-pol [2]	6	0.3555	2.1292e−09	5	0.3899	2.2891e−09
NR-p-car	5	0.2908	2.1026e−08	6	0.4689	7.9833e−12
NR-p-car [33]	5	0.3180	2.0742e−06	10	0.8899	1.401e+148
NR-c-pol	3	0.1973	6.4746e−07	4	0.3634	3.4366e−09
NR-c-car	3	0.1993	1.9438e−06	4	0.3619	8.6170e−09
NR-c-car [36]	10	0.6595	0.0023	10	0.9036	1.1482

We observe that variants using complex form (NR-p-com and NR-c-com) need more iterations and have a linear convergence compared to other variants. Thus, NR-p-com and NR-c-com are the least preferable variants of the Newton power flow method. Furthermore, remaining versions employing Polar and Cartesian coordinates converge after the same number of iterations. However, we discover that the residual norm of current-mismatch functions is much smaller than the residual norm of power-mismatch functions regardless of the choice of the coordinates. Thus, we can conclude that versions using current-mismatch functions are more suitable for solving distribution power flow problems than versions using power-mismatch functions. Variants polar current-mismatch (NR-c-pol) and Cartesian current-mismatch (NR-c-car) developed in this paper perform the best for two distribution networks in terms of both a number of iterations and the residual norm.

## 5.2. Transmission networks

Since the complex power-mismatch and complex current-mismatch versions are developed only for PQ buses, these variants are not applied to transmission power flow problems including PV buses. Tables 12 and 13 show the convergence result of all solution methods for transmission networks (TCase1354, TCase2737, TCase9241 and TCase13659).

For smaller transmission networks TCase1354 and TCase2737, all versions result in the same behavior except the Cartesian current-mismatch version developed in [36] which requires extra one iteration.

For the second large transmission network TCase9241, the variant NR-c-car [36] diverges whereas other versions converge. Furthermore, NR-c-pol and NR-c-car versions developed in this paper converge after only three iterations whereas other versions (NR-p-pol [2], NR-p-car and NR-p-car [33]) need five to six iterations. For the largest transmission network TCase13659, both versions NR-p-car [33] and NR-c-car [36] diverge whereas all variants (NR-p-car, NR-c-pol and NR-c-car) developed in this paper and NR-p-pol [2] find the solution. Additionally, these four converged versions

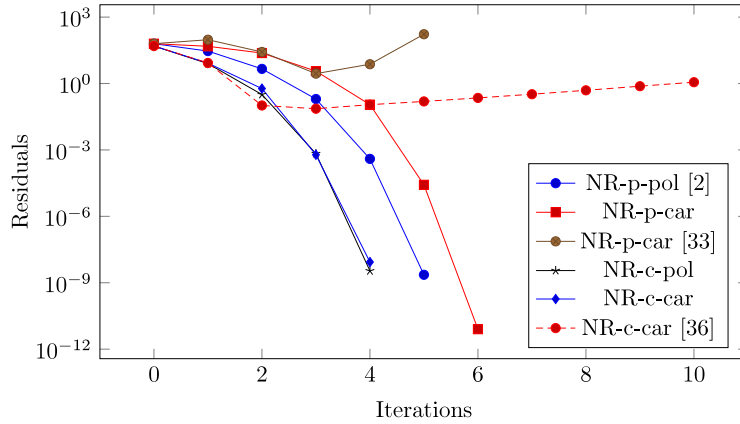


Fig. 1. Convergence of all Newton power flow versions on transmission network TCase13659.

have a quadratic convergence as shown in Fig. 1. Moreover, NR-c-pol and NR-c-car variants converge faster than the most famous variant NR-p-pol [2] in terms of iterations for both large transmission networks. Thus, we can conclude that polar current-mismatch (NR-c-pol) and Cartesian current-mismatch (NR-c-car) variants developed in this paper are more preferable for large transmission power flow problems.

### 6. Conclusion

In this paper, we formulate and analyze the Newton based power flow methods that are used for the power flow computation on balanced distribution and transmission networks. For the various methods we consider two different mismatch functions: the current and power balance equations and three different coordinate systems: Cartesian, polar and complex form. This leads to six different versions of the Newton power flow method. Studying these versions in a common framework enables us to analyze and compare all variants in a unified way. Furthermore, the existing variants of the Newton power flow method developed in [2,33,36] are implemented and compared with the newly developed/improved versions of the Newton power flow method (Cartesian power-mismatch, polar current-mismatch, Cartesian current-mismatch and complex current-mismatch). In case of the polar and Cartesian current-mismatch versions, the reactive power  $Q$  is chosen as a dependent variable for each PV bus. Thus, we compute the correction  $\Delta Q$  at each iteration and update  $Q$  using the computed corrections. Eqs. (2) and (3) are used instead of the voltage-magnitude-squared mismatch equation (1) in versions using Cartesian coordinates. The order of the Jacobian matrix equation is  $(2N - N_g - 2)$  for the versions using the power-mismatch function whereas versions using the current-mismatch function have  $(2N - 2)$  linear equations.

The polar current-mismatch and Cartesian current-mismatch variants of the Newton power flow method that are developed in this paper deliver the best result for both distribution and transmission networks. Therefore, we encourage power system operators to apply these two variants for power flow computations on balanced distribution and transmission networks.

In addition, the Cartesian current-mismatch version has an advantage in the calculation of the Jacobian matrix because its off-diagonal elements are constant and equal to the terms of the nodal admittance matrix. Moreover, depending on the properties of the given network, one version can work better than others. Therefore, it is crucial to study which version is more suitable for what kind of power networks. In the near future, these newly developed versions will be applied to three-phase power flow problems on unbalanced distribution networks and will be implemented in Matpower.

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### Appendix. Notation

- $N$ : number of buses in the network
- $N_g$ : number of generator buses
- $h$ : iteration counter
- $V_k = V_k^r + iV_k^m$ : complex voltage at bus  $k$

$|V_k|, \delta_k$ : voltage magnitude and angle at bus  $k$

$\vec{x}$ : vector of unknown variables

$\Delta\vec{x}$ : correction of unknown variables

$F_k(\vec{x})$ : complex power or current mismatch function at bus  $k$

$J(\vec{x})$ : Jacobian matrix of the mismatch function

$\Delta S_k = \Delta P_k + i\Delta Q_k$ : complex power mismatch at bus  $k$

$\Delta I_k = \Delta I_k^r + i\Delta I_k^m$ : complex current mismatch at bus  $k$

$S_k^{sp} = P_k^{sp} + iQ_k^{sp}$ : specified complex power at bus  $k$

$S_k^G = P_k^G + iQ_k^G$ : generated complex power at bus  $k$

$S_k^L = P_k^L + iQ_k^L$ : complex power load at bus  $k$

$Y_{ik} = G_{ik} + iB_{ik}$ : ( $i, k$ ) the element of nodal admittance matrix

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